

# UNCLASSIFIED

AD NUMBER
ADA186825
NEW LIMITATION CHANGE
TO Approved for public release, distribution unlimited
FROM Distribution authorized to U.S. Gov't. agencies and their contractors; Administrative/Operational Use; SEP 1987. Other requests shall be referred to Pacific Missile Test Center, Point Mugu, CA 93042.
AUTHORITY
PMTC ltr, 17 Nov 1987

THIS PAGE IS UNCLASSIFIED

2

Technical Publication TP000044

DTIC FILE COPY

# TELEMETRY APPLICATIONS HANDBOOK

By

EUGENE L. LAW  
and  
DONALD R. HUST

Weapons Instrumentation Division

DTIC  
ELECTE  
NOV 04 1987  
S D  
CSD

September 1987

DISTRIBUTION AUTHORIZED TO U.S. GOVERNMENT  
AGENCIES AND THEIR CONTRACTORS ONLY: ~~OPERATIONAL~~ A/O Use  
USE, SEPTEMBER 1987. OTHER REQUESTS FOR THIS  
DOCUMENT SHALL BE REFERRED TO THE COMMANDER,  
PACIFIC MISSILE TEST CENTER, POINT MUGU,  
CALIFORNIA, 93042-5000, ATTN: CODE 1061.  
DESTRUCTION NOTICE--DESTROY BY ANY METHOD THAT  
WILL PREVENT DISCLOSURE OF CONTENTS OR  
RECONSTRUCTION OF THIS DOCUMENT.

PACIFIC MISSILE TEST CENTER

Point Mugu, California 93042

DISTRIBUTION STATEMENT A

Approved for public release  
Distribution Unlimited

87 10 22 104

AD-A186 825



# PACIFIC MISSILE TEST CENTER

AN ACTIVITY OF THE NAVAL AIR SYSTEMS COMMAND

This handbook describes work performed for the Telemetry Group of the Range Commanders Council.

Mr. E. L. Law, Manager, Telemetry Group Support Task; Mr. D. R. Hust, Head, Electronic Design Branch; Mr. W. M. Dean, Head, Weapons Instrumentation Division; and Mr. E. D. Simmons, Chief Engineer, Weapons Evaluation Directorate have approved this handbook for publication.

W. R. Hattabaugh  
*Technical Director*

Technical Publication TP000044

Published by	Weapons Instrumentation Division
Security Classification	UNCLASSIFIED
First Printing	500 copies



DEPARTMENT OF THE NAVY

HEADQUARTERS  
PACIFIC MISSILE TEST CENTER  
POINT MUGU, CALIFORNIA 93042 -5000

IN REPLY REFER TO:

5605  
Ser 1018N/J-1162  
17 November 1987

From: Commander, Pacific Missile Test Center

Subj: TP000044, TELEMETRY APPLICATIONS HANDBOOK DATED SEPTEMBER 1987

1. We ask that the distribution statement for this technical report be changed as follows:

Approved for public release; distribution is unlimited.

*(Upon removal of distribution list)*

*A. E. Doidge*  
A. E. DOIDGE

By direction

Distribution:

COMNAVAIRSYSCOM (AIR-00D4, 2 cy's; AIR-04, 1 cy; AIR-53303, 1 cy; AIR-423, 1 cy;  
AIR-4233, 1 cy; AIR-4233B, 1 cy)  
DTIC (12 cy's)  
PACMISTESTCEN Liaison Office (1 cy)  
NAVAIRDEVCCEN (Code 6011, 1 cy)  
COMNAVSEASYSYSCOM (SEA-62Z32F, 1 cy; SEA-62Z31, 1 cy; PMS-400, 1 cy)  
NAVUSEAWARENGSTA (R. Rabel, 1 cy)  
NAVSEACENPAC (1 cy)  
NAVSEACENLANT (2 cy's)  
NAVAIRTESTCEN (RD00, 1 cy; RD42, 2 cy's; RD50, 3 cy's)  
NAVAVIONICCEN (Code 906, 1 cy; Code 811, 1 cy; Code 815, 1 cy)  
NAVSHIPWPNSYSENGSTA (Code 4521, 1 cy; Code 4250, 2 cy's)  
WPNSTA, FLTAC, Corona, CA (Code 34, 1 cy; Code 35, 1 cy; Code 3511, 1 cy; Code  
3544, 6 cy's)  
NAVORDMISTESTSTA (Code 503, 1 cy)  
LANTFLTWPNTAFAC (A. Quinones, 5 cy's, Code 80, 1 cy)  
NAVSWC (G65, 1 cy; Code 663, 1 cy)  
AEDC (DOPG, 1 cy; MS930, 1 cy)  
USAINSBD (ATSI-BD-TD, 1 cy)  
NAVOCEANSYSCEN (B641, 1 cy)  
AFWAL (FIBGA, 1 cy)  
AFTCC, Edwards AFB, CA (6520 TG/ENMD, Stop 239, 2 cy's; 6521 RANGES/ENRD, Stop 200,  
2 cy's, 6520 TESTG/EN10, 4 cy's)  
NAVWPNCEN (Code 3060, 1 cy; Code 6253, 2 cy's; Code 6406, 2 cy's; Code 6421, 3 cy's;  
Code 6426, 1 cy; Code 6423, 1 cy; Code 6233, 3 cy's; Code 6222, 1 cy; Code 6424,  
1 cy; Code 6421, 1 cy; Code 64204, 1 cy; Code 35063, 1 cy; Code 343, 1 cy)  
DIRNSA (R53, 2 cy's; V36, 2 cy's)  
AFGL, Hanscom AFB, MA (AFG2/LCR, 1 cy; AFGL/LCT, 2 cy's)  
ARDEC, Picatinny Arsenal, NJ (AMSMC-QAH-ECD, 2 cy's)  
WPNSTA DET (Code 3243, 3 cy's)  
NAS, Oceana, Virginia Beach, FL (FLTAC Field Office, 1 cy)  
White Sands Missile Range (STEWS-NR-DT, 1 cy; STEWS-ID-DT, 6 cy's)



UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE

AD-A186825

REPORT DOCUMENTATION PAGE

1. REPORT SECURITY CLASSIFICATION <b>UNCLASSIFIED</b>			1b. RESTRICTIVE MARKINGS	
2a. SECURITY CLASSIFICATION AUTHORITY			1. DISTRIBUTION/AVAILABILITY OF REPORT <b>DISTRIBUTION AUTHORIZED TO U.S. GOV'T AGENCIES AND THEIR CONTRACTORS ONLY</b>	
2b. DECLASSIFICATION/DOWNGRADING SCHEDULE			OPERATIONAL USE: SEPTEMBER 1987	
4. PERFORMING ORGANIZATION REPORT NUMBER(S) <b>TP000044</b>			5. MONITORING ORGANIZATION REPORT NUMBER(S)	
6a. NAME OF PERFORMING ORGANIZATION <b>PACIFIC MISSILE TEST CNTR</b>		6b. OFFICE SYMBOL (if applicable)	7a. NAME OF MONITORING ORGANIZATION	
6c. ADDRESS (City, State, and ZIP Code) <b>POINT MUGU, CA 93042-5000</b>			7b. ADDRESS (City, State, and ZIP Code)	
8a. NAME OF FUNDING/SPONSORING ORGANIZATION <b>TELEMETRY GROUP</b>		8b. OFFICE SYMBOL (if applicable)	9. PROCUREMENT INSTRUMENT IDENTIFICATION NUMBER	
8c. ADDRESS (City, State, and ZIP Code)			10. SOURCE OF FUNDING NUMBERS	
			PROGRAM ELEMENT NO	PROJECT NO
			TASK NO.	WORK UNIT ACCESSION NO
11. TITLE (Include Security Classification) <b>TELEMETRY APPLICATIONS HANDBOOK</b>				
12. PERSONAL AUTHOR(S) <b>EUGENE L. LAW AND DONALD R. HUST</b>				
13a. TYPE OF REPORT <b>FINAL</b>		13b. TIME COVERED FROM TO		14. DATE OF REPORT (Year, Month, Day) <b>1987, SEPTEMBER</b>
15. PAGE COUNT <b>337</b>				
16. SUPPLEMENTARY NOTATION				
17. COSATI CODES			18. SUBJECT TERMS (Continue on reverse if necessary and identify by block number)	
FIELD	GROUP	SUB-GROUP	TELEMETRY	
09	06		PULSE AMPLITUDE MODULATION	
			FREQUENCY MODULATION	
			PULSE CODE MODULATION	
			PHASE MODULATION	
			LINK ANALYSIS	
19. ABSTRACT (Continue on reverse if necessary and identify by block number)				
<p>The purpose of this handbook is to provide practical information about telemetry system engineering. This handbook is intended to be useful to both system designers and operators.</p> <p>This handbook is divided into five sections:</p> <ol style="list-style-type: none"> <li>1. Introduction,</li> <li>2. Telemetry terminology,</li> <li>3. Telemetry signals and noise,</li> <li>4. Telemetry transmitting system characterization,</li> <li>5. Telemetry receiving system characterization.</li> </ol>				
(Continued)				
20. DISTRIBUTION/AVAILABILITY OF ABSTRACT <input checked="" type="checkbox"/> UNCLASSIFIED/UNLIMITED <input type="checkbox"/> SAME AS RPT <input type="checkbox"/> DTIC USERS			21. ABSTRACT SECURITY CLASSIFICATION <b>UNCLASSIFIED</b>	
22a. NAME OF RESPONSIBLE INDIVIDUAL <b>EUGENE L. LAW</b>			22b. TELEPHONE (Include Area Code) <b>(805) 989-7046</b>	22c. OFFICE SYMBOL

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE

19. ABSTRACT (Concluded)

The subjects discussed include:

1. Parameter optimization for best data quality,
2. Radio frequency spectral occupancy,
3. Relationship of theory to "real-world" telemetry problems.

*signature*

*ALP*  
DISTRIBUTION AUTHORIZED TO U.S. GOVERNMENT AGENCIES AND  
THEIR CONTRACTORS ONLY; OPERATIONAL USE; SEPTEMBER 1967.  
OTHER REQUESTS FOR THIS DOCUMENT SHALL BE REFERRED TO THE  
COMMANDER, PACIFIC MISSILE TEST CENTER, PONT MUGU,  
CALIFORNIA 93042-5000, ATTN: CODE 1061. DESTRUCTION  
NOTICE: DESTROY BY ANY METHOD THAT WILL PREVENT  
DISCLOSURE OF CONTENTS OR RECONSTRUCTION OF THIS  
DOCUMENT.

UNCLASSIFIED

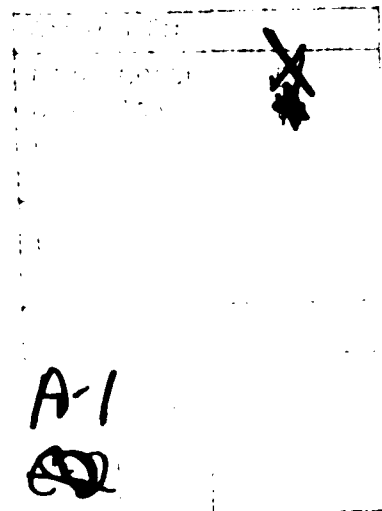
SECURITY CLASSIFICATION OF THIS PAGE

## PREFACE

For many years the Telemetry Group of the Range Commanders Council has recognized the continuing need for the development of practical telemetry applications guidelines. Guidelines oriented specifically to meet the demanding challenges facing telemetry systems planners, designers, and operators in their efforts to identify important systems parameters, solve system problems, and establish effective preventive maintenance procedures for the purpose of improving overall telemetry system performance. Recognizing that these needs must be met, the Telemetry Group of the Range Commanders Council initiated the development of this Telemetry Applications Handbook.

The demands placed upon systems planners, designers, and operators have changed significantly in recent years due to the increasingly complex requirements to monitor the activities of rapidly advancing space, air, ground, and ocean vehicles. State-of-the-art developments in the field of electronics have provided the means through which systems have kept pace with technological changes. Although many texts have been prepared and published in the field of telemetry, none are directly oriented toward practical application. Supportive practical information which provides the necessary operational tools has not kept pace with the demands placed upon telemetry systems personnel. Therefore, the major goal of the Telemetry Applications Handbook is to provide a practical application baseline that will have the effect of improving overall telemetry system performance. The guidelines provided will become the tools for telemetry systems personnel to achieve the intended goals of improved performance and compatibility.

Since the handbook is of significant importance to the personnel involved with the design, operation, and maintenance of telemetry systems, a great deal of concern is given to format, content, and level of text information. The final document is the result of Telemetry Group Committee reviews, inputs received through a telemetry oriented questionnaire/survey, and extensive laboratory testing. Text material follows system signal progression, that is, from source signal through the system to recovery of the source signal. In general, the handbook includes information on signal and noise considerations, transmission requirements, and reception requirements. Each of these general categories is further expanded by related illustrations such as systems block diagrams, graphs, photos, etc.



### **ACKNOWLEDGEMENT**

The authors are grateful for the patience and technical contributions of the Telemetry Group members who have been involved in the reviews of this handbook.

## TELEMETRY APPLICATIONS HANDBOOK

### TABLE of CONTENTS

	Page
1.0 INTRODUCTION	1.1- 1
1.1 Telemetry Applications Handbook	1.1- 1
1.2 Telemetry Systems	1.2- 1
2.0 TELEMETRY TERMINOLOGY	2.0- 1
2.1 Glossary of Terms	2.1- 1
2.2 Acronyms and Abbreviations	2.2- 1
3.0 TELEMETRY SIGNALS AND NOISE	3.0- 1
3.0.1 NRZ PCM/FM Summary	3.0- 2
3.0.2 Biphase PCM/FM Summary	3.0- 3
3.0.3 NRZ PCM/PM Summary	3.0- 4
3.0.4 Biphase PCM/PM Summary	3.0- 5
3.1 NRZ-PCM/FM	3.1- 1
3.1.1 Introduction	3.1- 1
3.1.2 Selection of Peak Deviation	3.1- 3
3.1.3 Selection of Premodulation Filter	3.1- 8
3.1.4 DC Component and AC Coupling	3.1- 8
3.1.5 Selection of Receiver IF Bandwidth	3.1-11
3.1.6 Selection of Demodulator Video Bandwidth	3.1-14
3.1.7 Selection of PCM Bit Synchronizer Bit Detector	3.1-14
3.1.8 RF Spectra	3.1-21
3.2 Biphase PCM/FM	3.2- 1
3.2.1 Introduction	3.2- 1
3.2.2 Selection of Peak Deviation	3.2- 1
3.2.3 Selection of Premodulation Filter	3.2- 5
3.2.4 Selection of Receiver IF Bandwidth	3.2- 5
3.2.5 Selection of Demodulator Video Bandwidth	3.2- 5
3.2.6 Selection of PCM Bit Synchronizer Bit Detector	3.2- 5
3.2.7 RF Spectra	3.2- 5
3.3 NRZ-PCM/PM	3.3- 1
3.3.1 Introduction	3.3- 1
3.3.2 Selection of Peak Deviation	3.3- 1
3.3.3 Selection of Premodulation Filter	3.3- 7
3.3.4 Selection of Receiver IF Bandwidth	3.3- 8
3.3.5 Selection of Demodulator Loop Bandwidth	3.3- 8
3.3.6 Selection of Demodulator Video Bandwidth	3.3- 8
3.3.7 Selection of PCM Bit Synchronizer Bit Detector	3.3-12
3.3.8 RF Spectra and Carrier Level	3.3-12

## TABLE of CONTENTS (Continued)

	Page
3.4 Biphase PCM/PM	3.4- 1
3.4.1 Introduction	3.4- 1
3.4.2 Selection of Peak Deviation	3.4- 3
3.4.3 Selection of Premodulation Filter	3.4- 3
3.4.4 Selection of Receiver IF Bandwidth	3.4-10
3.4.5 Selection of Demodulator Loop Bandwidth	3.4-10
3.4.6 RF Spectra	3.4-10
3.5 Phase Shift Keying	3.5- 1
3.6 NRZ-PAM/FM	3.6- 1
3.6.1 Introduction	3.6- 1
3.6.2 RF Deviation	3.6- 1
3.6.3 Premodulation Filter	3.6- 4
3.6.4 SNR at Output of NRZ PAM Decommutator	3.6- 4
3.6.5 Other Sources of Error in PAM	3.6- 5
3.6.6 NRZ PAM/FM Receiver IF Filter	3.6-18
3.6.7 NRZ PAM/FM Receiver Video Filter	3.6-18
3.6.8 PAM Baseband Spectra	3.6-18
3.6.9 NRZ PAM/FM RF Spectra	3.6-20
3.7 FM/FM Telemetry	3.7- 1
3.7.1 Introduction	3.7- 1
3.7.2 FM/FM SNR	3.7- 1
3.7.3 Transmitter Deviation	3.7-19
3.7.4 Receiver IF Bandwidth	3.7-22
3.7.5 Effect of Adjacent Channel or Co-channel Interference on FM/FM Discriminator Output	3.7-22
3.7.6 Record Level for Tape Recorder	3.7-24
3.7.7 Effect of Tape Recorder Flutter and Speed Error on FM/FM Data Quality	3.7-24
3.7.8 Preemphasis	3.7-24
3.7.9 FM Spectrum With Single Sine Wave Modulation	3.7-32
3.7.10 RF Spectrum of an FM/FM Multiplex	3.7-37
3.7.11 Noise Power Ratio	3.7-42
3.8 Hybrid Systems	3.8- 1
3.9 Link Analysis	3.9- 1
3.9.1 Introduction	3.9- 1
3.9.2 Transmitting System	3.9- 5
3.9.3 Communication Channel Losses	3.9- 5
3.9.4 Receiving System	3.9- 7
3.9.5 Link Margin Calculation	3.9- 8
3.10 Relay Systems	3.10-1
3.10.1 Introduction	3.10-1
3.10.2 Translation Relay SNR Calculation	3.10-2
3.10.3 Demodulation/Remodulation Relay SNR Calculation	3.10-4
3.11 FM Demodulator Noise	3.11-1
3.12 References	3.12-1

## TABLE of CONTENTS (Continued)

	Page
4.0 TELEMETRY TRANSMITTING SYSTEM CHARACTERIZATION	4.0- 1
4.1 Introduction	4.1- 1
4.2 Transmitting System Selection Guidelines	4.2- 1
4.3 References	4.3- 1
5.0 TELEMETRY RECEIVING SYSTEM CHARACTERIZATION	5.0- 1
5.0.1 Gain/System Noise Temperature (G/T)	5.0- 1
5.0.2 Bit Error Rate Testing	5.0- 2
5.0.3 Noise Power Ratio Testing	5.0- 2
5.1 Antennas	5.1- 1
5.1.1 Gain	5.1- 1
5.1.2 Beamwidth	5.1- 1
5.1.3 Noise Temperature	5.1- 1
5.1.4 Polarization	5.1- 1
5.2 Preamplifiers, Downconverters, and Multicouplers	5.2- 1
5.2.1 Preamplifier	5.2- 1
5.2.2 Noise Figure/Noise Temperature	5.2- 1
5.2.3 Downconverter	5.2- 4
5.2.4 Multicoupler	5.2- 4
5.3 Telemetry Receivers and Diversity Combiners	5.3- 1
5.3.1 Introduction	5.3- 1
5.3.2 Receiver Noise Figure	5.3- 2
5.3.3 Receiver Local Oscillators	5.3- 2
5.3.4 Receiver IF and Video Filters	5.3- 2
5.3.5 AGC Time Constant	5.3- 2
5.3.6 Demodulator Loop Bandwidth (PM and PSK)	5.3- 4
5.3.7 Automatic Frequency Control (AFC)	5.3- 4
5.3.8 Predetection Carrier	5.3- 4
5.3.9 Pop Noise Symmetry	5.3- 4
5.3.10 Signal Strength	5.3- 4
5.3.11 Diversity Combining	5.3- 5
5.3.12 Diversity Combining of PCM/FM Signals	5.3- 9
5.3.13 Diversity Combining of PCM/PM Signals	5.3- 9
5.4 Magnetic Tape Recorder/Reproducers	5.4- 1
5.4.1 Introduction	5.4- 1
5.4.2 Head Segment Gap Azimuth	5.4- 3
5.4.3 Spacing Loss	5.4- 6
5.4.4 Reproduce Gap Loss	5.4- 7
5.4.5 Bias Recording	5.4- 7
5.4.6 Equalization	5.4- 7
5.4.7 Reproducer Output SNR	5.4- 16
5.4.8 Predetection Recording	5.4- 16
5.4.9 Serial High Density Digital Recording (HDDR)	5.4- 23
5.4.10 Randomizer for RNRZ-L	5.4- 28

## TABLE of CONTENTS (Concluded)

	Page
5.5 Data Synchronizers and Discriminators	5.5- 1
5.6 Receiving System Parameter Selection Guidelines	5.6- 1
5.6.1 Introduction	5.6- 1
5.6.2 Receiver IF Bandwidth	5.6- 1
5.6.3 Receiver Oscillator Type	5.6- 2
5.6.4 Receiver AGC Time Constant	5.6- 2
5.6.5 Receiver Video Bandwidth and Coupling	5.6- 2
5.6.7 PM and PSK Demodulator Loop Bandwidth	5.6- 2
5.6.8 Predetection or Postdetection Combining	5.6- 2
5.6.9 Predetection Carrier Frequency	5.6- 2
5.6.10 Recording Method	5.6- 3
5.6.11 Tape Speed	5.6- 3
5.6.12 Bit Synchronizer Loop Bandwidth and Bit Detector Type	5.6- 3
5.7 Data Quality Monitoring	5.7- 1
5.8 References	5.8- 1
Index	I- 1



UNCLASSIFIED

TP000044  
September 1987

PACIFIC MISSILE TEST CENTER  
Point Mugu, California 93042-5000

TELEMETRY APPLICATIONS HANDBOOK

By  
EUGENE L. LAW  
and  
DONALD R. HUST

SUMMARY

The purpose of this handbook is to provide practical information about telemetry system engineering. This handbook is intended to be useful to both system designers and operators.

This handbook is divided into five sections:

1. Introduction
2. Telemetry terminology
3. Telemetry signals and noise
4. Telemetry transmitting system characterization
5. Telemetry receiving system characterization.

The subjects discussed include:

1. Parameter optimization for best data quality
2. Radio frequency spectral occupancy
3. Relationship of theory to "real-world" telemetry problems.

DISTRIBUTION AUTHORIZED TO U.S. GOVERNMENT AGENCIES AND THEIR CONTRACTORS ONLY; OPERATIONAL USE; SEPTEMBER 1987. OTHER REQUESTS FOR THIS DOCUMENT SHALL BE REFERRED TO THE COMMANDER, PACIFIC MISSILE TEST CENTER, POINT MUGU, CALIFORNIA, 93042-5000, ATTN: CODE 1061. DESTRUCTION NOTICE--DESTROY BY ANY METHOD THAT WILL PREVENT DISCLOSURE OF CONTENTS OR RECONSTRUCTION OF THIS DOCUMENT.

UNCLASSIFIED

## 1.0 INTRODUCTION

### 1.1 TELEMETRY APPLICATIONS HANDBOOK

The Telemetry Applications Handbook is a handbook of practical application guidelines whose purpose is to provide information which will lead to improvement in overall telemetry system performance and compatibility. The text has been prepared under the direction of the Telemetry Group of the Range Commanders Council (TG-RCC) to fill the gap between telemetry theory and application. The entire text is designed for use by telemetry system planners, designers, and operators. The handbook is published as a companion to the TG-RCC documents 106 (Telemetry Standards) and 118 (Test Methods for Telemetry Systems and Subsystems).

The information in the handbook is presented in the order of signal flow through a telemetry system. That is, the discussions begin at the origin of the source signals and proceed through the system to the receiving subsystem output, where the source signals are recovered. The text of the handbook is divided into the following major sections: Telemetry Signals and Noise, Telemetry Transmitting System Characterization, and Telemetry Receiving System Characterization. The discussions in each of these sections provide information on system design, problem prevention, problem recognition (existing and potential), problem isolation techniques, determination of the origin of problems, and approaches to be used in finding solutions to problems. Guidance is provided to assist in identifying important systems characteristics and to establish effective preventive maintenance procedures. Support to each of the topics discussed is provided through the liberal use of signal and system illustrations, graphs, photographs, etc.

The Telemetry Signals and Noise section includes discussions on data quality, baseband and radio frequency (RF) spectrums, and bandwidth requirements for the transmission and reception of source signals. The most desirable conditions exist when the source signals are processed through the telemetry system with little or no degradation. However, in practice this is seldom achieved, as many factors in the telemetry link may cause changes in the source signals, resulting in reduced data quality. A few of the major factors contributing to degradation of data quality include: noise, excessive filtering, improper deviation, system nonlinearities, and improper choice of modulation format or code. Careful attention to telemetry system design is the most effective means for minimizing degradation of source signal quality.

The discussion of baseband and RF signals is concerned with the design considerations that must be given to these signals within the telemetry system. Baseband refers to the band of frequencies occupied by the information signals before they are used to modulate the RF carrier. The usual distinction made between the baseband and RF signal frequencies is that the baseband signals range over significantly lower frequencies than the RF signals. The detailed discussions include considerations of the effects introduced by deviation of the carrier signals; effects due to filtering of the conditioned information signals, and bandwidths required to correctly process these signals.

Bandwidth requirements are a major concern in maintaining the quality of the telemetry data. The information presented includes discussions of the effects of over and under use of system bandwidths and also presents considerations involved in selection of system bandwidths for the optimum transmission and reception of telemetry data and tradeoffs which can be made.

The subsection on Link Analysis presents discussions on a number of diverse topics including antenna properties, propagation loss, channel effects, noise figure, signal diversity characteristics, and relay systems. It is obvious that this list of topics includes controllable and noncontrollable performance characteristics. Controllable system characteristics, including those of the transmitting and receiving antennas and relay systems, are discussed in terms of performance requirements needed to optimize the transmission and reception of data. Noncontrollable items are discussed in terms of the effects they may produce in the received data. Relay systems are included here because the placement of such a system is of necessity between the transmission and reception antennas.

Up to this point in the discussions the material presented has been concerned with signal quality, quantity, and through necessity, some methodology. The next section is concerned with the characterization of telemetry transmitting systems. Emphasis is placed on the selection of those parameters necessary to assemble a telemetry system, through the transmitting subsystem. After discussing the signal and bandwidth requirements, it is essential to consider what is required in interfacing signals with the conditioning and transmitting portions of the system. The discussion focuses on the requirements placed upon system elements including transducers, signal conditioning, signal sampling and digitizing, data multiplexing, data formatting and coding, premodulation filtering, RF modulation, and antennas, and the appropriate methods of interfacing signals and systems. The information presented starts at the origin of the measured quantity and carries on through the antenna of the transmitting system.

The section on Telemetry Receiving System Characterization begins with the signal at the receiving antenna, follows through the entire receiving process and ends prior to data display. System front-end characteristic discussions include the gain and beamwidth of the receiving antenna, and the noise figure, gain, and linearity characteristics of the preamplifiers and multicouplers. Continuing on through the system, information is provided with respect to bandwidth requirements, recording methods such as post-detection and pre-detection, the measurement of system signal quality using bit error rate (BER) and noise power ratio (NPR) testing techniques. After having processed the received signal through the entire receiving system with minimum signal degradation, consideration must be given to the type of processed signal analysis and/or storage media to be used. In real-time data processing signals are displayed for immediate observation and analysis; in post flight (non-real-time) processing the signal of interest is stored and reviewed at a later time. The process of storing and recovering the stored data has been and is a subject of major concern to range operations.

Typically, range data is stored on magnetic tape and is, therefore, recorded and reproduced using a magnetic tape recorder/reproducer. The emphasis of these discussions is on the characteristics of the recorder/reproducer system, its maintenance and operation. Subjects discussed will also include recording modes, system speed controls, system adjustments, performance tests to determine quality of operation, methods for assuring optimum crossplay, and important magnetic tape characteristics.

Important consideration must be given to recovery of the original signal, whether or not the output of the receiver system is processed in real- or post-flight time. The remainder of the discussion in this section will therefore, relate the methods and characteristics of demodulation and synchronization used in the recovery of the source signals.

## 1.2 TELEMETRY SYSTEMS

The field of telemetry has developed from the need to transmit information from one location to another; due primarily to inaccessibility of the source to be monitored directly. Its principle objective is to accurately transmit information between distant or remote locations.

The following discussion is intended to provide a broad overview of telemetry systems and will include information on telemetry system structure. The main emphasis is placed upon the system functions and the design decisions to be made by the telemetry engineer/technician.

The reference point for these discussions is the definition of a telemetry system. A telemetry system (telemetering system) is an electrical/electronic system for measuring a source quantity, transmitting the measured source quantity to a distant and/or remote receiving station, and there, indicating or recording the measured source signal. Data analysis is considered a separate topic and therefore is not included as part of the Telemetry Handbook.

In general, a telemetry (telemetering) system can be divided into two major functional subsystems (see figures 1.2-1 and 1.2-2). The transmitting subsystem includes: a source section (transducers), a source-signal processing (including signal conditioning and multiplexing) section, and a transmitting section. The receiving subsystem includes: receiving antenna(s), preamplifier(s), receiver(s), magnetic recorder(s), demodulator(s), data synchronizer(s), and data processor(s) and display(s). Since each of these major components can significantly affect the quality of the information to be recovered at the receiving subsystem output, it is very important that the functions and signal characteristics of each component be clearly defined. It is extremely advantageous to have an understanding of the more important performance characteristics required of each component to assure that the quality of the information is not degraded as it is processed through the various stages of the entire telemetry system. Brief descriptions of the functional role of each component are provided in the following discussion; but performance characteristics will be discussed in detail only in the main body of the Telemetry Handbook.

The source information originates as a signal which is to be measured or monitored. This signal may be of any form, such as electrical, mechanical, thermal, acoustical, etc. Since the telemetry system is designed to process electrical signals, it is necessary to transform non-electrical signals through the use of a transformation or conversion device known as a transducer. A transducer is defined to be "a device by means of which energy may flow from one or more transmission systems to one or more other transmission systems." That is, the non-electrical energy of, say, a vibration on a metallic surface is converted through the use of a mechanical-to-electrical transducer whose output electrical signal becomes the input to the signal conditioning subsystem. Very simply stated, a transducer is an energy form converter. Since the design and application of transducers is beyond the scope of this discussion, it is sufficient to state that the input signal is derived from a transducer that is incorporated to transform the signal to be monitored into an electrical signal. The output signal of the transducer, although electrical in nature, may exhibit a wide range of signal characteristics in amplitude, frequency, and/or phase. These signals must be properly interfaced to the subsequent sections of the telemetry system. Interface conditioning (signal conditioning) of these signals is normally done in the signal processing section of the telemetering system.

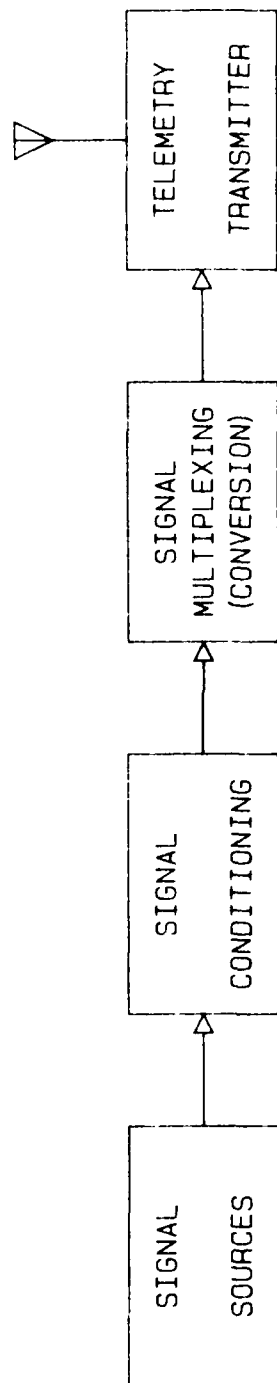


Figure 1.2-1. Telemetry Transmitting System.

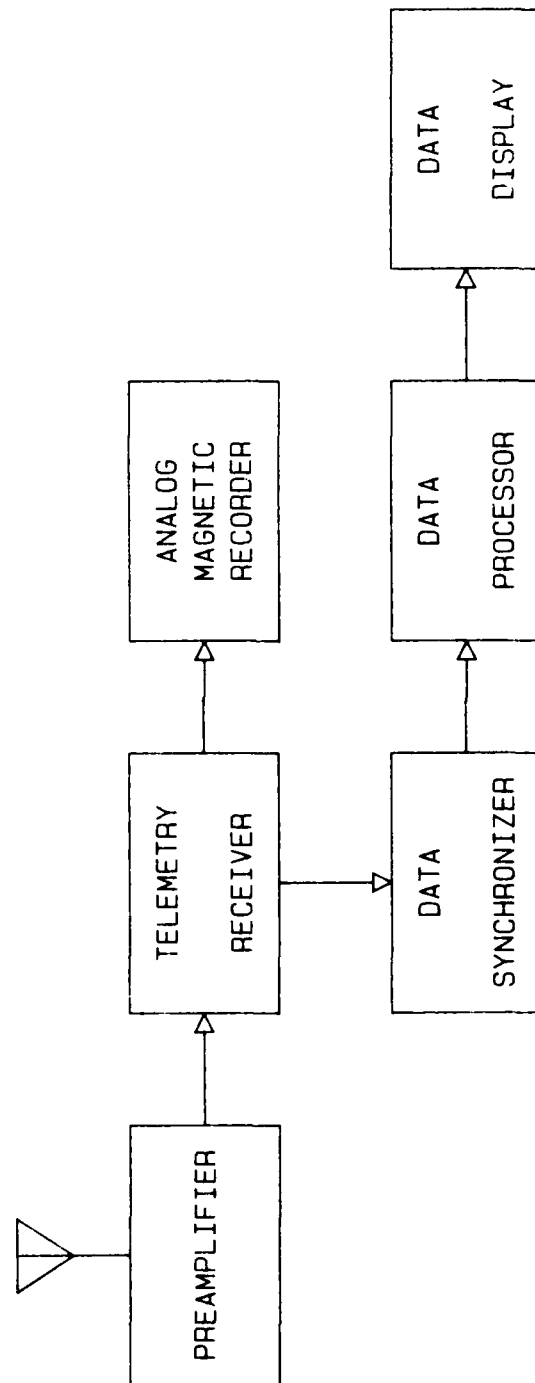


Figure 1.2-2. Telemetry Receiving System.

Signal conditioning in the broad sense implies a wide range of conditioning techniques from relatively simple to extremely complex, depending on the particular telemetry system requirement and application. The principal objective of signal conditioning is to provide control of signal characteristics (amplitude, offset, and frequency) for correct interface and compatibility with follow-on circuitry and assure to the greatest extent possible that the integrity and quality of the source signal will be maintained through the transmission and reception process. The most general type of signal conditioning involves the conversion of signal amplitude (gain and offset), frequency, and phase to signals which will interface with follow-on circuitry in the telemetry system. This conversion may be as simple as providing a resistive voltage divider network to establish the signal offset, amplitude, and impedance match to subsequent stages in the circuitry of the system. Most signal conditioners consist of resistors, capacitors and operational amplifiers. However, more complex conditioning techniques are sometimes needed for special applications. Signal conditioning techniques employed to meet these more complex applications include: special filtering techniques to limit the spectral components in the signals to be processed; phase, frequency, or amplitude detection; digital-to-analog conversion; nonlinear processing; etc.

The discussion up to this point implies that a telemetry system is used to transmit only a single signal. This is far from reality. A practical telemetry system must often transmit many different signals through a single channel or RF link. To accomplish this task, signal multiplexing is incorporated in the signal processing section of the telemetry system. Generally, signal multiplexing takes one of two forms; frequency-division multiplexing (FDM) or time-division multiplexing (TDM). In frequency-division multiplexing, two or more source signals are transmitted over a single channel by dividing the available baseband frequency space into several non-overlapping channels. The source signals are used to frequency modulate subcarrier oscillators (SCOs) whose output frequencies are contained within the baseband channel. The terms subcarrier oscillator and voltage controlled oscillator (VCO) are sometimes used interchangeably. The signals are recovered through the use of frequency discriminators. Time-division multiplexing is a method for transmitting two or more signals over a common channel by dividing the channel into time intervals so that the source signals may be sampled and time-sequence-multiplexed to form a composite signal train. Signals are recovered through the use of a demultiplexer which sorts out the time spaces so that the original sampled signals may be reassembled.

At this point in the discussion, a short recapitulation may be useful. The source information, whether it be a single signal or many signals, has been produced by a transducer, or other information source, conditioned in the signal conditioning network to meet interface requirements, may have been modified through analog-to-digital or digital-to-analog conversions, and combined through the use of FDM and/or TDM techniques. The resulting multiplexed signal is much more complex than the output from any one of the sources. This complex signal, representing the information from all the transducers, must now be transmitted to the receiving section of the telemetering system.

The design of the transmitting section must be carefully considered as it provides the functions to modulate the RF carrier signal, amplify the modulated carrier signal, interface the transmitter output to the transmitting antenna, and direct the transmitted RF signal in the desired direction. In order to simplify the introductory discussion of a telemetry system, the transmitter and transmitting antenna will be considered as a single section. The purpose of this section is to provide the means by which the composite information signal may be sent to the receiving location for detection and processing.

Several very important factors must be considered in the design of the transmitting section; they include RF signal stability requirements, RF carrier modulation (deviation) requirements, transmission bandwidth requirements and/or restrictions, the type of modulation employed, RF signal power requirements, and the pattern and polarization of the transmitting antenna. These factors directly impact the receiving section performance characteristics required to accurately receive and demodulate the transmitted signal. Therefore, the characteristics of the receiving and transmitting systems must be considered together to derive the optimum design for any system.

The RF carrier deviation, the baseband bandwidth, and the modulation technique determine the RF bandwidth of the transmitted signal. The RF bandwidth is important to the conservation of spectrum space and to the processing functions of the receiving system. The receiving system must be properly configured to process the received signal and minimize degradation due to the effect of filtering and noise.

The design of the receiving system must be compatible with the particular type of modulation employed in the transmitter to deviate the RF carrier signal. Typical modulation methods include FM (frequency modulation) and PM (phase modulation) techniques. Equally important to the transmission/reception process are the transmitted RF power, the gain of the transmitting and receiving antennas, and the noise temperature of the receiving system. Power and gain are very important factors in determining the signal-to-noise ratio of the signal to be processed by the receiving system. The polarization of the receiving antenna must be compatible with that of the transmitting antenna for optimum transfer of energy between the two antenna systems and provide for the least amount of RF signal loss and subsequent degradation of the signal-to-noise ratio.

The final step involved in successful recovery of the original source information signals depends upon the characteristics of the receiving section. For the purpose of these discussions the receiving section will include: receiving antenna(s), telemetry receiver(s), demodulator(s), magnetic tape recorder(s), and other necessary equipment.



## 2.0 TELEMETRY TERMINOLOGY

This section is divided into two parts:

A glossary of terms (2.1) that are frequently used in the field of telemetry.

A list of telemetry related acronyms and abbreviations (2.2).

## 2.1 GLOSSARY OF TERMS

- A -

**ACQUISITION:** Process of acquiring synchronization; can be clock synchronization or receiving antenna pointing toward the transmitting antenna.

**ACQUISITION TIME:** The time interval required to establish clock synchronization or antenna track.

**ALIASING EFFECT:** Apparent downward shift in frequency of components which are higher than one-half the sampling frequency resulting from a sampling rate which is too low in frequency.

**AMPLIFIER:** An electronic device used to increase the amplitude of electronic signals.

**AMPLIFIER, LOW NOISE:** An amplifier whose noise temperature is low.

**AMPLITUDE EQUALIZATION:** The process of reducing frequency response distortion by the introduction of networks to compensate for the differences in attenuation at various frequencies.

**ANTENNA PATTERN (RADIATION PATTERN):** A graphical representation of the radiation properties of the antenna as a function of space coordinates. *Radiation properties* include power, phase, and polarization. In the usual case the radiation pattern is determined in the far field region and is represented as a function of directional coordinates.

**ANTIPODAL:** Diametrically opposite, exact opposites; e.g. the NRZ-L symbols for "one" and "zero" are referred to as antipodal symbols.

**ATTENUATION, ATMOSPHERIC:** The attenuation of a radio signal as it passes through the atmosphere due to particles in the atmosphere, e.g., raindrops, water vapor, and other gases.

**ATTENUATION, FLAME:** The attenuation of a radio signal as it passes through the ionized gas and particles of the exhaust from a rocket motor.

**AZIMUTH ALIGNMENT (FOR RECORDER/REPRODUCER HEADS):** Alignment of the recording and reproducing head gaps to provide system to system compatibility and to produce the optimum output. Alignment considerations must include the record head gap, the reproduce head gap, and the dynamic path of the magnetic tape.

**BANDWIDTH:** A range of frequencies that conform to a specified standard, usually  $\pm 3$  dB of the amplitude of the reference frequency. The information capacity of a channel.

**BANDWIDTH (CONTINUOUS FREQUENCY BAND):** The difference between the limiting frequencies. The range of frequencies within which performance, with respect to some characteristic, falls within specific limits.

**BANDWIDTH, NECESSARY:** The International Telecommunication Union (ITU) and the National Telecommunications and Information Administration (NTIA) have defined necessary bandwidth as follows: "For a given class of emission, the width of the frequency band which is just sufficient to ensure the transmission of information at the rate and with the quality required under specified conditions."

**BANDWIDTH, OCCUPIED:** The ITU and NTIA have defined occupied bandwidth as follows: "The width of a frequency band such that below the lower, and above the upper, frequency limits, the mean powers emitted are each equal to a specified percentage of the total mean power of a given emission." This percentage is frequently specified as 0.5% and the resulting bandwidth referred to as the 99% power bandwidth. The Range Commanders Council has an alternate definition of occupied bandwidth that includes all spectral components that are larger than the larger of -60 dBc or -25 dBm.

**BASEBAND (CARRIER OR SUBCARRIER TRANSMISSION SYSTEM):** The band of frequencies occupied by the signal before it modulates the carrier (or subcarrier) frequency to form the transmitted signal. The signal in baseband ranges over a distinctly lower frequency than the carrier frequency, and may include a direct current (DC), component.

**BASELINE RESTORATION:** Recovery of the DC baseline reference of a signal that has been modulated by the effects of long strings of "ones" or "zeros."

**BEAMWIDTH (ANTENNA):** Half power beamwidth plane containing the direction of the maximum value of the beam. The angle between the two directions in which the radiation intensity is one-half the maximum value of the beam.

**BIAS SIGNAL, HIGH FREQUENCY:** A high frequency (usually at least three times the maximum signal to be recorded) sinusoidal signal linearly added to the analog data signal to linearize the magnetic recording/reproducing characteristic.

**BI-LEVEL DIGITAL SIGNAL:** A digital signal which is comprised of only two levels.

**BI-PHASE LEVEL (BI $\phi$ -L):** A method of representing digital data where a level change occurs at the center of every bit period. A "one" is represented by a "high" level with a mid-bit transition to the "low" level. A "zero" is represented by a "low" level with a mid-bit transition to the "high" level.

- B -

**BINARY CODE:** A method of representing numbers using two states such as; on or off, high level or low level, etc.

**BIT:** An abbreviation for binary digit.

**BIT ERROR:** A bit error has occurred when the expected bit value is not present; e.g. a "zero" occurring when a "one" is expected or a "one" occurring when a "zero" is expected.

**BIT ERROR PROBABILITY (BEP):** The ratio of the number of bits in error to the number of bits transmitted during a given time interval.

**BIT ERROR RATE (BER):** The number of bits in error during a given time interval or a given number of bits.

**BIT PACKING DENSITY (LINEAR):** The number of bits of useful information contained within a given linear dimension, usually expressed in bits per inch or millimeter.

**BIT RATE:** The speed at which bits are transmitted, usually expressed in bits per second (b/s or bps).

**BIT SLIP:** The increase or decrease in detected bit rate by one or more bits with respect to the actual bit rate.

**BIT SLIPPAGE PROBABILITY (BSP):** The ratio of the number of bits gained or lost (slipped) to the number of bits transmitted during a given interval of time.

**BIT SLIPPAGE RATE:** The number of bits gained or lost (slipped) during a given time interval or given number of bits.

**BIT STREAM:** A continuous series of bits transmitted over a channel.

**BIT SYNCHRONIZER:** An electronic device that produces a reconstructed version of the transmitted clock and bit stream from an input bit stream that may have been contaminated by noise and distortion.

**BIT SYNCHRONIZATION:** In step or in phase as applied to a digital sequence; e.g., a bit sequence in step/in phase with its source clock.

**BURST:** A continuous group of events occurring together in time. An analog signal sequence or pulse train that starts at a prescribed time and continues for a specified duration or number of cycles.

**BURST ERROR:** A series of closely spaced errors occurring in a transmission channel caused by a common event.

**BYTE:** A sequence of adjacent binary bits of specified length; e.g., 4, 6, or 8 bits in length. A byte is usually defined to be 8 bits long.

**CARRIER:** An analog signal of constant amplitude and frequency that is modulated by information signals to produce a signal suitable for transmission.

**CARRIER-TO-NOISE RATIO (CNR):** The ratio of carrier to noise after bandlimiting but before any nonlinear process such as amplitude limiting.

**CENTER FREQUENCY:** The average frequency of a signal when modulated by a symmetrical signal.

**CHANNEL:** The path through which signals flow.

**CLOCK:** A signal waveform used to synchronize digital circuits.

**CLOCK (RECONSTRUCTED):** A clock signal which is recovered from the data at the data processing site.

**CLOCK SLIP:** An increase or decrease of more than 180 degrees of the reconstructed clock relative to a perfectly recovered clock.

**CLOCK SYNCHRONIZATION:** The process of aligning a clock at a remote site to a clock at the originating site.

**CLOCKING:** Communication signal time synchronization information.

**CODING:** Method by which digital data is converted, following a prescribed set of rules.

**COMMUTATION:** Sequential sampling, on a repetitive basis, of multiple data sources for transmitting and/or recording on a single channel basis.

**COMMUTATOR:** A device used to accomplish time-division multiplexing by repetitive sequential switching techniques.

**COMPRESSION POINT, 1 dB:** The point at which the gain of an amplifier is reduced by 1 dB with respect to its small signal gain.

**CONSTANT BANDWIDTH:** A frequency division multiplexing system in which each channel occupies the same bandwidth regardless of its center frequency. The amount of deviation is held within an allocated bandwidth and is not determined as a percentage of the center frequency as in a proportional bandwidth system.

- C -

**CORRELATION DETECTION:** A method of detection in which a signal is compared, point-to-point, with an internally generated reference. The output of such a detector is a measure of the degree of similarity of the input and reference signals. The reference signal is constructed in such a way that it is at all times a prediction, or best guess, of what the input signal should be at that time.

**CROSS MODULATION:** A type of intermodulation of a desired carrier by undesired carriers.

**CROSSPLAY:** Reproducing a previously recorded tape on a system other than that used to record the tape.

**CROSSTALK:** Interference in a given transmitting or recording channel which has its origin in another channel. Undesired signal energy appearing in one signal path as a result of coupling from other signal paths.

**CUTOFF FREQUENCY:** The frequency that marks the edge of the passband of a filter and the beginning of the transition to the stopband. It is usually defined to be the frequency at which the signal is attenuated by 3 dB relative to the response at a reference frequency.

- D -

**DATA AZIMUTH (DYNAMIC):** The departure from the nominal head segment gap azimuth angles (static) because of the dynamic interface between the heads and the moving tape.

**DATA BANDWIDTH:** The difference between the highest and lowest frequency of the data to be transmitted; usually defined by the -3 dB points.

**DATA CONVERSION:** The process of changing data from one form of representation to another.

**DATA MULTIPLEXING:** The process of combining two or more signals into a single composite signal. The two basic methods of multiplexing involve the separation of signals by time division and frequency division.

**DATA QUALITY:** A measure of "goodness" of data. The measure of goodness can be bit error rate, signal-to-noise ratio, maximum (or rms) error as a percentage of full scale, etc.

**DATA TRACK:** The recorder channel (track) on which data has been or is to be recorded.

**dB<sub>i</sub>:** Antenna gain in decibels referenced to the gain of an omnidirectional antenna with 100% efficiency.

**dBm:** Power level in decibels referenced to a level of one milliwatt (0.001 watt), i.e.,  $\text{dBm} = 10 \log_{10} (P / 0.001)$  where P is in watts.

**dBv:** Voltage level in decibels referenced to a level of one volt, i.e.,  $\text{dBv} = 20 \log_{10} (V / 1)$  where V is in volts.

**DECIBEL, power (dB):** Ten times the log of the ratio of two power values, i.e.,  $\text{dB} = 10 \log_{10} (P_1 / P_2)$

**DECIBEL, voltage (dB):** Twenty times the log of the ratio of two voltage values, i.e.,  $\text{dB} = 20 \log_{10} (V_1 / V_2)$

**DELAY DISTORTION (PHASE DISTORTION):** Distortion occurring in communication channels due to variations in signal propagation speeds at different frequencies. Measured in time relative to a reference frequency.

**DELAY MODULATION (DM-M):** Method for representing digital data, where a "one" is represented by a mid-bit transition and a "zero" is represented by a transition at the end of the bit when the next bit is a "zero" and no transition when the next bit is a "one"

**DEMODULATOR:** A device to effect the process of demodulation. See also, demodulation

**DEMODULATION:** The process of recovery or extraction of the original information signal from the modulated RF signal.

- D -

**DERANDOMIZER:** A device which performs the inverse operation of a randomizer; recovers data which was previously randomized.

**DETECTION:** Determination of the presence of a signal. The process by which a signal corresponding to the modulating signal is obtained from a modulated carrier.

**DETECTOR, BALANCED:** Demodulator for frequency modulation systems. In one form, the output consists of the rectified difference of the two voltages produced across two resonant circuits, one circuit being tuned slightly above the carrier frequency and the other slightly below.

**DETECTION, LINEAR:** The form of detection in which the output voltage is proportional to the voltage of the input wave.

**DEVIATION:** The algebraic difference between a given value and its corresponding central reference value.

**DEVIATION DISTORTION:** Distortion in an FM receiver caused by inadequate bandwidth, amplitude modulation rejection, or discriminator linearity.

**DEVIATION, PEAK FREQUENCY:** The maximum difference between the instantaneous frequency of the modulated signal and the reference carrier frequency.

**DEVIATION, PEAK PHASE:** The maximum difference between the instantaneous phase of the modulated signal and the reference carrier signal.

**DEVIATION RATIO:** The ratio of one-half the defined channel peak-to-peak deviation to the discriminator low-pass output filter bandwidth.

**DEVIATION, RESIDUAL:** Apparent modulation due to noise in the transmitter also known as incidental frequency modulation.

**DIGITAL-TO-ANALOG CONVERTER (DAC):** A device that converts an input binary code into an analog voltage.

**DIGITIZE:** To assign digital numbers to characters and words according to fixed rules of ordering. To convert from analog to digital form.

**DIRECT RECORDING with AC BIAS:** A magnetic recording technique employing a high-frequency bias signal which is linearly added to the data signal. The composite signal is then used to drive the record-head segment.

**DISCRIMINATOR, FM:** An electronic device which operates as a frequency to voltage converter.

**DIVERSITY COMBINER:** An electronic device which sums the signals from two or more sources.



- D -

**DIVERSITY RECEPTION:** A method of radio reception whereby, in order to minimize the effects of fading, a resultant signal is obtained by combination and/or selection of two or more sources of received-signal energy which carry the same modulation or intelligence, but which may differ in strength or signal-to-noise ratio. Diversity reception may employ frequency, polarization, time or space diversity.

**DOPPLER EFFECT:** A principle of physics that, as the distance between a source of constant frequency and an observer diminishes or increases, the received frequencies are greater or less.

**DOPPLER SHIFT:** The change in frequency of a system caused by the doppler effect.

**DOWN-CONVERTER:** An electronic device that translates a given frequency band to a frequency band with a lower center frequency.

**DRIFT:** A slow change in either absolute level or slope of an input-output characteristic.

**DROPOUT:** A momentary loss of signal in a transmission channel; usually RF or magnetic tape in telemetry applications.

**DUCTING (RF TRANSMISSION):** Confinement of electromagnetic wave propagation to a restricted atmospheric layer by steep gradients in the index of refraction with altitude.

**ENHANCED NON-RETURN-TO-ZERO LEVEL (ENRZ-L):** Method for representing digital data, trademark of the DATATAPE Division of the Kodak Corporation. The input data NRZ-L bits are collected into separate groups of seven bits, bits 2, 3, 6, and 7 are inverted, and an eighth bit is added to make the parity odd (odd number of ones).

**ENVELOPE DELAY:** A characteristic of communication channels where variations in signal delay with respect to frequency occur across the data channel bandwidth. See also, delay distortion and phase distortion.

**ERROR CORRECTION:** The process of correcting bits in error through the use of redundant data bits.

**ERROR DETECTION:** The process of detecting bit errors.

**ERROR MULTIPLICATION:** A process in which individual isolated input bit errors cause multiple output bit errors. The degree of multiplication of errors is characteristic of the coding system employed.

**EQUALIZATION:** A method used to compensate for amplitude and phase distortions occurring in a communication channel. Equalizers are designed to provide the inverse of the channel distortion so that the signal can be recovered in its original form. See also, distortion.

**EXCLUSIVE-OR GATE:** The exclusive-OR gate is defined as a two-input device whose output assumes the "one" state if one and only one input assumes the "one" state.

**EYE PATTERN:** The pattern that results, as displayed on an oscilloscope, from the superpositioning of "ones" and "zeros" in a digital data sequence, when the time base of the oscilloscope is synchronized to the bit rate clock.

**FILTER, BANDPASS:** A filter having a single transmission band extending from a frequency higher than zero to a frequency lower than infinity.

**FILTER, BANDSTOP:** A filter which passes frequencies from zero to a lower cutoff frequency and from a higher cutoff frequency to infinity. Signals at frequencies between the lower and higher cutoff are attenuated. This filter is also called a notch filter or a band-reject filter.

**FILTER, CONSTANT AMPLITUDE:** A filter which is designed to have a maximally flat amplitude response; a Butterworth filter.

**FILTER, CONSTANT DELAY:** A filter which is designed to have a maximally flat delay response; a Bessel filter.

**FILTER, HIGH-PASS:** A filter having a single transmission band extending from some cutoff frequency, not zero, up to infinite frequency.

**FILTER, LOW-PASS:** A filter having a single transmission band extending from zero to some cutoff frequency, not infinite.

**FLAME ATTENUATION:** The attenuation of a radio signal as it passes through the ionized gas and particles of the exhaust from a rocket motor.

**FLAWS, MAGNETIC TAPE:** Regions of a magnetic tape where the density of magnetic particles is much lower than the nominal value. Regions of a magnetic tape which have been physically damaged.

**FLUTTER:** The undesired frequency changes produced by speed variations of the magnetic tape during recording and reproduction.

**FLUX TRANSITION:** A 180° change in the flux pattern of a magnetic medium brought about by the reversal of the magnetic poles within the medium.

**FLUX TRANSITION DENSITY (LINEAR):** The number of flux reversals occurring during a given length of tape (linear dimension in inches or millimeters).

**FM DISCRIMINATOR:** An electronic device that acts like a frequency-to-voltage converter.

**FM/FM (FREQUENCY MODULATION/FREQUENCY MODULATION):** Frequency modulation of a carrier by subcarriers which are frequency modulated by information signals.

**FORMAT:** A predetermined arrangement of characters, fields, lines, punctuation, page numbers, etc.

**FRAME:** A set of digital data encompassed within a specified boundary; e.g., minor frame, major frame, data frame, etc. The boundary is marked by a frame synchronization word.

**FRAME FORMAT IDENTIFICATION:** A word which uniquely identifies which PCM format is currently being transmitted when more than one format is possible.

**FRAME OF DATA:** A sequence of data bits in which the position of each data bit can be identified by reference to the frame synchronization pattern.

**FREQUENCY DEVIATION:** In frequency modulation, the difference between the instantaneous frequency of the modulated wave and the unmodulated carrier frequency.

**FREQUENCY DEVIATION LIMIT:** The upper and lower frequency limits beyond which a subcarrier should not be deviated.

**FREQUENCY DIVERSITY:** That form of diversity that uses both transmission and reception at more than one frequency.

**FREQUENCY DIVISION MULTIPLEXING:** A multiplexing technique in which the channel bandwidth is divided into different frequency subchannels. Permits more than one signal source to share the same communication channel.

**FREQUENCY DIVISION MULTIPLEX:** A system for the transmission of information about two or more quantities (measurands) over a common channel by dividing the frequency band. Amplitude, frequency, or phase modulation of the subcarriers may be employed. A process or device in which each signal channel modulates a separate subcarrier, the subcarriers being spaced in frequency to avoid overlapping of the subcarrier sidebands.

**FREQUENCY MODULATION (FM):** A method for transmitting information where the amplitude of the information signal is used to vary the frequency of the carrier signal.

**FREQUENCY OFFSET:** A deviation from the reference frequency. May be static or dynamic; e.g., a varying offset or a fixed frequency offset, such as occurs when a DC voltage is applied to an FM carrier system.

**FREQUENCY RESPONSE:** A measure of how effectively a device passes the different frequencies applied to it.

**FREQUENCY SHIFT KEYING (FSK):** A form of frequency modulation in which the modulating signal shifts the carrier frequency between predetermined values, and the output signal has no phase discontinuity. Commonly, the instantaneous frequency is shifted between two discrete values, termed the Mark and Space frequencies.

- G -

**GAIN (AMPLITUDE):** An increase in signal amplitude, normally expressed in decibels (dB).

**GAP LENGTH (PHYSICAL):** The dimension between leading and trailing edges of a record or reproduce head-segment gap measured along a line perpendicular to the leading and trailing edges of the gap.

**GAUSSIAN NOISE:** Noise whose amplitude is characterized by the normal distribution.

**GROUND STATION:** A telemetry receiving, recording, processing and display system. This term is also used to refer to systems which contain a subset of the above functions.

**GROUP DELAY:** The derivative of radian phase with respect to radian frequency, often called envelope delay.

**G/T (RADIO ANTENNAS):** The ratio of the maximum power gain to the noise temperature (in degrees Kelvin) of an antenna and its associated receiving system.

**GUARD BAND:** The unused frequency spaces between subcarriers in FDM systems and between RF carriers; used to guard against interference.

- H -

**HARMONICS:** Frequencies that are multiples of a fundamental frequency. Odd harmonics are odd multiples of the fundamental frequency and even harmonics are even multiples of the fundamental frequency.

**HARMONIC DISTORTION:** The production of harmonic frequencies at the output of a nonlinear device when a sinusoidal signal is applied to the input.

**HARMONIC FREQUENCIES:** Frequencies that occur at multiples of the fundamental frequency.

**HEAD, MAGNETIC:** A device that records, reads or erases data on magnetic tape.

**HEAD SEGMENT:** A single transducer which either records a signal on tape or reproduces a signal previously recorded on tape.

**HIGH DENSITY DIGITAL RECORDING (HDDR):** Recording of digital data, on a magnetic recording medium, having a linear flux transition density in excess of 15,000 transitions per inch.

**HORIZONTALLY POLARIZED WAVE:** A linearly polarized wave whose electric field vector is horizontal with respect to the earth's surface.

**HYBRID MODULATION:** A combination of the modulation methods, PCM/FM, PCM/PM, FM/FM, etc., used to impress information on a carrier for transmission.

**HYSTERESIS (MAGNETIC):** The property of a magnetic material which causes the magnetic induction for a given magnetizing force to depend on the previous conditions of magnetization.

**HYSTERESIS LOSS (MAGNETIC):** The power lost in a magnetic material as a result of magnetic hysteresis.

- I J K L -

**INCIDENTAL FM:** The short term jitter or undesired FM deviation of a local oscillator. Also known as residual FM.

**INSERTION LOSS:** The decrease in power delivered to the load when a device is inserted between the source and load.

**INTERFERENCE (COUPLING):** Interference resulting from signals transferring (coupling) between circuits.

**INTERFERENCE (DATA TRANSMISSION):** Interference in a signal transmission path is either extraneous power which tends to interfere with the reception of the desired signals or the disturbance of signals which results.

**INTERMODULATION DISTORTION:** Distortion brought about by the interaction of two or more frequencies resulting in erroneous information signal transmission.

**INTERMEDIATE FREQUENCY (IF):** A frequency to which a signal is shifted locally as an intermediate step in transmission or reception.

**JITTER:** Information signal variations relative to a reference time position. Variations can be in time, frequency, and/or phase. These variations may result in erroneous detection of information signals; particularly pulse type systems. Frequency modulation of the bit rate or bit rate clock.

**JITTER RATE:** Rate or frequency at which the bit rate or bit rate clock is being modulated.

**KILOBITS PER INCH (kb/in):** Linear packing density expressed in thousands of bits per linear inch. Usually used in digital magnetic recording.

**L-BAND:** A term referring to the band of frequencies between 1000 and 2000 MHz. The telemetry portion of L-band extends from 1435 to 1540 MHz. The frequencies between 1700 and 1850 MHz are frequently referred to as upper L-band signals.

**LEFT-HAND POLARIZED WAVE:** An elliptically polarized electromagnetic wave in which the rotation of the electric field vector is counterclockwise when looking in the direction of propagation.

**LINEARITY:** The condition where in the change in the value of one quantity is directly proportional to the change in the value of another quantity. A relationship existing between two quantities such that the change in one quantity is exactly and directly (linearly) proportional to the change in the other quantity.

**LOCK:** The state of being synchronized in frequency, phase, or motion to another signal or object.

**MAJOR FRAME:** The data structure consisting of the smallest number of minor frames which includes at least one sample of each parameter in the format.

**MATCHED LOAD:** A device used to terminate a transmission line so that all of the incoming energy is absorbed.

**MAXIMAL LENGTH SEQUENCE:** A pseudo-random sequence of length  $2^N - 1$  generated by a shift register of length  $N$ .

**MILLER CODE:** See Delay Modulation.

**MILLER SQUARED ( $M^2$ ):** Method for representing digital data where the bit stream to be encoded is divided into data sequences of three types:

Type A: Any number of consecutive logic "ones."

Type B: Two logic "zeros" separated by either no logic "ones" or an odd number of "ones"; e.g., 00, 010, 01110.

Type C: A logic "zero" followed by an even number of logic "ones" and terminated by a "zero" not counted as part of the sequence; e.g., 011, 01111.

For types A and B, "ones" are coded with transitions in the middle of the bit and consecutive "zeros" have transitions between them; the same as for delay modulation. However, in type C sequences the transition in the middle of the final "one" is inhibited.

**MINIMUM TRANSITION DENSITY:** The minimum number of transitions for a given number of bits for any input bit sequence.

**MINOR FRAME:** The data structure in time sequence from the beginning of one minor frame synchronization pattern to the beginning of the next minor frame synchronization pattern.

**MODULATION INDEX:** The modulation index ( $\beta$ ) is equal to the peak phase deviation when a single sinusoid angle modulates the carrier:

$$\beta = \Delta\phi.$$

For frequency modulation the modulation index is often expressed as the ratio of the peak frequency deviation to the frequency of the modulating signal:

$$\beta = \Delta f / f_m$$

where  $\Delta f$  is the peak carrier frequency deviation and  $f_m$  is the modulation frequency.



- M -

MODULATOR: A device which causes some parameter of a carrier signal to vary in step with the modulating signal.

MULTICOUPLER: A device used to interface one antenna to several receivers with gain of one or larger.

MULTIPATH: The phenomenon where signals reach the receiving antenna by two or more separate paths. This can cause echoes or ghosting.

NOISE: Any unwanted disturbance or spurious signal which modifies the transmitting, indicating, or recording of the desired signal.

NOISE FIGURE: The ratio of total output noise power to output noise power due to noise present at the input of the device, when the input source is at a temperature of 290°K; usually expressed in dB.

NOISE, FLUCTUATION: Noise whose amplitude is completely random. The error in the output of a demodulator when the signal is larger than the noise.

NOISE, GAUSSIAN: Noise whose amplitude has a normal (Gaussian) distribution.

NOISE, IMPULSE: Noise generated in discrete energy bursts which has a characteristic wave shape of its own.

NOISE LOADING: The process of simulating the sum of many independent modulating signals through the use of one Gaussian noise signal.

NOISE LOADING TEST SET: An electronic device which generates and receives a Gaussian noise signal. It is used to measure the noise floor and intermodulation level of a transmission system.

NOISE, POP: The error in the demodulated output which occurs when the vector sum of the signal plus noise encircles the origin. The instantaneous noise amplitude has to be larger than the instantaneous signal amplitude for this to occur. This is also known as click noise.

NOISE, RANDOM: A signal whose instantaneous amplitude is determined at random and is therefore unpredictable. It contains no periodic frequency components and has a continuous frequency spectrum.

NOISE TEMPERATURE: The temperature of a passive system having an available noise power per unit bandwidth equal to that of the actual terminals. The noise temperature of a simple resistor is the actual temperature of the resistor, while the noise temperature of a diode may be many times the observed absolute temperature. The standard reference temperature  $T_0$  for noise measurements is 290 degrees Kelvin (K).

NOISE, WHITE: Noise whose power is distributed uniformly over all frequencies. Since ideal white noise is an impossibility, bandwidth restrictions must be applied.

- N -

**NOISE POWER RATIO (NPR):** The decibel ratio of the noise power with the baseband fully loaded to the noise power with the baseband fully loaded except for a narrow band around the measurement frequency. All noise powers are measured in a narrow band around the measurement frequency.

**NON-RETURN-TO-ZERO LEVEL (NRZ-L):** A binary method of representing digital data where a "one" is represented by one level and a "zero" is represented by the other level in a bi-level system. The level does not return to zero between the data pulses.

**NORMAL RECORD LEVEL:** The input level to an IRIG magnetic tape recorder which produces 1% third harmonic distortion with an input frequency equal to 10% of the upper bandedge frequency of the recorder/reproducer system.

- 0 -

ODD PARITY: Bit added to a binary code group which is used to make the number of "ones" or "zeros" in a group odd.

OVERHEAD BITS: Extra bits added to a digital sequence of data bits which are used to control and/or interpret system response. Also may be used for error detection and correction (EDAC).

**PACKING DENSITY, LINEAR:** The number of units of useful information contained within a given linear dimension, usually expressed in units per inch or millimeter; the number of binary digit magnetic pulses stored on a tape per linear inch, on a single track.

**PARALLEL HIGH DENSITY DIGITAL RECORDING (HDDR):** Method of recording a digital data sequence, where the data sequence is multiplexed onto more than one recording channel.

**PARITY BIT:** A bit added to a binary code group which is used to make the number of "ones" or "zeros" even or odd in that group.

**P-BAND:** The band of frequencies between 215 and 320 MHz used primarily as a common frequency band into which L-band and S-band telemetry signals are downconverted in some telemetry receiving stations. A portion of this band was used for telemetry transmission before 1970 (some programs continue to use this band on a waiver basis).

**PCM, PARALLEL:** A PCM technique in which pulses are transmitted simultaneously over parallel channels. The technique is often encountered in magnetic tape recording.

**PCM, SERIAL:** PCM transmission in which a single data channel is used and the pulse code signals are received in sequential order.

**PHASE DISTORTION (DELAY DISTORTION):** Distortion occurring in communication channels due to variations in signal propagation speeds at different frequencies. Measured in time relative to a reference frequency.

**PHASE EQUALIZATION:** The process of reducing phase distortion by the introduction of networks to compensate for the differences in delay at various frequencies.

**PHASE JITTER:** A dynamic variation of signal phase about some phase reference point.

**PHASE SHIFT KEYING (PSK):** Modulation technique where the modulated carrier is shifted either +90 degrees or -90 degrees relative to the reference carrier. This is usually accomplished by amplitude modulation of the carrier by  $\pm 1$ .

**POLARITY:** Having two opposite states such as positive and negative voltages or north and south poles.

**POLARIZATION DIVERSITY (RECEPTION):** That form of diversity reception that uses receiving antennas whose polarizations are mutually orthogonal (usually vertical and horizontal or left-hand circular and right-hand circular).

**PREAMPLIFIER:** An amplifier connected to a low level signal source to present suitable input and output impedances and provide gain so that the signal may be further processed without appreciable degradation in the signal to noise ratio.

**PREEMPHASIS:** A process in a system designed to emphasize the amplitude of some frequency components with respect to the amplitude of others in order to improve the signal-to-noise ratio or reduce distortion.

**PREMODULATION FILTERING:** The filtering of a signal prior to carrier modulation. The effect is to reduce the energy contained in the sidebands of the modulated carrier.

**PRINT-THROUGH (MAGNETIC TAPE):** The inadvertent magnetization of a layer of magnetic tape by an adjacent layer.

**PROPAGATION DELAY:** The necessary time required for a signal to be transmitted from one point to another.

**PROPAGATION LOSS (FREESPACE):** The loss of energy caused by the "spreading" of an electromagnetic wave as it travels through space. This loss (dB) can be calculated using:

$$20 \log_{10} (4\pi D/\lambda)$$

where:

$\lambda$  is the wavelength of the transmitted signal

D is the distance between the transmitter and receiver.

**PROPORTIONAL BANDWIDTH:** In a proportional bandwidth system the bandwidth of each channel is proportional to its center frequency. The maximum channel deviation is the product of the deviation value in percent divided by 100 and the center frequency of the channel.

**PSEUDO-RANDOM PATTERN:** A non-random pattern having statistical properties resembling a random pattern.

**PSEUDO-RANDOM SEQUENCE (PRS):** A non-random digital data sequence having statistical properties resembling a random digital sequence.

**PSEUDO-RANDOM SEQUENCE MODULATED NRZ-L:** Method for representing digital data where the NRZ-L bit sequence is modulo-2 summed with a pseudo-random sequence (PRS).

**PULSE AMPLITUDE MODULATION FREQUENCY MODULATION (PAM FM):**

Frequency modulation of a carrier by pulses, the amplitude of which contains the information to be transmitted.

**PULSE AVERAGING DEMODULATOR:** A type of FM demodulator in which a constant area pulse is generated for each zero crossing (can also use only positive or negative going zero crossings). The pulse train is low-pass filtered to produce a voltage which is proportional to the input frequency.

**PULSE CODE MODULATION (PCM):** Time division multiplexing (TDM) technique in which samples of data are represented in binary form by a group of discrete pulses.

**PULSE CODE MODULATION FREQUENCY MODULATION (PCM FM):** Frequency modulation of a carrier by pulse code modulation (PCM) information.

**PULSE CODE MODULATION/FREQUENCY MODULATION/FREQUENCY MODULATION (PCM/FM/FM):** Frequency modulation of a carrier by subcarriers which are frequency modulated by pulse code modulated information.

**PULSE CODE MODULATION/PHASE MODULATION (PCM/PM):** Phase modulation of a carrier by PCM information.

**RADIATION LOSS:** The part of the transmission loss due to radiation of radio frequency (RF) power.

**RANDOMIZE:** The process of converting a regular signal into a random signal.

**RANDOMIZED NON-RETURN-TO-ZERO:** A coding technique which is used to convert a bit stream into a bit stream with properties similar to random data. The IRIG randomizer adds (modulo 2) the input bit stream and the output bit stream delayed by 14 and 15 bits to produce the new output bit. This is frequently used for magnetic recording. The derandomizer is self-synchronizing.

**RECORD LEVEL, NORMAL:** The input level to an IRIG magnetic tape recorder which produces 1% third harmonic distortion with an input frequency equal to 10% of the upper bandedge frequency of the recorder/reproducer system.

**REGENERATED CLOCK:** Clock signal which has been generated or reconstructed from a digital data sequence. Reconstructed clock.

**RELAY:** A radio station (ground or airborne) used for the reception and retransmission of the signals from another radio station.

**RELAY POD:** An airborne receiver-transmitter combination which receives a signal, performs frequency translation, and retransmits it. Used in telemetry systems to relay signals from test vehicles to telemetry ground stations.

**REPEATER STATION:** An intermediate point in a transmission system where signals are received, amplified or reshaped, and retransmitted.

**RE-SYNCHRONIZATION:** Reestablish synchronous operation after having lost it, return it to being in step or in phase again.

**RETURN-TO-ZERO (RZ):** PCM code in which the encoded signal is at zero volts for the second half of each encoded bit.

**REVERSE PLAYBACK:** Reproduction of previously recorded data in a direction of tape travel which is the reverse of the direction in which the data was recorded.

**RF TRANSMISSION:** Transmission of data from one site to another through the use of a radio frequency carrier.

**RIGHT-HAND POLARIZED WAVE:** An elliptically polarized electromagnetic wave in which the rotation of the electric field vector is clockwise when looking in the direction of propagation.



**SAMPLED SIGNAL:** The sequence of values of a signal taken at discrete instants.

**SATURATION:** A condition where an increase in input signal amplitude does not produce an increase in output amplitude.

**S-BAND:** The range of frequencies between 2000 and 4000 MHz. The telemetry portions of this band are 2200 to 2300 MHz and 2310 to 2390 MHz.

**SECOND HARMONIC DISTORTION:** The ratio of the rms voltage at twice a fundamental frequency to the rms voltage at the fundamental frequency; usually expressed in % or dB.

**SENSITIVITY, RECEIVER:** That characteristic which determines the minimum strength of signal input capable of causing a desired value of signal output.

**SERVO-CONTROL (RECORDER/REPRODUCER):** The use of a reference signal to control the playback speed of the recorder/reproducer.

**SERIAL HIGH DENSITY DIGITAL RECORDING (HDDR):** Method of recording a digital data sequence, having a flux transition density in excess of 15,000 transitions per inch, where the data sequence is recorded on one recording channel.

**SHEDDING, TAPE:** Loss of magnetic coating from tape during operation on a tape transport.

**SHIFT REGISTER:** A logic network comprised of flip-flops connected in series; a binary state applied to the first register input can be shifted through the entire series of registers. Delay network.

**SIDE LOBE (ANTENNA PATTERN):** A radiation lobe in any direction other than that of the intended lobe. NOTE: When the intended lobe is not specified it shall be taken to be the major lobe.

**SIGNAL CONDITIONING:** Conditioning performed on an information signal to provide the performance characteristics required for certain types of data transmission.

**SIGNAL-TO-NOISE RATIO (SNR):** The relative power (or voltage) levels of signal and noise on a communications line; often expressed in dB. This term is usually expressed in terms of peak values in the case of impulse noise and in terms of root mean square (rms) values in the case of Gaussian noise.

**SIGNATURE RECORDING:** The recording of a signal which can be used to align the reproduce machine to the recording machine.

**SNR MARGIN:** Excess SNR over that required to achieve a given data quality for a given communication channel.

**SPACE DIVERSITY RECEPTION:** That form of diversity reception that uses receiving antennas placed in different locations.

**SPECTRUM:** The distribution of the amplitude, and sometimes phase, of the components of a signal as a function of frequency.

**STANDARD RECORD LEVEL (RECORDERS/REPRODUCERS):** The input level to an IRIG magnetic tape recorder which produces 1% third harmonic distortion with an input frequency equal to 10% of the upper bandedge frequency of the recorder/reproducer system.

**SUBCOMMUTATION:** The process of sampling a parameter at a submultiple of the minor frame rate.

**SUPERCOMMUTATION:** The process of sampling a parameter at a rate which is a multiple of the minor frame rate.

**SUPERHETERODYNE:** The process of translating a high frequency to a lower frequency.

**SYNCHRONIZATION:** The maintenance of one operation in step with another, also called sync.

**SYNCHRONIZATION WORD:** Overhead bits inserted into a frame of data which are used to demultiplex the data bits.

**SYNCHRONOUS:** In step or in phase as applied to two or more digital data sequences; e.g., two digital sequences which are synchronous with each other. A term in which the performance of a sequence of operations is controlled by equally spaced clock signals or pulses.

**TACH-SERVO (RECORDER/REPRODUCER):** The process of controlling the speed of the playback machine by its own internal speed reference.

**TAPE FLAWS:** Defects in the physical characteristics of a magnetic tape; e.g., irregularities in oxide coating, edge cutting, base material, and/or backing material. These irregularities may cause drop-outs, amplitude fluctuations, and poor tracking.

**TAPE SERVO (RECORDER/REPRODUCER):** The process of controlling the speed of the playback machine by synchronizing to a speed control signal recorded on the tape by the recording machine.

**TELEMETRY:** An electrical system for measuring a quantity, transmitting the result to a different location, and there, indicating or recording the quantity measured. Interpretation is not part of the telemetry process.

**THERMAL NOISE:** A type of electromagnetic noise produced in conductors or electronic circuitry whose power is proportional to temperature.

**THIRD HARMONIC DISTORTION:** The ratio of the rms voltage at three times the fundamental frequency to the rms voltage at the fundamental frequency; usually expressed in % or dB.

**THRESHOLD, FM:** The smallest value of SNR (or CNR) at the input to the demodulator such that a small change in input SNR produces an equal (or smaller) change in output SNR.

**TIME DIVERSITY RECEPTION:** That form of diversity reception that uses multiple transmissions which are separated in time.

**TIME DIVERSITY TRANSMISSION:** That form of diversity transmission that uses multiple transmissions separated in time.

**TIME DIVISION MULTIPLEXING (TDM):** A method for transmitting two or more quantities of source information (measurands) over a common channel by dividing available time intervals among the information signals to form a composite pulse train.

**TRACK (RECORDER):** One channel of a recorder/reproducer system.

**TRACKING ANTENNA:** An antenna which moves the position of its major lobe so that a selected moving target is contained within the major lobe.

**TRANSDUCER:** A device by means of which energy may flow from one or more transmission systems to one or more other transmission systems. The energy may be of any form, such as electrical, mechanical, or acoustical.

**TRANSITION DENSITY PROBABILITY:** The actual number of state changes from "high" to "low" or "low" to "high" divided by the number of bits during a given time interval.

- U V W X Y Z -

**UPCONVERTER:** An electronic device for translating a frequency band to a frequency band with a higher center frequency.

**VERTICALLY POLARIZED WAVE:** A linearly polarized electromagnetic wave whose electric field vector is vertical with respect to the earth's surface.

**VIDEO:** The demodulated output of a telemetry receiver. A television or radar signal used to drive a cathode-ray tube.

**WAVE:** A disturbance that is a function of time or space or both. A disturbance propagated in a medium or through space. Disturbance indicates mechanical, voltage, current, electric field strength, or temperature displacement, etc.

**WAVE ANALYZER:** An electronic instrument for measuring the amplitude and frequency of various components of a complex signal.

**WHITE NOISE:** Noise which has a constant power spectral density over a specified bandwidth.

## 2.2 ACRONYMS AND ABBREVIATIONS

### A

AC	Alternating Current
A/D, ADC	Analog-to-Digital Converter
AFC	Automatic Frequency Control
AGC	Automatic Gain Control
AM	Amplitude Modulation
ANSI	American National Standards Institute
APC	Automatic Phase Control
AWGN	Additive White Gaussian Noise
AZ	Azimuth

### B

BCD	Binary Coded Decimal
BEP	Bit Error Probability
BER	Bit Error Rate
BI $\phi$ -L, -M, -S	Biphase Level, Mark, Space
BITE	Built-in Test Equipment
BIT SYNC	Bit Synchronizer
BPF	Bandpass Filter
BPIF	Bandpass Input Filter
bps, b/s	Bit Per Second
BPSK	Binary Phase Shift Keying
BR	Bit Rate
BSP	Bit Slippage Probability
BSR	Bit Slippage Rate
BSSC	Bit Synchronizer and Signal Conditioner
BW	Bandwidth

### C

CA	Constant Amplitude
CBW	Constant Bandwidth
CD	Constant Delay
CMOS	Complimentary Metal-Oxide-Semiconductor
CNR	Carrier-to-Noise Ratio
cps	Cycles Per Second
CRC	Cyclical Redundancy Check

## D

D/A, DAC	Digital-to-Analog Converter
dB	Decibel
dBc	Decibels Referenced to the Carrier Level
dB <sub>i</sub>	Decibels Referenced to Isotropic
dBm	Decibels Referenced to one Milliwatt
dBV	Decibels Referenced to one Volt
dBW	Decibels Referenced to one Watt
dc	Direct Current
DEM <sub>OD</sub>	Demodulator
DEM <sub>UX</sub>	Demultiplexer
DM	Delay Modulation, aka Miller Code, Modified Frequency Modulation
DSV	Digital Sum Variation

## E

ECC	Error-Correction Coding
ECL	Emitter Coupled Logic
EDAC	Error Detection and Correction
ENPBW	Equivalent Noise Power Bandwidth
EUC	Engineering Unit Conversion

## F

FDM	Frequency Division Multiplexing
FFI	Frame Format Identification
FIFO	First-In First-Out
FM	Frequency Modulation
FM/FM	Frequency Modulation/Frequency Modulation
FMG	Frequency Management Group
FRPI	Flux Reversals Per Inch
F/S	Filter and Sample
FSK	Frequency Shift Keying

## G

GCR	Group Code for Recording
GHz	Gigahertz
G/T	Gain/Noise Temperature

## H

HDDR	High Density Digital Recording
HE	High Energy
HR	High Resolution
Hz	Hertz

## I

IC	Integrated Circuit
I/D	Integrate and Dump
IF	Intermediate Frequency
IFM	Incidental Frequency Modulation
IFT	International Foundation for Telemetry
in/s	Inches Per Second
I/O	Input/Output
ips, IPS	Inches Per Second
IRIG	Inter-Range Instrumentation Group
I/S	Interference-to-Signal Ratio
ISI	Intersymbol Interference
ITC	International Telemetry Conference
ITDE	Inter-Track Displacement Error
ITU	International Telecommunications Union

## J

$J_i(x)$	$i^{\text{th}}$ Order Bessel Function of the First Kind
----------	---

## K

kbi, kb/in	Kilobits Per Inch
KHz	Kilohertz

## L

LBE	Lower Bandedge
LBW	Loop Bandwidth
LHC, LHCP	Left Hand Circular Polarization
LNA	Low Noise Amplifier
LOS	Line of Sight, Loss of Signal
LPF	Low-pass Filter
LSB	Least Significant Bit

## M

M <sup>2</sup>	Miller Squared
MCT	Manufacturers Center Line Tape
MHz	Megahertz
MI	Modulation Index
$\mu$ s	Microsecond
ms	Millisecond
MSB	Most Significant Bit
MUX	Multiplexer

## N

NLT	Noise Loading Test
NPR	Noise Power Ratio
NPRF, NPRO	Noise Power Ratio Floor
NPRI	Noise Power Ratio Intermodulation
NRL	Normal Record Level
NRZ-L, -M, -S	Non-Return-to-Zero Level, Mark, Space
ns	Nanosecond
NTIA	National Telecommunication and Information Administration

## P

PAM	Pulse Amplitude Modulation
PAM/FM	Pulse Amplitude Modulation/Frequency Modulation
PBW	Proportional Bandwidth
PCB	Printed Circuit Board
PCM	Pulse Code Modulation
PCM/FM	Pulse Code Modulation/Frequency Modulation
PCM/FM/FM	Pulse Code Modulation/Frequency Modulation/Frequency Modulation
PCM/PM	Pulse Code Modulation/Phase Modulation
PDM	Pulse Duration Modulation
PFD	Power Flux Density
PLL	Phase Locked Loop
PM	Phase Modulation
PN	Pseudo Noise
POST-D	Post Detection
p-p	Peak-to-Peak
ppm	Parts Per Million
PPM	Pulse Position Modulation
PREAMP	Preamplifier
PRE-D	Predetection
PREMOD	Premodulation
PR	Pseudo Random
PRN	Pseudo Random Noise
PRS	Pseudo Random Sequence
PROM	Programmable Read Only Memory
PSK	Phase Shift Keying
PWA	Printed Wiring Assembly



## R

RAM	Random Access Memory
RCC	Range Commanders Council
RCD	Record
RCDR	Recorder
RCVR	Receiver
RDP	Radiation Density Pattern
RCD/REPRO	Record/Reproduce; Recorder/Reproducer
REPRO	Reproduce
RF	Radio Frequency
RHC, RHCP	Right Hand Circular Polarization
rms	Root-Mean-Square
RNRZ	Randomized Non-Return-to-Zero
ROM	Read Only Memory
RSC	Reed-Solomon Code
RZ	Return-to-Zero

## S

SCO	Subcarrier Oscillator
SFID	Subframe Identification
S/H	Sample and Hold
S/I	Signal-to-Interference Ratio
SIM	Simulated
SNR	Signal-to-Noise Ratio
SR	Standard Resolution
SRL	Standard Record Level
SYNC	Synchronization

## T

TBE	Time Base Error
TCRG	Time Code Reader/Generator
TDM	Time Division Multiplex
TG	Telemetry Group
THIC	Tape Head Interface Committee
TLM, TM	Telemetry, Telemeter
TP	Test Point
TPI	Tracks Per Inch
TSC	Tape Speed Compensation
TSCC	Telemetry Standards Coordinating Committee
TTL	Transistor-Transistor Logic

## U

UBE	Upper Bandedge
UHF	Ultra High Frequency

V

VCO	Voltage Controlled Oscillator
VCXO	Voltage Controlled Crystal Oscillator
VHF	Very High Frequency
VSWR	Voltage Standing Wave Ratio

W

WRT	Working Reference Tape
-----	------------------------

X

XMIT	Transmit
XMTR	Transmitter
XTAL	Crystal

### 3.0 TELEMETRY SIGNALS and NOISE

This section discusses the characteristics of various telemetry signals. The topics addressed include:

1. Data quality
2. Premodulation filtering
3. Transmitter and subcarrier oscillator deviation
4. Receiver filter selection
5. Baseband spectral characteristics
6. Radio frequency spectral characteristics
7. Link analysis
8. Frequency modulation demodulator noise characteristics.

Both time division multiplex (TDM) and frequency division multiplex (FDM) signals are discussed in this section. TDM systems use different time slots to send different signals. Pulse code modulation (PCM) and pulse amplitude modulation (PAM) are examples of TDM systems. FDM systems use different frequency slots to send different signals at the same time. Frequency modulation/frequency modulation (FM/FM), where several subcarrier oscillators are modulated by different information signals, is an example of an FDM system. Hybrid systems use both TDM and FDM in the same system. An example of a hybrid system is a PCM signal on the baseband with several higher frequency SCOs.

This section includes information on PCM signals using both frequency and phase modulation and both non-return-to-zero (NRZ) and biphase (Manchester) codes. Since PCM is used in most new telemeters, brief summaries of PCM characteristics are included in subsection 3.0. Information is also presented on NRZ-PAM/FM signals. The use of noise power ratio (NPR) to simulate FM/FM signals is also addressed.

### 3.0.1 NRZ PCM/FM Summary

Polarity Insensitive	No (Level Code); Yes (Mark and Space Codes)
DC Component	Yes
Transitions	Not Guaranteed
Optimum Peak Deviation	$0.35 f_B$
Premodulation Filtering	$0.7 f_B$ or Wider
AC Coupling	No
BER vs SNR	11.8 dB IF SNR in Bandwidth Equal to the Bit Rate for $10^{-5}$ BER (Optimum)
Bit Errors Determined by	Pop Noise
Receiver IF Bandwidth	Bit Rate Plus
Receiver Video Bandwidth	Bit Rate/2 to Bit Rate
Preferred Bit Detector	Filter and Sample
Predetection Recording	Recommended
Postdetection Recording	Randomization or BI $\phi$ Recommended
Loop Bandwidth	N/A
Demodulator Output Polarity Known	Yes
Bandwidth for 99% Power	$1.16 \times \text{Bit Rate}$ (Premodulation Filter = $0.7 f_B$ )
Maximum Bit Rate in IRIG 1 MHz Bandwidth	740 kb/s (Premodulation Filter = $0.7 f_B$ )

Where  $f_B$  is Equal to the Bit Rate Frequency.

### 3.0.2 Biphase PCM/FM Summary

Polarity Insensitive	No (Level Code); Yes (Mark and Space Codes)
DC Component	None
Transitions	At Least One Every Bit Period
Optimum Peak Deviation	$0.65 f_B$
Premodulation Filtering	$1.4 f_B$ or Wider
AC Coupling	Yes
BER vs SNR	14.8 dB IF SNR in Bandwidth Equal to the Bit Rate for $10^{-5}$ BER (Optimum)
Bit Errors Determined by	Pop Noise
Receiver IF Bandwidth	Two X Bit Rate or Wider
Receiver Video Bandwidth	Bit Rate to 2 X Bit Rate
Preferred Bit Detector	Usually No Choice
Predetection Recording	Recommended
Postdetection Recording	BI $\phi$ Recommended
Loop Bandwidth	N/A
Demodulator Output Polarity Known	Yes
RF Bandwidth for 99% Power	2 X Bit Rate (Premodulation Filter = $1.4 f_B$ )
Maximum Bit Rate in IRIG 1 MHz Bandwidth	333 kb/s (Premodulation Filter = $1.4 f_B$ )

Where  $f_B$  is Equal to the Bit Rate Frequency.

### 3.0.3 NRZ PCM/PM Summary

Polarity Insensitive	No (Level Code); Yes (Mark and Space Codes)
DC Component	Yes
Transitions	Not Guaranteed
Optimum Peak Deviation	90°
Premodulation Filtering	1.0 $f_B$ or Wider
AC Coupling	No
BER vs SNR	10.7 dB IF SNR in Bandwidth Equal to Bit Rate for $10^{-5}$ BER (Optimum with Mark or Space Codes)
Bit Errors Determined by	Additive White Gaussian Noise
Receiver IF Bandwidth	As Wide as Possible Without Interference
Receiver Video Bandwidth	Bit Rate or Wider
Preferred Bit Detector	I/D if Filters are Wider than 0.7 $f_B$
Predetection Recording	Recommended
Postdetection Recording	Randomization or BIØ Recommended
Loop Bandwidth	Less than 0.05 $f_B$
Demodulator Output Polarity Known	No
RF Bandwidth for 99% Power	4 X Bit Rate (Premodulation Filter = 1.0 $f_B$ )
Maximum Bit Rate in IRIG 1 MHz Bandwidth	333 kb/s (Premodulation Filter = 1.0 $f_B$ )

Where  $f_B$  is Equal to the Bit Rate Frequency.

### 3.0.4 Biphase PCM/PM Summary

Polarity Insensitive	No (Level Code); Yes (Mark and Space Codes)
DC Component	None
Transitions	At Least One Every Bit Period
Optimum Peak Deviation	90° (Mark and Space Codes); 75° (Level Code)
Premodulation Filtering	2.0 $f_B$ or Wider
AC Coupling	Yes
BER vs SNR	11.0 dB IF SNR in Bandwidth Equal to Bit Rate for $10^{-5}$ BER (Optimum with Mark or Space Codes)
Bit Errors Determined by	Additive White Gaussian Noise
Receiver IF Bandwidth	As Wide as Possible Without Interference
Receiver Video Bandwidth	2 X Bit Rate or Wider
Preferred Bit Detector	Usually No Choice
Predetection Recording	Recommended
Postdetection Recording	BI $\phi$ Recommended
Loop Bandwidth	Less than: 0.05 $f_B$ (90°); 0.02 $f_B$ (75°)
Demodulator Output Polarity Known	No (PSK Demod); Yes (PM Demod)
RF Bandwidth for 99% Power	8 X Bit Rate (90°); 6 X Bit Rate (75°) (Premodulation Filter = 2.0 $f_B$ )
Maximum Bit Rate in IRIG 1 MHz Bandwidth	125 kb/s (90°) to 166 kb/s (75°) (Premodulation Filter = 2.0 $f_B$ )

Where  $f_B$  is Equal to the Bit Rate Frequency.

### 3.1 NRZ PCM/FM

#### 3.1.1 Introduction

Non-return-to-zero pulse code modulation/frequency modulation (NRZ PCM/FM) is a combined coding and modulation method used to send digital data over a transmission link. The method provides a shift in carrier frequency of  $x$  hertz (Hz) higher in frequency to represent one state of a binary signal (usually the ONE state) and a shift of  $x$  hertz lower in frequency to represent the other state (usually the ZERO state) of the binary signal. The most commonly used code for PCM/FM is the non-return-to-zero level (NRZ-L) code.<sup>1</sup> As the name, NRZ-L implies, the level of the modulation stays the same until the data changes state - that is, the level does not go to zero level between the data pulses.

The non-return-to-zero mark and space (NRZ-M and NRZ-S) versions are sometimes used when very long strings of either ones or zeros are expected in the data stream. These codes are illustrated in reference 1. If long streams of zeros (but not of ones) are expected in the data stream, then the NRZ-S coding method is used because it provides a transition for each zero in the data stream. The NRZ-M code is used to force transitions in the data stream when long strings of ones are expected in the data. The purpose for selecting a coding method which provides additional transitions is that the PCM bit synchronizer needs transitions to generate a reconstructed clock of the proper phase and frequency.

The NRZ-M and NRZ-S codes have the advantage of being polarity insensitive. That is, the PCM bit stream can be inverted and no change will occur in the output of the PCM bit synchronizer. A disadvantage of using these codes is that every isolated bit error causes the following bit to be in error also. Therefore, if one is going to use an error-correcting code in a system where the mark or space codes are used, the error correction encoding should be done after the data is converted to the mark or space code.

Several other techniques may be used to prevent the problems associated with long strings of ONES or ZEROS in the bit stream, they include: randomizing the data, adding an odd parity bit to words that have an odd number of data bits, and using biphasic (Manchester) coding.

The intermediate frequency (IF) signal-to-noise ratio (SNR) for a bit error rate (BER) of  $10^{-5}$  in figure 3.1-1 is approximately 11.8 dB. Increasing the IF SNR by 1 dB decreases the BER to approximately  $10^{-6}$ . The BER will decrease by at least a factor of 10 for each additional dB the IF SNR is increased. Decreasing the IF SNR by 1.2 dB (to 10.6 dB) increases the BER to approximately  $10^{-4}$ . The BER values will be different if the premodulation or IF filters are different than in figure 3.1-1 or if any extra encoding/decoding is used.

<sup>1</sup>Secretariat, Range Commanders Council, *Telemetry Standards*, White Sands Missile Range, New Mexico, RCC, May 1986. (IRIG Standard 106-86).



MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz TYPE	PEAK DEV	BIT DET
+ NRZ-L PCM/FM	1000	1000	NONE	306	F/S
o NRZ-L PCM/FM	1000	1000	NONE	405	F/S
* NRZ-L PCM/FM	1000	1000	NONE	350	F/S

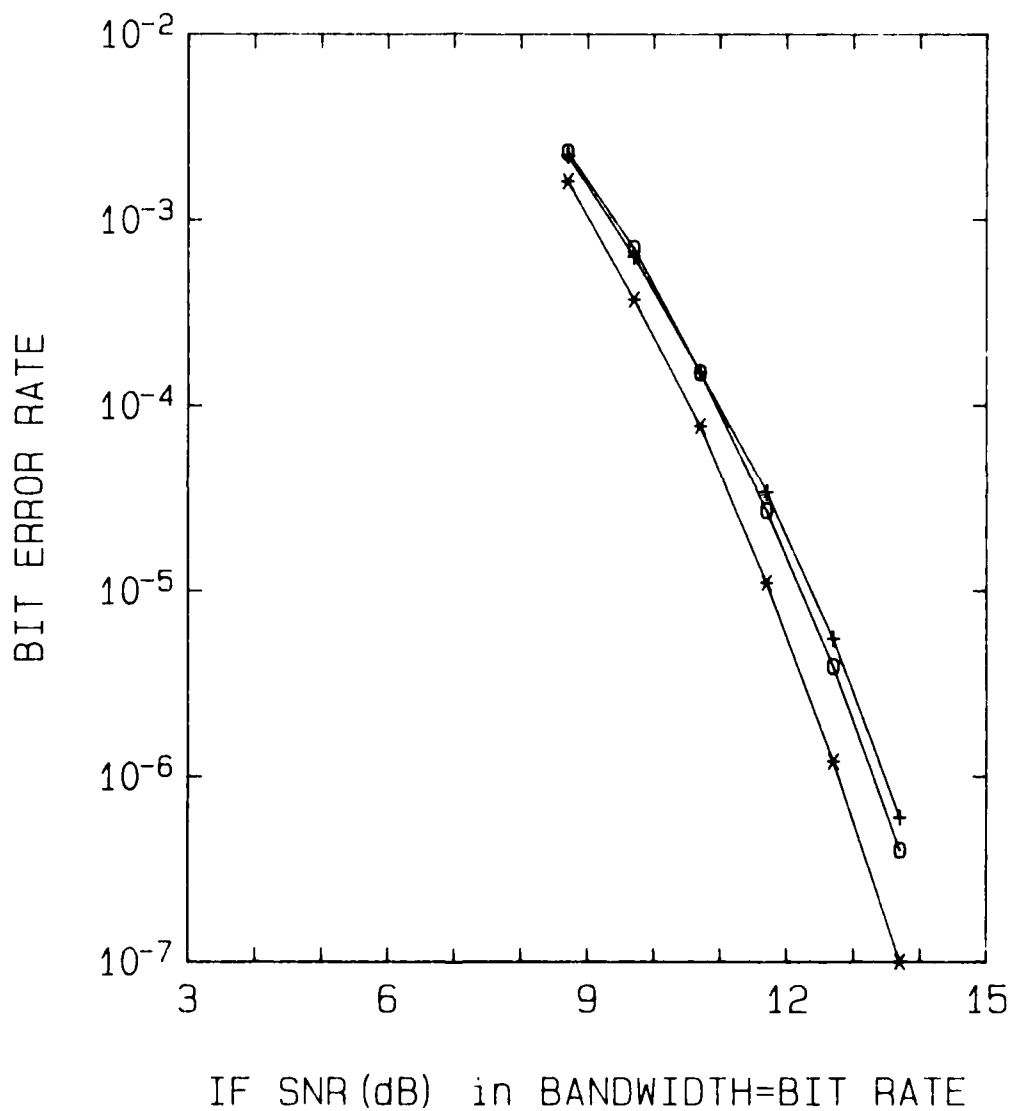


Figure 3.1-1. NRZ-L PCM/FM BER for Three Peak Deviations.

### 3.1.2 Selection of Peak Deviation

The optimum peak deviation for NRZ PCM FM is approximately 0.35 times the bit rate; i.e., a 1.0 megabit per second (Mb/s) bit stream should have a peak deviation of 350 kilohertz (kHz) and a peak-to-peak deviation of 700 kHz.<sup>2,3,4,5</sup> The RF spectra for various peak deviations are presented in subsection 3.1.8. Most papers on the subject of PCM FM deviation use peak-to-peak values (usually symbolized by an  $h$ ), but peak deviation is used in this document to keep PCM FM consistent with FM/FM, PAM/FM, and PCM/PM where peak deviation is generally used to describe the amount of deviation. This optimum value of peak deviation is valid when using IF bandwidths (BW's) that are between 1 and 3 times the bit rate and for systems where the total incidental frequency modulation (IFM) is much smaller than the peak deviation. Incidental frequency modulation is defined as follows: the carrier deviation produced by frequency modulation when the modulating signals are not wanted and are internal to the RF signal source. Typical transmitter IFM specifications are 5 kHz peak and/or 2 kHz rms. Therefore, the minimum PCM FM peak deviations should be 15 to 20 kHz; i.e., 3 to 4 times peak or 7.5 to 10 times rms. The actual minimum useable peak deviation is a function of the actual transmitter frequency stability and the receiving system frequency stability. In addition, phase modulation may be preferable to frequency modulation for low bit rate systems. If the predetection bandwidth is wider than 3 times the bit rate, the optimum peak deviation is approximately 0.35 times the predetection bandwidth. As an example, assume we need to transmit 64 kb/s (NRZ-L PCM/FM) and the receiving system's narrowest IF bandwidth is 500 kHz. In addition, assume that predetection recording and/or demodulation are not options. The IF SNR for a  $10^{-5}$  BER with a 22 kHz peak deviation is approximately 10.3 dB. The IF SNR for a  $10^{-5}$  BER with a peak deviation of 175 kHz is approximately 7.6 dB. However, a better option, if available, would be to use NRZ-M (or NRZ-S) PCM/PM with 90 degree peak deviation and a PSK demodulator. A  $10^{-5}$  BER could be achieved with an IF SNR of approximately 1.8 dB (IF SNR in bandwidth equal to bit rate of 10.7 dB). Data quality, usually measured by bit error rate (BER) performance, is affected by the amount of carrier deviation and also the premodulation filter bandwidth, predetection filter, demodulator, and bit detector characteristics.

<sup>2</sup>Kotelnikov, V. A. The Theory of Optimum Noise Immunity. Dover, New York, 1968.

<sup>3</sup>Gagliardi, R. M. Introduction to Communications Engineering. Wiley, New York, 1978.

<sup>4</sup>Tjhung, T. T., and Wittke, P. H. "Carrier Transmission of Binary Data in a Restricted Band," in IEEE Transactions on Communications, Vol. COM-18, pp. 295-304, August 1970.

<sup>5</sup>Cartier, D. E. "Limiter-Discriminator Detection Performance of Manchester and NRZ Coded FSK," in IEEE Transactions of Aerospace and Electronic Systems, Vol. AES-13, pp. 62-70, January 1977.

When peak deviation is increased to a value of approximately 0.4 times the bit rate, the BER performance is typically degraded by a few tenths of a dB; i.e., at a BER of  $1 \times 10^{-5}$ , the degradation is in a range of 0.2 to 0.4 dB (refer to figures 3.1-1 and 3.1-2). The major cause of degradation to signal quality is the additional attenuation introduced by the predetection IF filter at the peak deviation value; i.e., approximately 0.5 dB more attenuation is present at  $\pm 400$  kHz than at  $\pm 350$  kHz (see figure 3.1-3). The result is that the instantaneous IF SNR is reduced by approximately 0.5 dB, thus producing more bit errors in the data stream due to "pop" noise. Another cause of additional pops (see section 3.11) with higher peak deviation is that the difference in frequency between the instantaneous signal frequency and the instantaneous noise frequency is usually larger. Therefore, the probability of the noise being larger than the signal for a long enough time interval to cause a pop is increased because the required time interval is inversely proportional to the difference in frequency. An additional possible cause of increased BER with increased deviation is that the phase linearity of the IF filter gets worse towards the band edges which produces more intersymbol interference.

However, the signal energy per bit is increased by 1.2 dB,  $(20 \log (0.4/0.35))$  which significantly reduces the number of bit errors due to fluctuation noise (see section 3.11). Therefore, when the premodulation filter bandwidth is set to one-half the bit rate, the degradation due to slight over deviation should be negligible. The reason the degradation is negligible is that the narrow premodulation filter bandwidth reduces the amplitude of single bits of either polarity, thus increasing the susceptibility to the effects of fluctuation noise. Therefore, with an IF bandwidth equal to the bit rate and a premodulation filter bandwidth equal to one-half the bit rate, fluctuation noise is the major cause of bit errors.

*In the case where the peak deviation is decreased to a value corresponding to approximately 0.3 times the bit rate, the bit error performance is typically degraded by approximately 0.6 dB at a BER of  $1 \times 10^{-5}$  (with the predetection IF bandwidth set equal to the data bit rate). The reason for this degradation is that the signal energy per bit is reduced by 1.3 dB,  $20 \log (0.3/0.35)$ , which has the effect of significantly increasing the number of bit errors due to fluctuation noise. This increase in bit errors more than compensates for the decrease in bit errors resulting from pop noise, because of decreased predetection IF attenuation (approximately 0.4 dB in figure 3.1-3).*

Decreasing the peak deviation by 3 dB and 6 dB requires an increase in SNR of 2.3 and 5.2 dB at a BER of  $10^{-5}$ . This is illustrated in figure 3.1-4. Under the following conditions: BER =  $10^{-5}$ , IF BW =  $1.4 \times$  bit rate,  $\Delta f = 0.35$  times bit rate and premodulation filter bandwidth =  $0.7$  times bit rate, approximately one-third of the errors are due to fluctuation noise and two-thirds to pop noise. Increasing the deviation rapidly increases the errors due to pop noise (a peak deviation of  $0.7$  times the bit rate degrades the data quality by 4 to 6 dB when the IF bandwidth is equal to the bit rate), while decreasing the deviation rapidly increases the errors due to fluctuation noise. The minimum BER is achieved when the peak deviation is  $0.35$  ( $-10\%$ ,  $+20\%$ ) of the bit rate for IF bandwidths between 1 and 3 times the bit rate.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
X NRZ-L PCM/FM	1000	1500	700	CD	200	F/S
O NRZ-L PCM/FM	1000	1500	700	CD	400	F/S
+ NRZ-L PCM/FM	1000	1500	700	CD	500	F/S
o NRZ-L PCM/FM	1000	1500	700	CA	357	F/S
* NRZ-L PCM/FM	1000	1500	700	CD	357	F/S

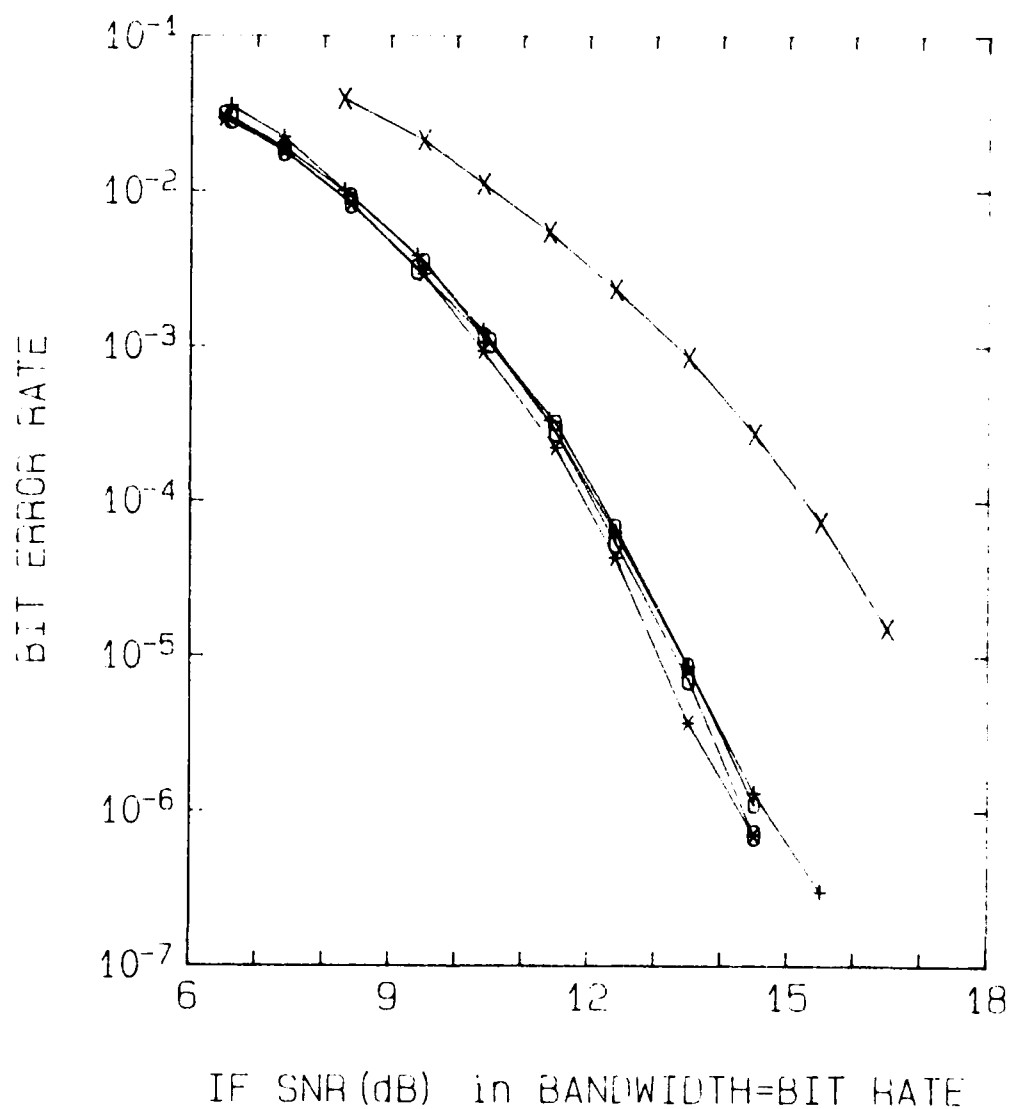


Figure 3.1-2. NRZ-L PCM/FM BER for Various Peak Deviations.

IF BW=1.000 MHz

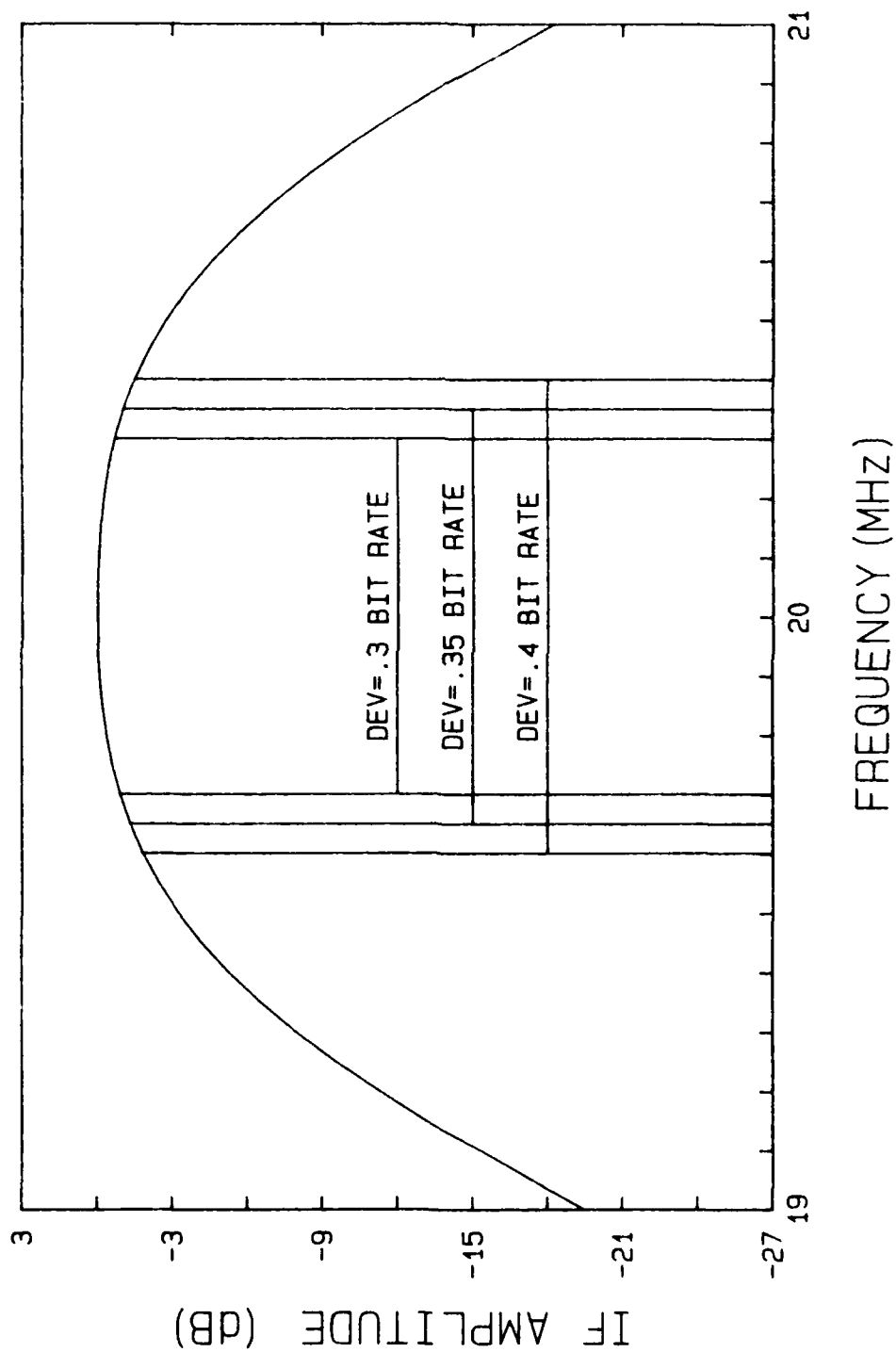


Figure 3.1-3. IF Filter Attenuation Versus Peak Deviation.

MODULATION TYPE	BIT RATE IF BW kb/s kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
--------------------	----------------------------	---------------	------	-------------	------------

+	NRZ-L PCM/FM	700	1000	500	CD	123	F/S
o	NRZ-L PCM/FM	700	1000	500	CD	173	F/S
*	NRZ-L PCM/FM	700	1000	500	CD	245	F/S

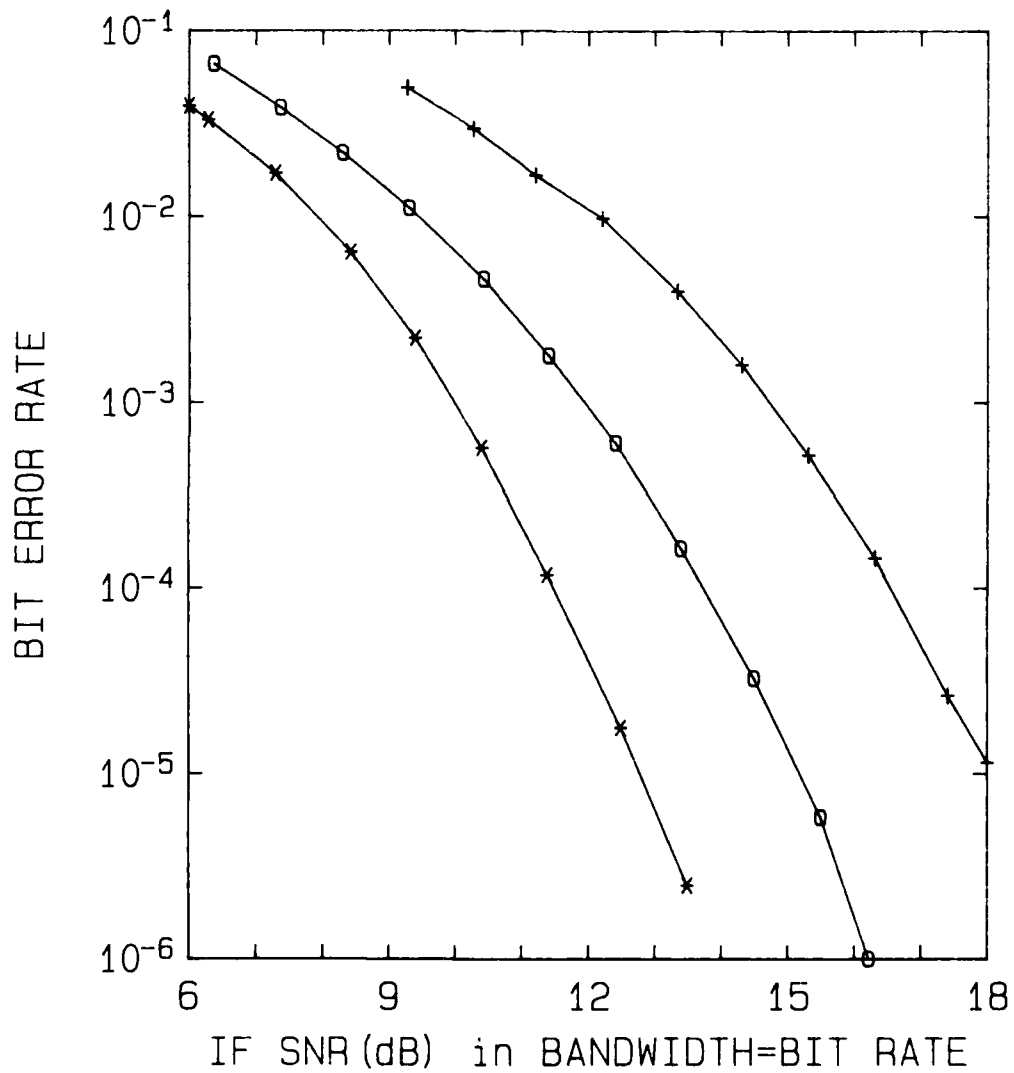


Figure 3.1-4. BER for Peak DEV/Bit Rate=0.175, 0.25, and 0.35

### 3.1.3 Selection of Premodulation Filter

Premodulation filters are used to reduce the baseband and RF bandwidths of the PCM signal. The best premodulation filter is the widest linear phase filter which allows the spectral occupancy requirements to be met. A low pass filter bandwidth (-3 dB) having a value that is equal to or greater than 0.7 times the bit rate will not cause a significant increase in the bit error rate. However, the use of a premodulation filter bandwidth of 0.5 times the bit rate will degrade the performance by 1 dB when the IF bandwidth is equal to the bit rate. The bit error rates achieved while using linear phase filters were repeatedly as good or better than the bit error rates achieved while using constant amplitude (CA) filters having the same 3 dB bandwidth.

Figures 3.1-5 through 3.1-8 show the PCM wavetrains which result when an NRZ-L signal is filtered at the bit rate and one-half the bit rate using 5-pole constant delay (CD) and constant amplitude low pass filters.

### 3.1.4 Direct Current (DC) Component and Alternating Current (AC) Coupling

The level of the DC component contained in an NRZ-L data stream can vary over a wide range: from essentially no DC component with randomized data to essentially 100% DC when long strings of data without a transition are encountered. The use of AC coupling eliminates the DC component. The Inter-Range Instrumentation Group (IRIG) Standards prohibit the use of AC coupling of many NRZ-L signals by the statement that "frequency deviation from the carrier shall be the same for each occurrence of the same level." AC coupling should be avoided because it forces the average value of the data stream to be zero V DC. When the number of ones and zeros is nearly equal over any short time interval, the frequency for a one will be  $f_0 + x$  and the frequency for a zero will be  $f_0 - x$ . However, if the ratio of ones to zeros changes to three ones to each zero and the signal is AC-coupled, then the frequency for a one will be  $f_0 + x/2$  and the frequency for a zero will be  $f_0 - 3x/2$ . The lack of balance between the ones and zeros can cause major data degradation problems due to the effects of signal attenuation in the final IF filter of the receiver or in any other bandwidth-limited device in the telemetry system; i.e., such as an analog microwave link because the level that is present least often appears to be deviated farther from the carrier, as is illustrated in figure 3.1-9. In figure 3.1-9, the DC-coupled frequencies for ones and zeros are attenuated by 0.9 dB by the receiver IF filter. Assume the BER is  $10^{-5}$ . Increasing the signal by 0.8 dB decreases the BER to  $1.6 \times 10^{-6}$  and decreasing the signal by 2.8 dB increases the BER to  $10^{-3}$ . Therefore, the BER for the AC-coupled signal would be:

$$3/4 (1.6 \times 10^{-6}) + 1/4 (10^{-3}) = 2.5 \times 10^{-4}.$$

The RF power would have to be increased by 1.9 dB to decrease the BER to  $10^{-5}$ . Therefore, the data quality has been degraded by 1.9 dB by AC-coupling the signal. The degradation would be greater if the ratio of ones to zeros (or vice versa) was larger than 3 to 1. An additional problem encountered when using AC coupling is that the energy associated with each bit in a long string of data bits without transitions is less than the energy in the previous bit because of the decay due to the resistance-capacitance (RC) time constant. Therefore, NRZ signals should never be AC-coupled unless some sort of positive control exists over the ratio of ones to zeros (the ratio should be one). One method of achieving this control is to randomize the NRZ signal. However, most randomization techniques cause an increase in the BER. Adding a parity bit does not provide sufficient control.

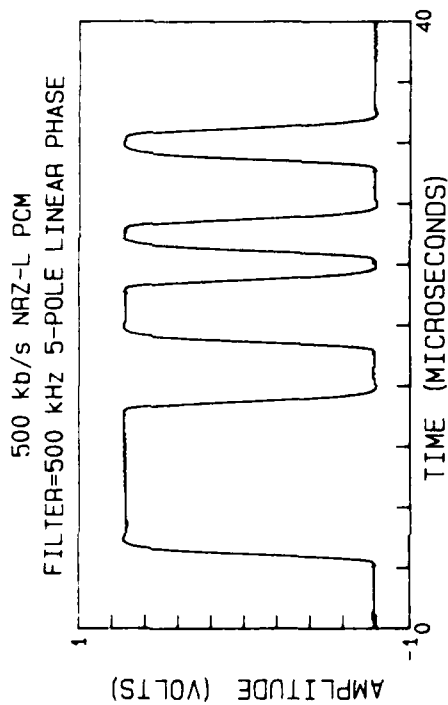


Figure 3.1-5. NRZ-L Signal with PREMOD Filter=Bit Rate (CD).

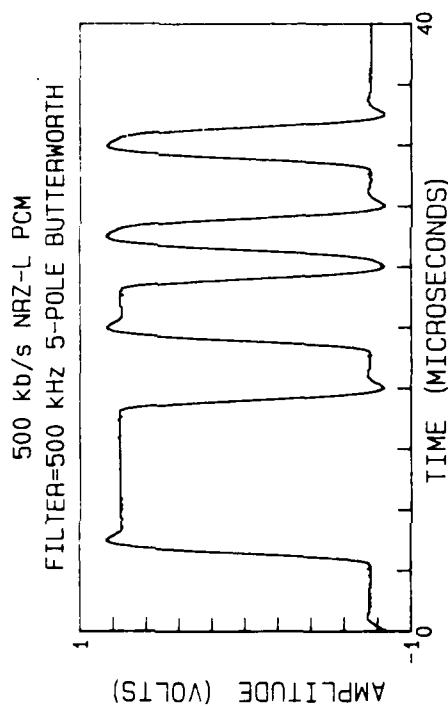


Figure 3.1-6. NRZ-L Signal with PREMOD Filter=Bit Rate (CA).

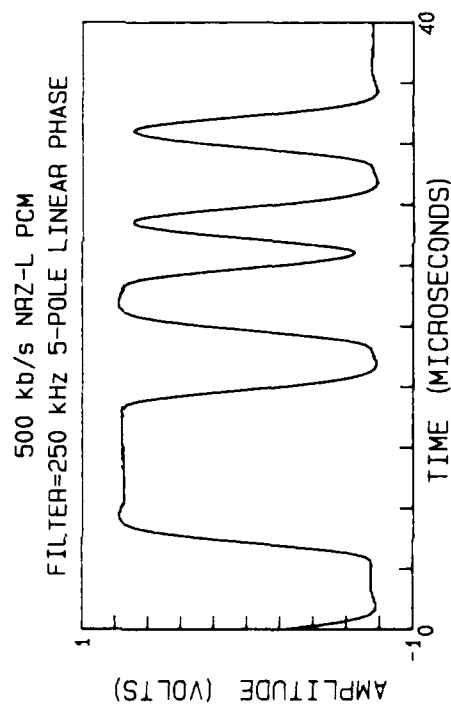


Figure 3.1-7. NRZ-L Signal with PREMOD Filter=Bit Rate/2 (CD).

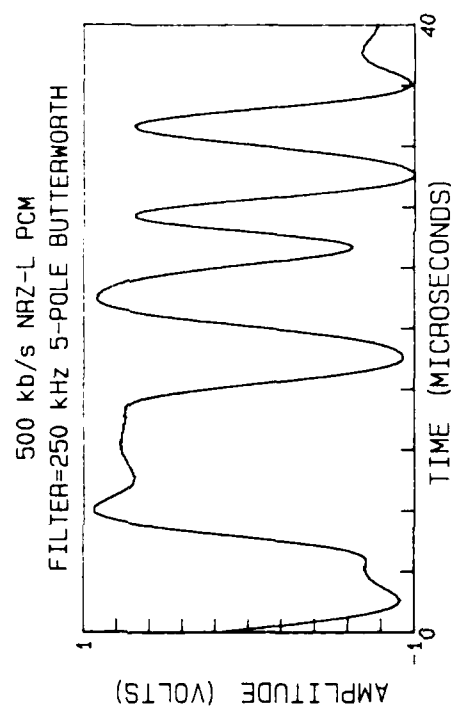


Figure 3.1-8. NRZ-L Signal with PREMOD Filter=Bit Rate/2 (CA).



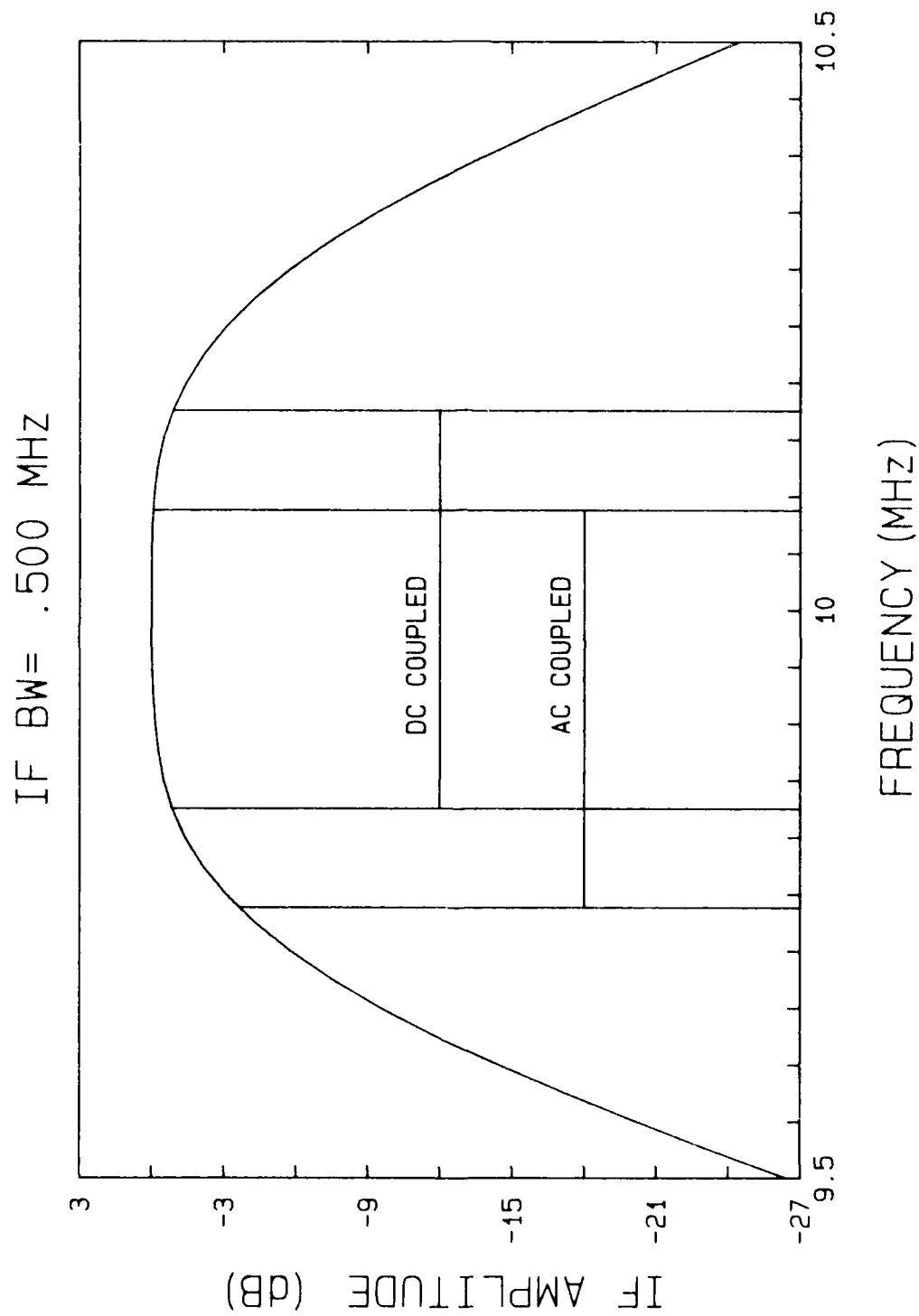


Figure 3.1-9. Effect of AC Coupling on NRZ PCM/FM Signal.

### 3.1.5 Selection of Receiver IF Bandwidth

When using a peak deviation value corresponding to approximately 0.35 times the bit rate, the optimum IF bandwidth is approximately equal to the bit rate. This is illustrated in figure 3.1-10. Comparing IF SNRs in a bandwidth equal to the bit rate, we find that 500 kb/s (IF bandwidth/bit rate = 1) performs 0.2 dB better than 400 kb/s (IF bandwidth/bit rate = 1.25) and 1 dB better than 600 kb/s (IF bandwidth/bit rate = 0.83) at a BER of  $10^{-4}$ . However, the IF SNR in a 500 kHz IF bandwidth is 1 dB lower than the IF SNR in a 400 kHz IF bandwidth ( $10 \log (500/400)$ ). Therefore, if we were receiving both 400 kb/s and 500 kb/s through 500-kHz IF filters, the 400-kb/s data would achieve a  $10^{-4}$  BER with 0.8 dB less actual IF SNR (or less transmitted power). A lower bit rate will always provide a lower BER if the system is properly designed. The 600-kb/s data rapidly degrades relative to the other bit rates at low BERs because of the excessive filtering of the bit stream. Using an IF bandwidth equal to 1.5 times the bit rate causes a degradation of approximately 0.7 dB, and a bandwidth of twice the bit rate causes a degradation of approximately 1.8 dB. It is noted that when an IF bandwidth with a value equal to the bit rate is used, the receiver tuning becomes very critical. The effect of improper tuning is illustrated in figure 3.1-11. Tuning problems can be encountered due to transmitter or receiver frequency errors, transmitter drift, doppler shift, receiver drift, and ground station operator error. Small tuning errors can produce relatively large increases in the bit error rate. The reason for the increase in bit error rate is that the slopes of the IF bandpass filter roll off quite rapidly outside of the receiver passband; thereby attenuating the signal when the receiver is detuned. The following example points out the effects of receiver detuning: For a signal at 500 kb/s data rate passing through a 500-kHz IF bandwidth, the penalty is approximately 1 dB for 50 kHz of detuning and 2.5 dB for 100 kHz of detuning. For comparison, the penalty for using a 750-kHz IF bandwidth is approximately 0.7 dB, and a 1.0-MHz IF bandwidth is approximately 1.8 dB. The loss with a 100-kHz detuning error and a 750-kHz IF is approximately 1.0 dB and with a 1.0-MHz IF is approximately 0.6 dB. The actual losses in a given receiver depend on the amplitude and phase characteristics of the receiver filters. The amplitude characteristic of some receiver IF filters is not symmetrical about the center frequency. This causes excessive bit errors in one of the two states of the PCM signal.

A second area of concern associated with using receiver IF bandwidths set equal to the bit rate is that many receiver IF filters provide poor phase performance in the vicinity of their upper and lower band edges. Degraded phase performance can produce intersymbol interference and distorted bit symbol waveforms resulting in an increase in the bit error rate; especially at the lower bit error rates. Signal-to-noise ratio penalties of approximately 1 dB (0.7 to 1.4 dB) are typical at bit error rates of  $1 \times 10^{-5}$  with an IF bandwidth set to a value equal to the bit rate when a linear phase IF filter is not used. The penalty for using a non-linear phase IF filter decreases at higher bit error rates and for IF bandwidths which are set wider than a value equal to the bit rate because the bit error rate is dominated by pop noise under these conditions.

When PCM/FM signals are predetection-recorded, the receiver IF bandwidth should be set wider than the bit rate. Two major reasons for selecting the wider IF bandwidths when using predetection recording techniques are: (1) The effective filtering includes not only the receiver bandpass filter, but also the predetection

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
--------------------	------------------	--------------	---------------	------	-------------	------------

+	NRZ-L PCM/FM	600	500	500	CD	210 F/S
o	NRZ-L PCM/FM	500	500	500	CD	175 F/S
*	NRZ-L PCM/FM	400	500	500	CD	140 F/S

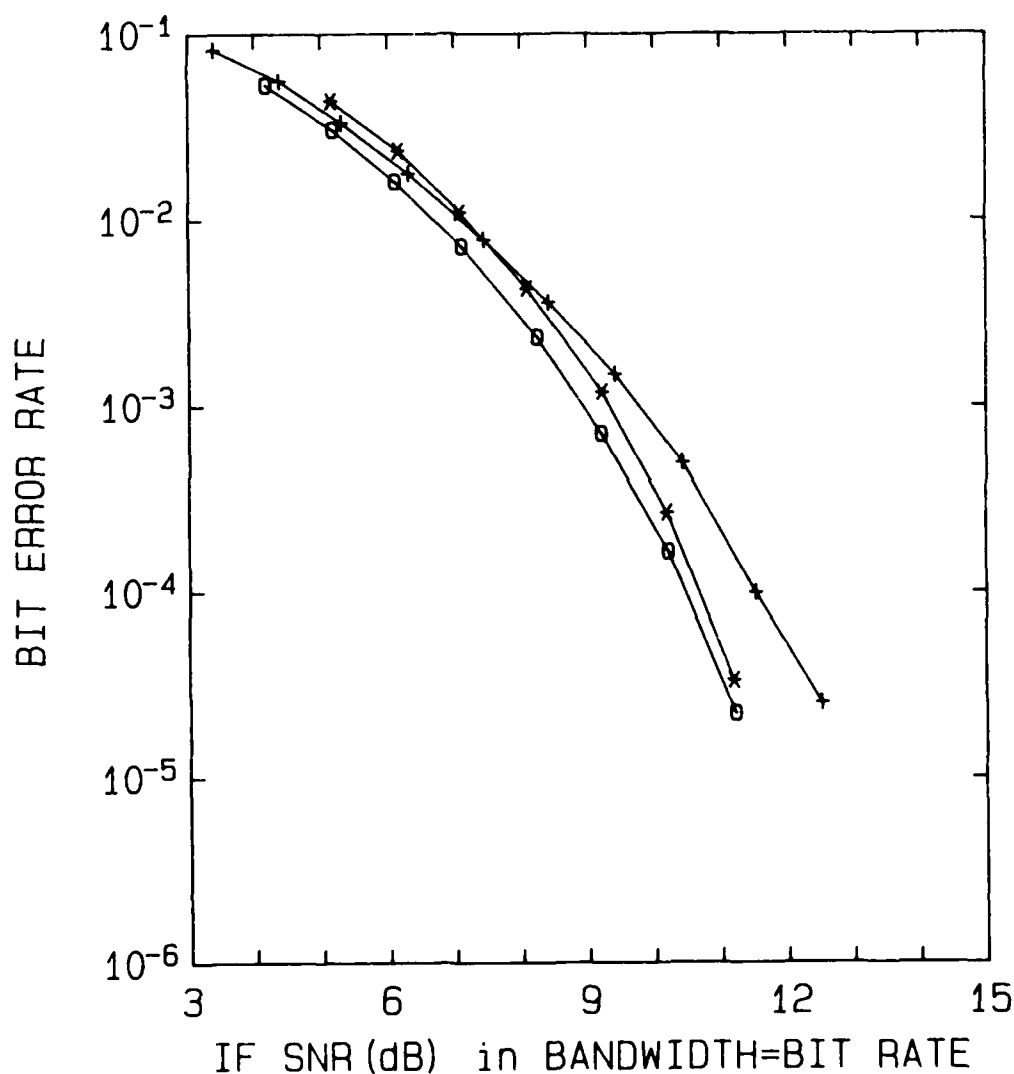


Figure 3.1-10. BER with 400, 500, and 600 kb/s in 500 kHz IF BW

MODULATION TYPE	IF BW kHz	PREMOD TYPE	PEAK DEV	BIT DET
0 NRZ-L PCM/FM-100	1000	1000CA 700	CD	357 F/S
+ NRZ-L PCM/FM+100	1000	1000CA 700	CD	357 F/S
o NRZ-L PCM/FM AFC	1000	1000CA 700	CD	357 F/S
* NRZ-L PCM/FM	1000	1000CA 700	CD	357 F/S

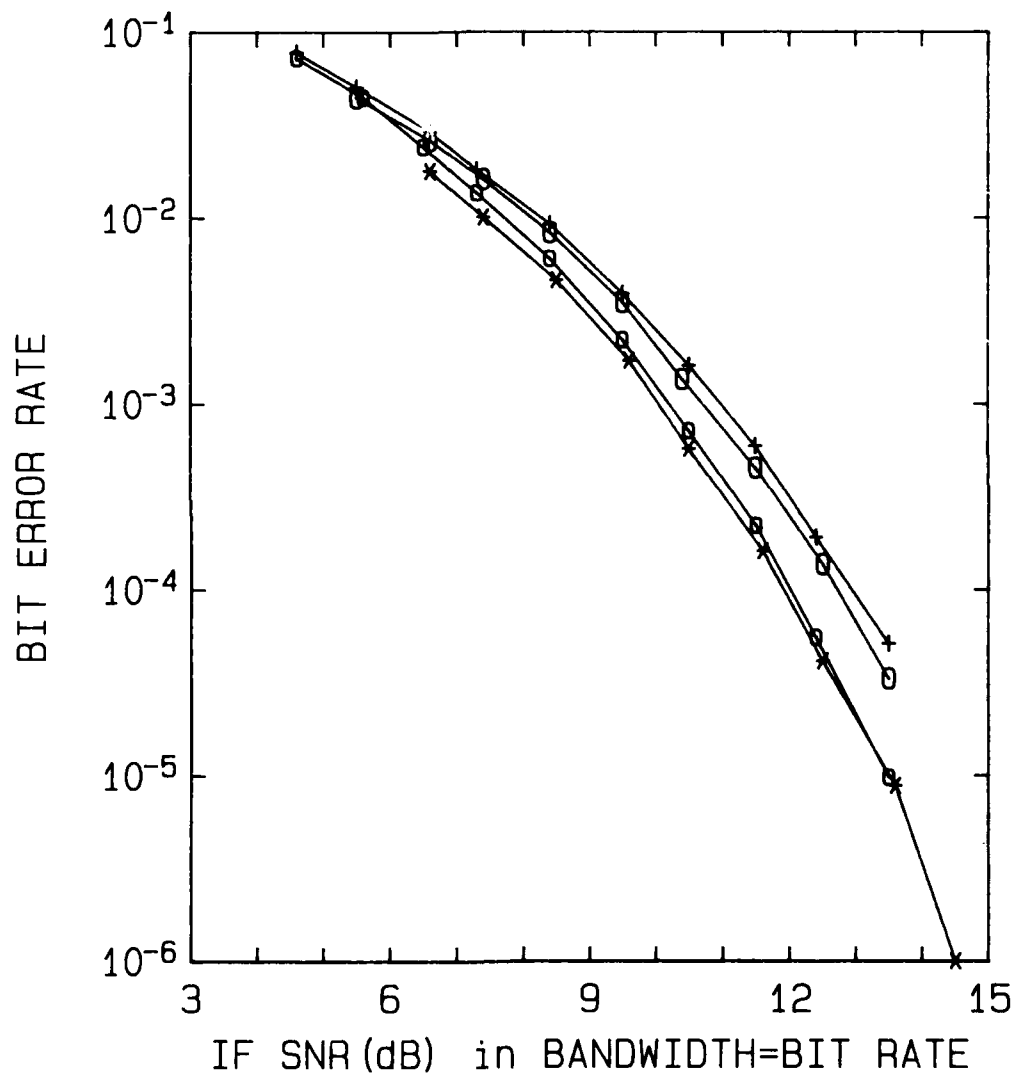


Figure 3.1-11. BER with AFC and with 100 kHz Detuning.

downconverter, the magnetic tape recorder/reproducer, and the predetection filter in the demodulator; (2) The selection of the wider IF filter provides the means for recording the signal with a minimum amount of degradation. It is extremely difficult to recover data which has been degraded through excessive filtering prior to recording on magnetic tape; however, it is relatively simple to filter out excessive out-of-band noise which is recorded on the magnetic tape. It is to be noted that the receiver bandwidth should never be wider than approximately two times the predetection carrier frequency. Extremely wide IF bandwidths should not be used because the noise frequency components will fold-over around the zero hertz origin and back into the data frequencies. The result is that, when using extremely wide IF filter bandwidths, a degradation of 3 dB in the SNR could occur.

The bit error rate, for a given unmodulated carrier IF SNR, decreases as the IF bandwidth is increased. This is illustrated in figure 3.1-12. This is very misleading because the IF SNR can not stay constant unless the transmitted power (or some other parameter) is increased. A fair comparison requires that the other link parameters remain constant while the parameter of interest is varied. This means that the bandwidth must remain constant when other parameters are varied. Using a bandwidth equal to the bit rate (as long as the bit rate is fixed) achieves this goal. The bit error rate versus IF SNR for IF bandwidths wider than 3 times the bit rate is nearly the same because the instantaneous signal suffers very little attenuation due to IF filtering. Most receiver IF filters are quite flat over the middle 25% of their 3-dB bandwidth. However, if one plots the BER versus IF SNR in a bandwidth equal to the bit rate (see figure 3.1-13), one can readily see that the use of wide IF bandwidths greatly degrades the data quality. The use of an IF bandwidth equal to three times the bit rate requires 3 to 3.5 dB more IF SNR in a bandwidth equal to the bit rate than does the use of an IF bandwidth equal to the bit rate. This is equivalent to doubling the transmitted power. The use of an IF bandwidth equal to 1.5 times the bit rate usually causes a degradation of less than 1 dB. This is illustrated in figure 3.1-14.

### **3.1.6 Selection of Demodulator Video Bandwidth**

The demodulator video bandwidth should not be set to a value which is less than one-half the bit rate. The preferred choice is usually a value which is between 0.7 and one times the bit rate; that is, for a 700-kb/s bit rate, the video bandwidth would be set to either 500 or 750 kHz. Note that filtering of the demodulated bit stream is also performed by the bit synchronizer. The use of narrow demodulator video filters, that is, less than 0.7 times the bit rate, will have the effect of making the PCM bit stream look "cleaner" to the eye, but may degrade the data quality. The reason being that the amplitude of the single bits is reduced more than the noise components. One exception does exist, if the bit synchronizer does not include a filter, but rather only samples the incoming data bit stream, the receiver video filter should be set to approximately 0.5 times the bit rate. The effect of video filtering is illustrated in figures 3.1-15, 3.1-16, and 3.1-17.

### **3.1.7 Selection of PCM Bit Synchronizer Bit Detector**

The use of a filter and sample (F/S) bit detector in the bit synchronizer system is usually the best choice for NRZ PCM/FM data. The only exceptions to the recommended filter and sample detector are in applications involving either

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
0 NRZ-L PCM/FM	500	3000	350	CD	178	F/S
+ NRZ-L PCM/FM	500	1500	350	CD	178	F/S
o NRZ-L PCM/FM	500	1000	350	CD	178	F/S
* NRZ-L PCM/FM	500	500	350	CD	178	F/S

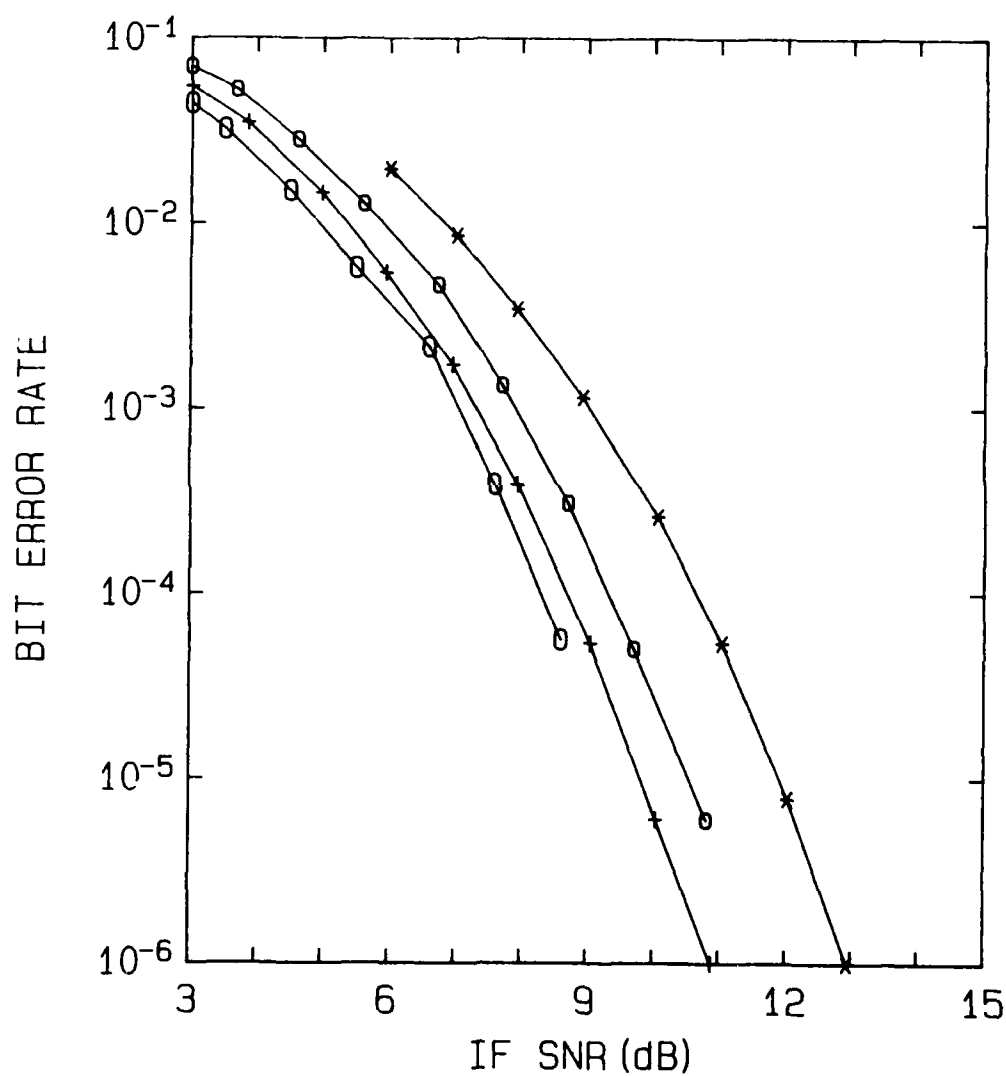


Figure 3.1-12. BER Versus IF SNR for Several IF BWs.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	PREMOD TYPE	PEAK DEV	BIT DET
0 NRZ-L PCM/FM	500	3000	500	CD	178	F/S
+ NRZ-L PCM/FM	500	1500	500	CD	178	F/S
o NRZ-L PCM/FM	500	1000	500	CD	178	F/S
* NRZ-L PCM/FM	500	500	500	CD	178	F/S

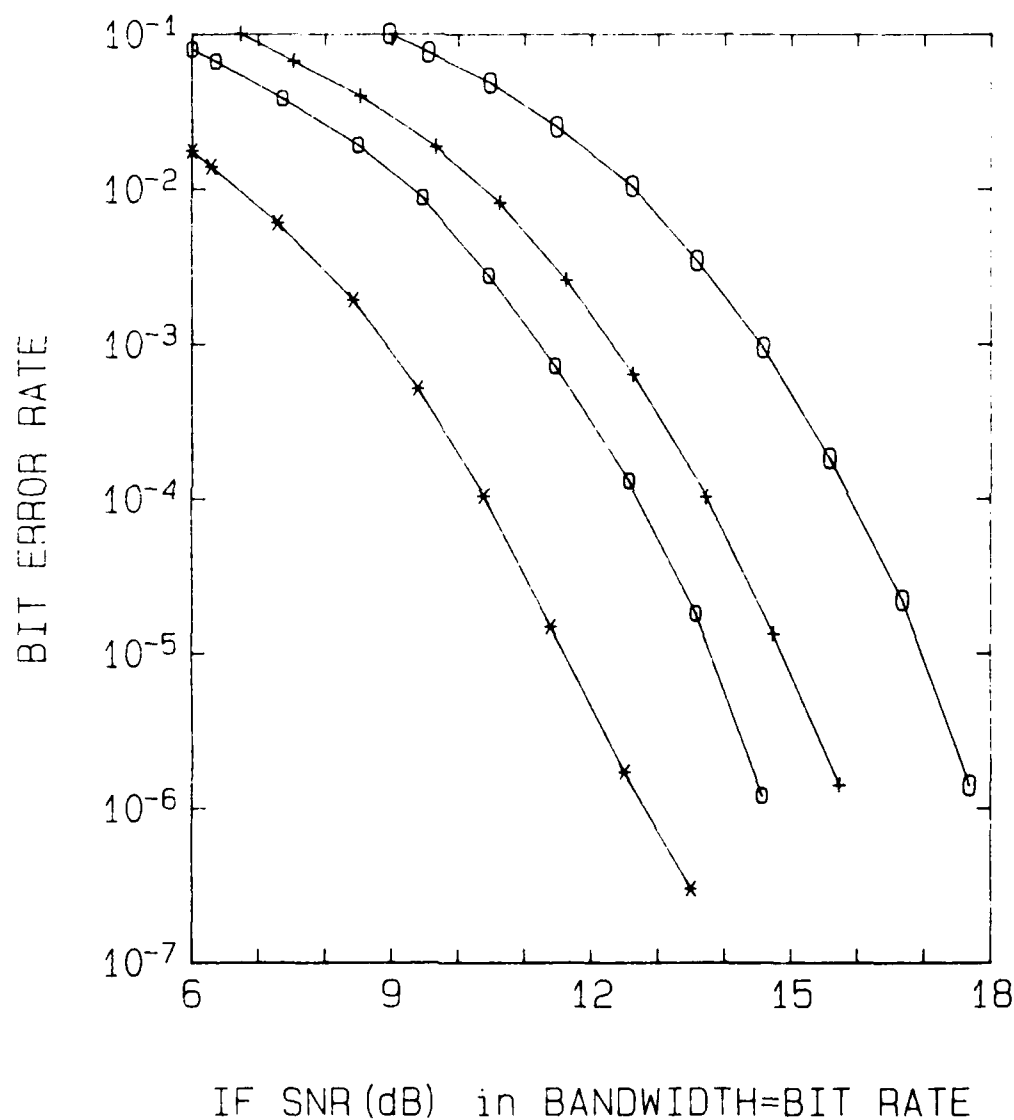


Figure 3.1-13. BER with IF BW/Bit Rate = 1, 2, 3, and 6.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
0 NRZ-L PCM/FM	1000	1500	700	CD	356	F/S
+ NRZ-L PCM/FM	1000	1500	1000	CD	356	F/S
o NRZ-L PCM/FM	1000	1000	700	CD	356	F/S
* NRZ-L PCM/FM	1000	1000	1000	CD	356	F/S

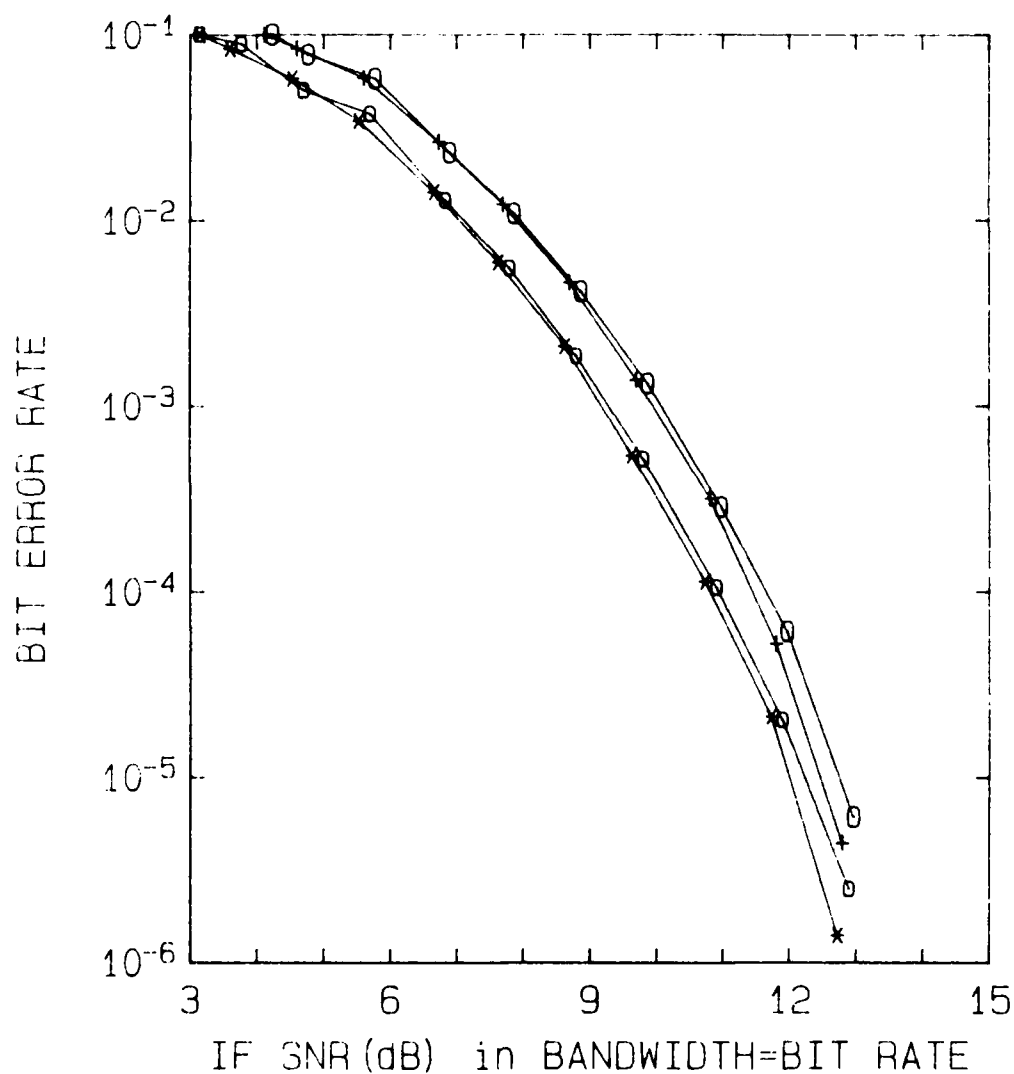


Figure 3.1-14. BER with IF BW/Bit Rate = 1 and 1.5.



MODULATION TYPE	BIT RATE IF BW kb/s	PREMOD kHz	VIDEO BIT DET
0 NRZ-L PCM/FM	1000	1000	500 I/D
+ NRZ-L PCM/FM	1000	1000	500 F/S
o NRZ-L PCM/FM	1000	500	500 F/S
* NRZ-L PCM/FM	1000	500	1000 F/S

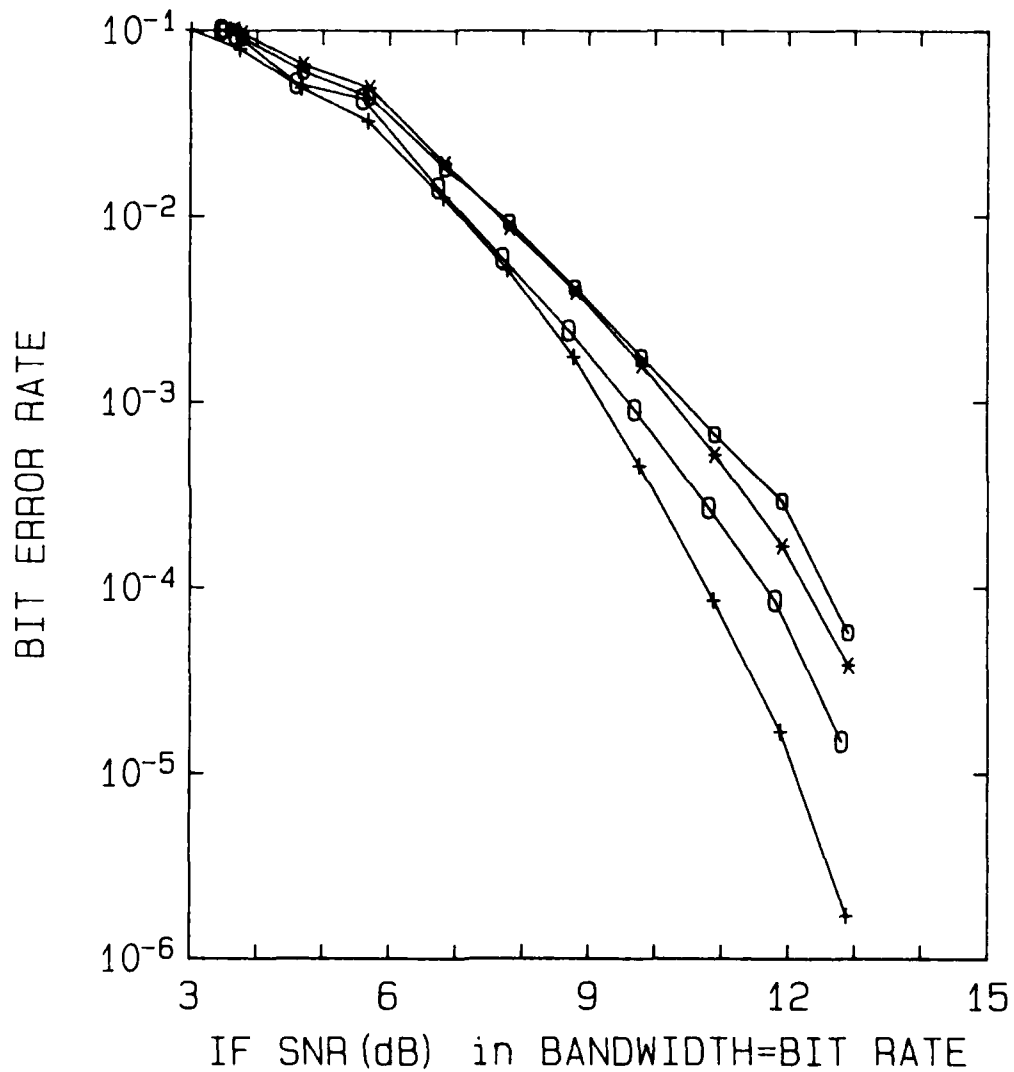


Figure 3.1-15. BER with Video and PREMOD BWs=0.5 and 1 Bit Rate.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	VIDEOL BIT kHz	DET
+ NRZ-L PCM/FM	1000	1000	700	CD	500 F/S
o NRZ-L PCM/FM	1000	1000	700	CD	750 F/S
* NRZ-L PCM/FM	1000	1000	700	CD	1000 F/S

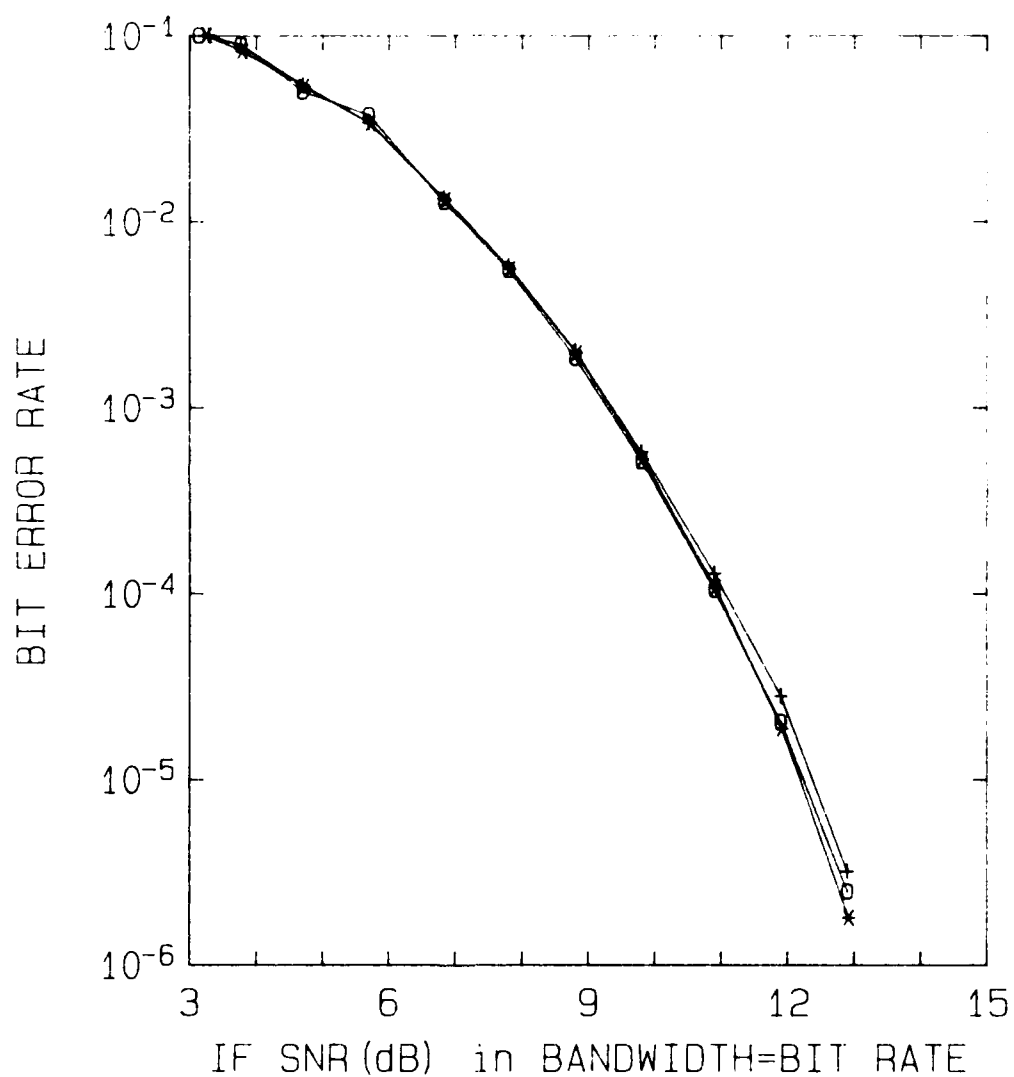


Figure 3.1-16. BER with Video BW=0.5, 0.75, and 1 Bit Rate.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	VIDEO BIT kHz	BIT DET
+ NRZ-L PCM/FM	1000	1500	700	CD	500	F/S
o NRZ-L PCM/FM	1000	1500	700	CD	750	F/S
* NRZ-L PCM/FM	1000	1500	700	CD	1000	F/S

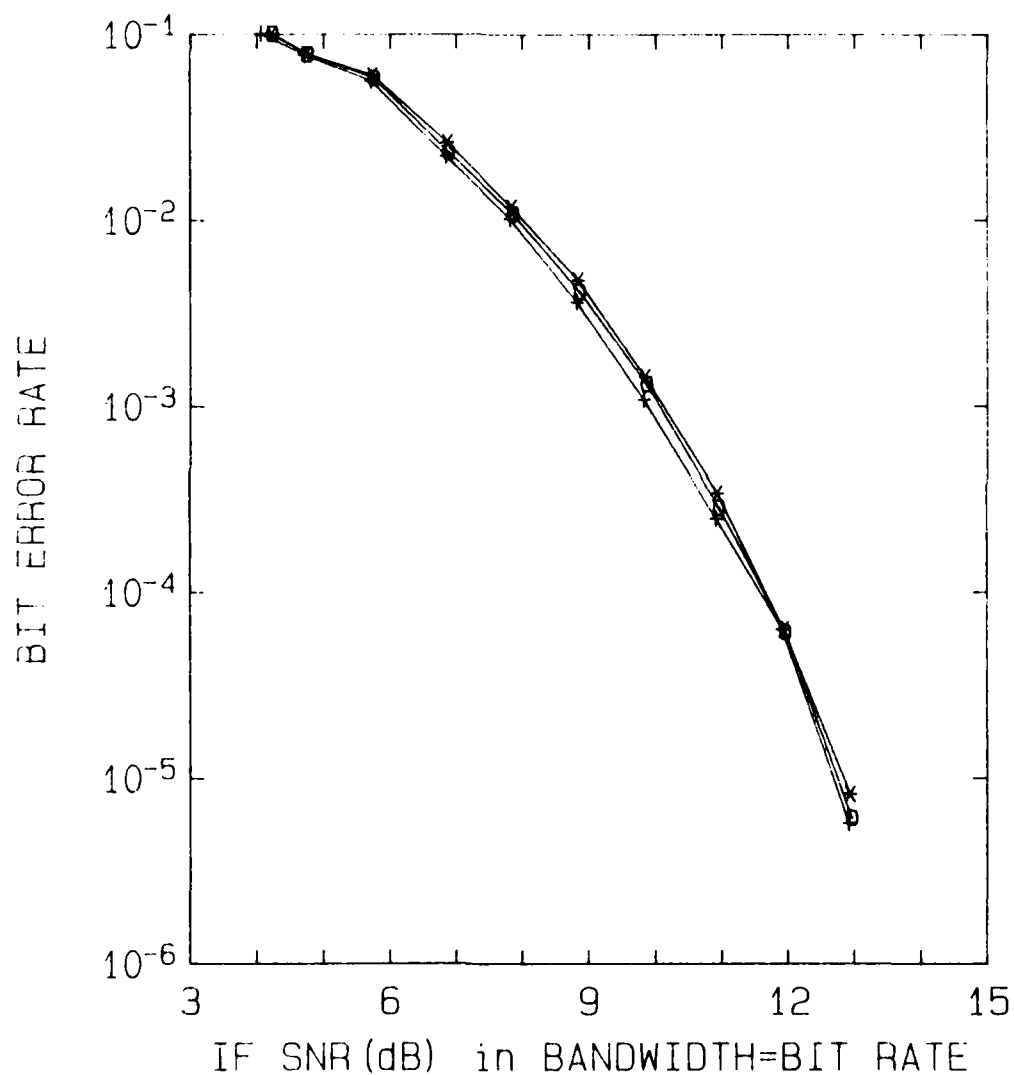


Figure 3.1-17. BER with Video BW=0.5, 0.75, and 1 Bit Rate.

excessive or very minimal filtering of the data. In the case involving excessive filtering of the PCM signal prior to the PCM bit synchronizer, a sample bit detector may provide the best results; however, most modern bit synchronizer systems do not provide a sample bit detector as an option. In the case of an essentially unfiltered PCM data stream, the integrate and dump (I/D) bit detector may provide improved performance over that of the sample bit detector selection. However, the difference in performance is nearly insignificant because most of the bit errors are the result of noise pops under the conditions involving a wide IF bandwidth relative to the bit rate and essentially no other filtering.

### 3.1.8 RF Spectra

The measured RF spectrum of pseudo-random (pseudo-noise (PN)) NRZ PCM/FM data using a peak deviation equal to 0.356 times the data bit rate (premodulation filter not used) is shown in figure 3.1-18. The frequency scale is relative to the center frequency for all RF spectral plots. Approximately 91% of the spectral power shown in figure 3.1-18 is contained in a bandwidth equal to the bit rate. The bandwidth containing 99% of the power (NTIA occupied bandwidth) is 1.42 MHz. This is equal to 1.78 times the bit rate. This value is quite close to the calculated value of 1.8 times the bit rate for rectangular NRZ PCM/FM with peak deviation equal to 0.35 times the bit rate listed by Korn.<sup>6</sup> The RF spectra for pseudo-random NRZ PCM/FM with peak deviation values corresponding to 0.1, 0.175, 0.25, 0.356, 0.42, 0.5, 0.71, and 1.0 times the bit rate are presented in figures 3.1-19 through 3.1-26, respectively. The premodulation filter used was a 5-pole linear phase filter with the -3 dB roll-off point at 800 kHz for all eight spectra. The 99% power bandwidth versus peak deviation is shown in table 3.1-1 for four of the peak deviations listed above.

The data presented in table 3.1-1 reveal that increasing the peak deviation from 0.356 times the bit rate to 0.42 times the bit rate increases the 99% power bandwidth by 11.6% and also increases the IRIG -60 dBc bandwidth by 6.4%. The IRIG -60 dBc bandwidth is defined as the bandwidth beyond which all components are 60 dB below the unmodulated carrier level when measured in a 3-kHz bandwidth. Doubling the peak deviation to 0.712 times the bit rate increases the 99% power bandwidth by 43.8% and increases the IRIG -60 dBc bandwidth by 45.1%.

The effect on the RF spectrum as a result of using a variety of premodulation filter types is shown in figures 3.1-22, and 3.1-27 through 3.1-33. The 99% power bandwidths, the IRIG -60 dBc bandwidths, and the percentage of the power in a bandwidth equal to the bit rate are shown in table 3.1-2.

<sup>6</sup>Korn, I. "Error Probability and Bandwidth of Digital Modulation," in *IEEE Transactions on Communications*, Vol. COM-28, pp. 287-290, February 1980.

800 kb/s NRZ-L PCM/FM 2047 BIT PN

PREMOD FILTER= NONE

PEAK DEVIATION= 285 kHz

RESOLUTION BW= 30 kHz VIDEO BW= 100 Hz

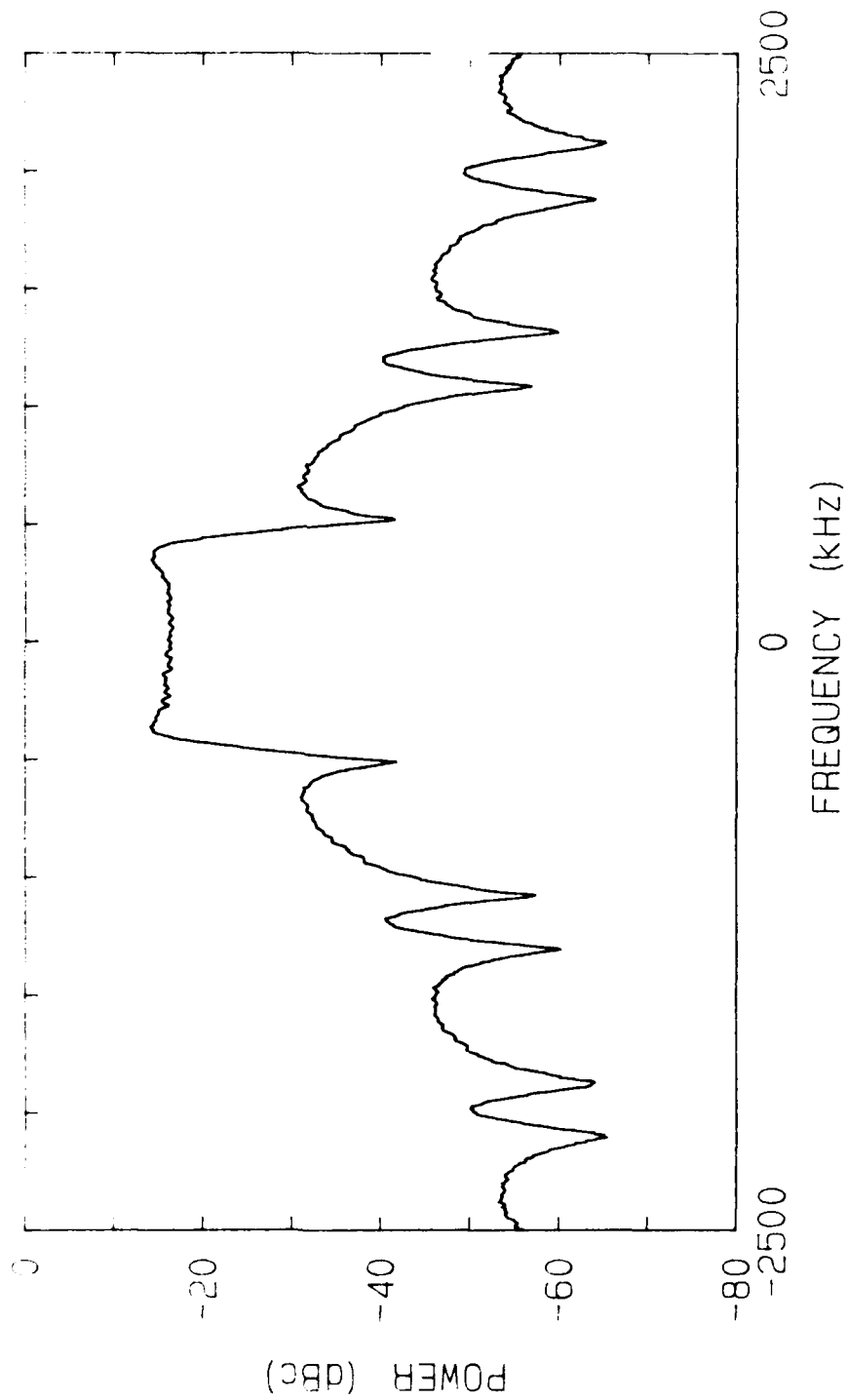


Figure 3.1-18. NRZ PCM/FM RF Spectrum (No PREMOD, Peak DEV=0.35 Bit Rate).

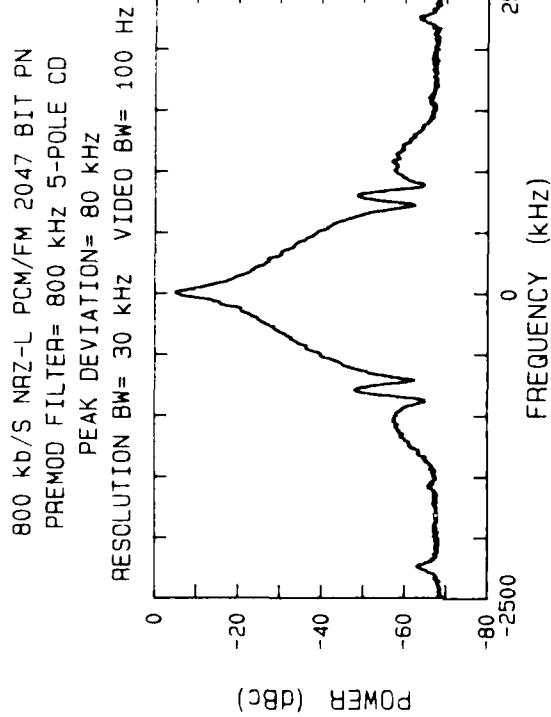


Figure 3.1-19. AF Spectrum PREMOD=800 kHz CD Peak DEV=0.1 Bit Rate. Figure 3.1-20. AF Spectrum PREMOD=800 kHz CD Peak DEV=0.175 Bit Rate.

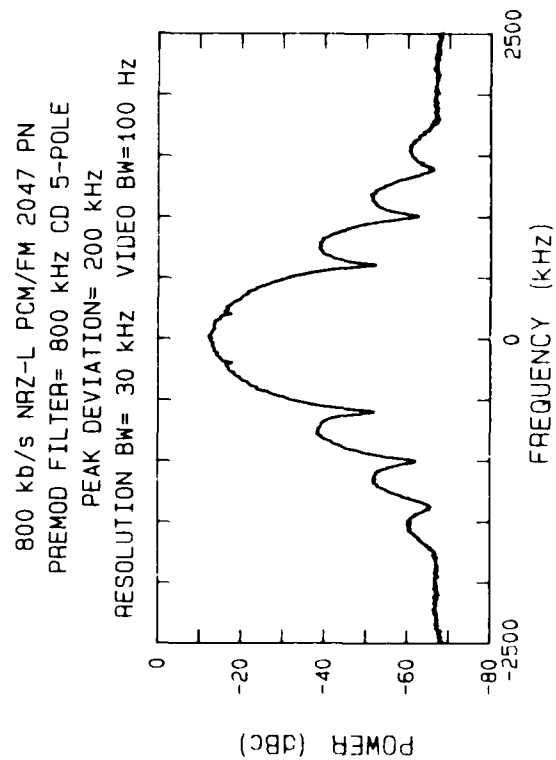
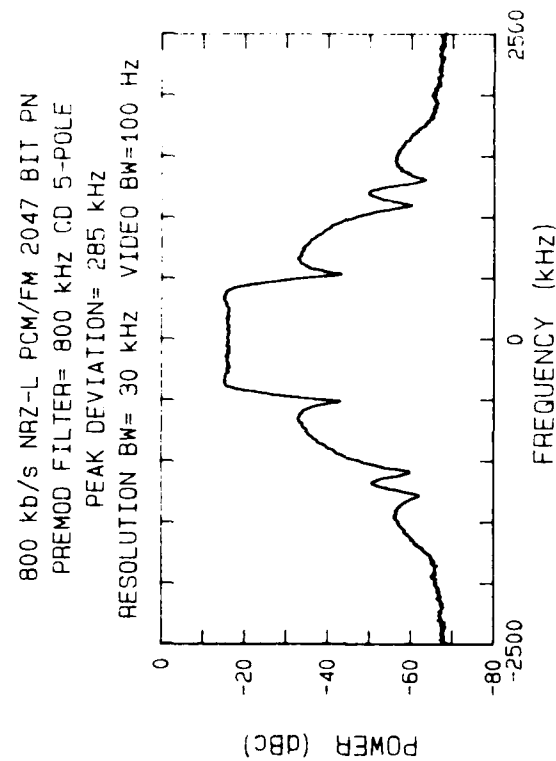
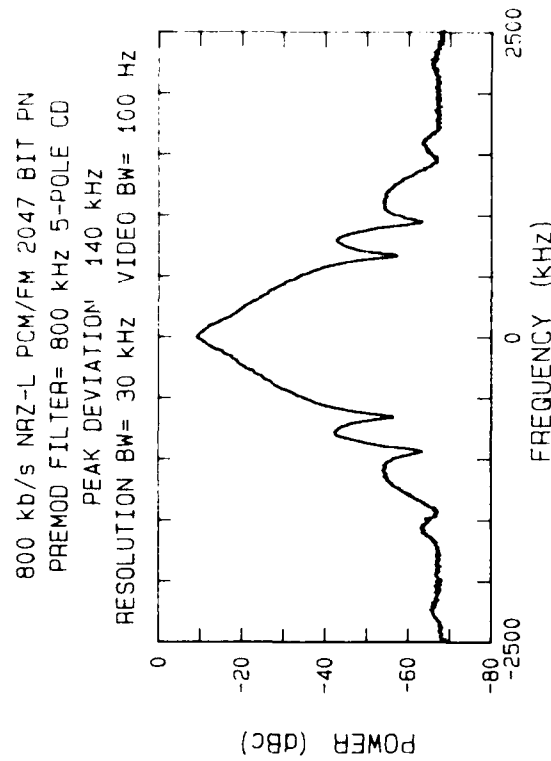


Figure 3.1-21. AF Spectrum PREMOD=800 kHz CD Peak DEV=0.25 Bit Rate. Figure 3.1-22. AF Spectrum PREMOD=800 kHz CD Peak DEV=0.35 Bit Rate.



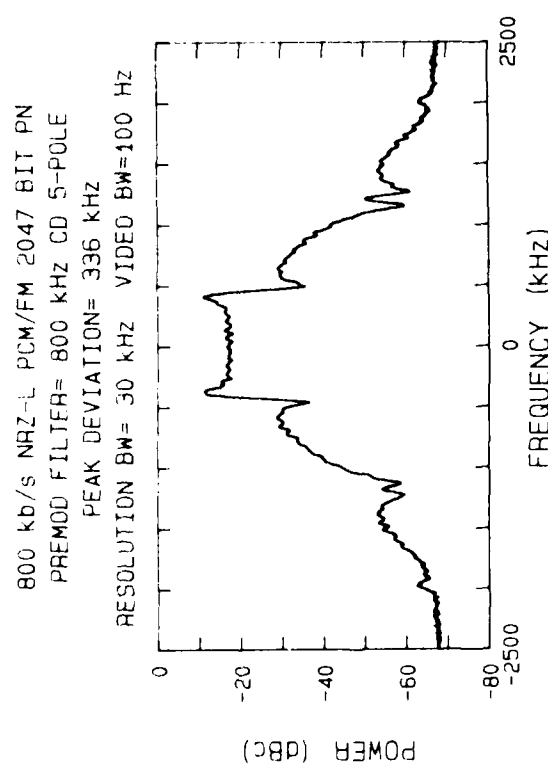


Figure 3.1-23. RF Spectrum PREMOD=800 kHz CD Peak DEV=0.42 Bit Rate.

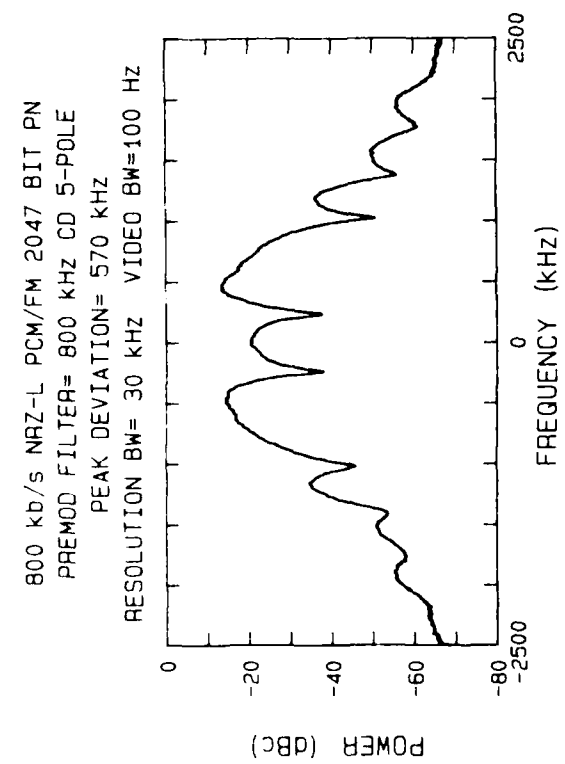


Figure 3.1-25. RF Spectrum PREMOD=800 kHz CD Peak DEV=0.71 Bit Rate.

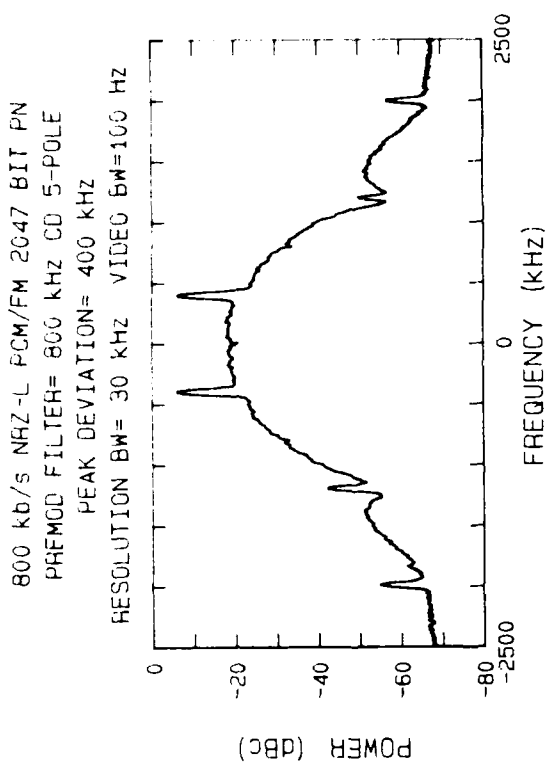


Figure 3.1-24. RF Spectrum PREMOD=800 kHz CD Peak DEV=0.50 Bit Rate.

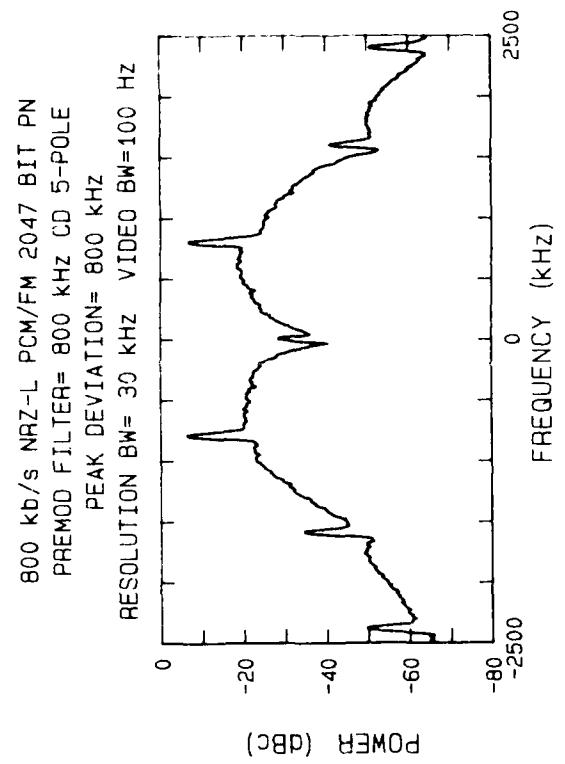


Figure 3.1-26. RF Spectrum PREMOD=800 kHz CD Peak DEV=1.00 Bit Rate.

Table 3.1-1. RF Spectral Characteristics for Various Peak Deviations.

800 kb/s NRZ-L PCM/FM 800 kHz 5-pole Linear Phase Premodulation Filter					
Peak Deviation kHz	/Bit Rate	99% Power Bandwidth kHz	/Bit Rate	IRIG -60 dBc Bandwidth (kHz)	% of Power in BW Equal to the Bit Rate
200	0.25	900	1.13	1910	97.6
285	0.356	1210	1.51	2040	92.0
336	0.42	1350	1.69	2170	83.7
570	0.712	1740	2.18	2960	23.7

Table 3.1-2. RF Spectral Characteristics for Various Premodulation Filters.

800 kb/s NRZ-L PCM/FM 285 kHz Peak Deviation					
Premodulation Bandwidth (kHz)	Type	99% Power Bandwidth kHz	/Bit Rate	IRIG -60 dBc Bandwidth (kHz)	% of Power in BW Equal to the Bit Rate
None		1420	1.78	4010	91.0
800	CD	1210	1.51	2040	92.0
800	CA	1330	1.66	2390	90.6
560	CD	930	1.16	2010	93.9
560	CA	950	1.19	2020	93.5
400	CD	890	1.11	1860	95.6
400	CA	890	1.11	1830	95.5
800	RC	1200	1.50	2500	92.6
560	RC	940	1.18	2500	93.7



800 kb/s NRZ-L PCM/FM 2047 BIT PN  
PREMOD FILTER= 800 kHz CA 5-POLE  
PEAK DEVIATION= 285 kHz  
RESOLUTION BW= 30 kHz VIDEO BW=100 Hz

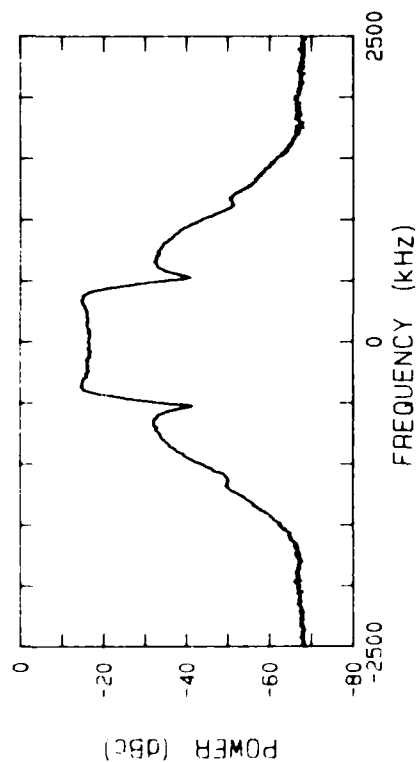


Figure 3.1-27. AF Spectrum PREMOD=800 kHz CA Peak DEV=0.35 Bit Rate.

800 kb/s NRZ-L PCM/FM 2047 BIT PN  
PREMOD FILTER= 560 kHz CA 5-POLE  
PEAK DEVIATION= 285 kHz  
RESOLUTION BW= 30 kHz VIDEO BW=100 Hz

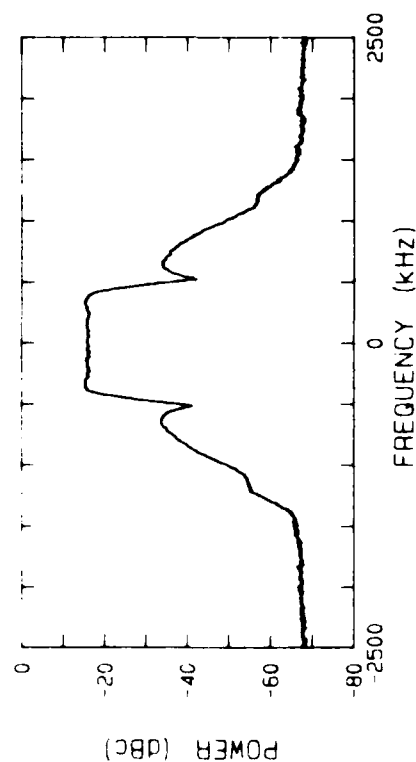


Figure 3.1-29. AF Spectrum PREMOD=560 kHz CA Peak DEV=0.35 Bit Rate.

800 kb/s NRZ-L PCM/FM 2047 BIT PN  
PREMOD FILTER= 560 kHz CD 5-POLE  
PEAK DEVIATION= 285 kHz  
RESOLUTION BW= 30 kHz VIDEO BW=100 Hz

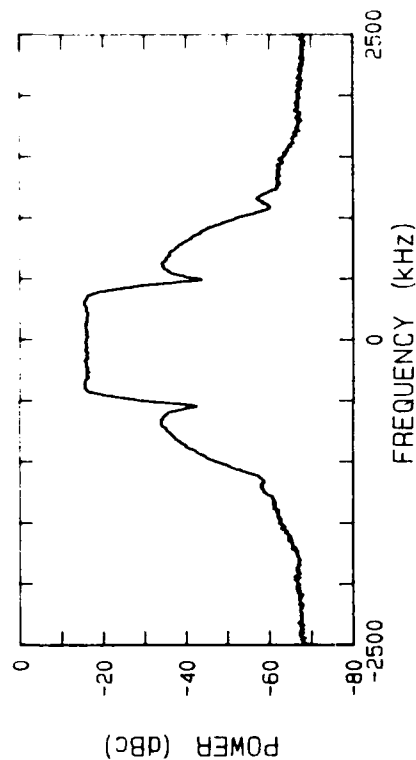


Figure 3.1-28. AF Spectrum PREMOD=560 kHz CD Peak DEV=0.35 Bit Rate.

800 kb/s NRZ-L PCM/FM 2047 BIT PN  
PREMOD FILTER= 400 kHz CD 5-POLE  
PEAK DEVIATION= 285 kHz  
RESOLUTION BW= 30 kHz VIDEO BW=100 Hz

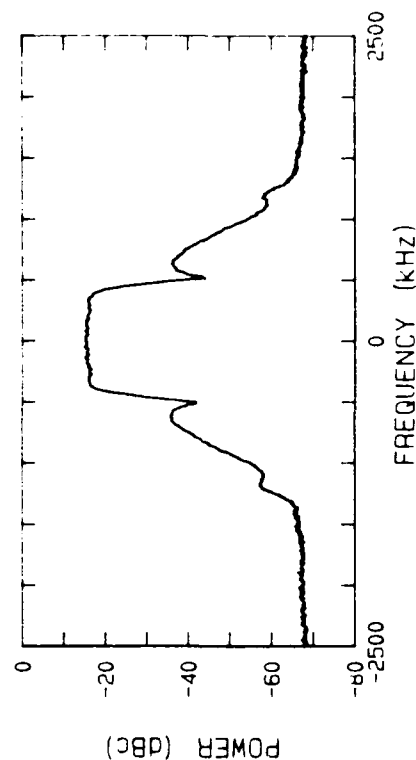


Figure 3.1-30. AF Spectrum PREMOD=400 kHz CD Peak DEV=0.35 Bit Rate.

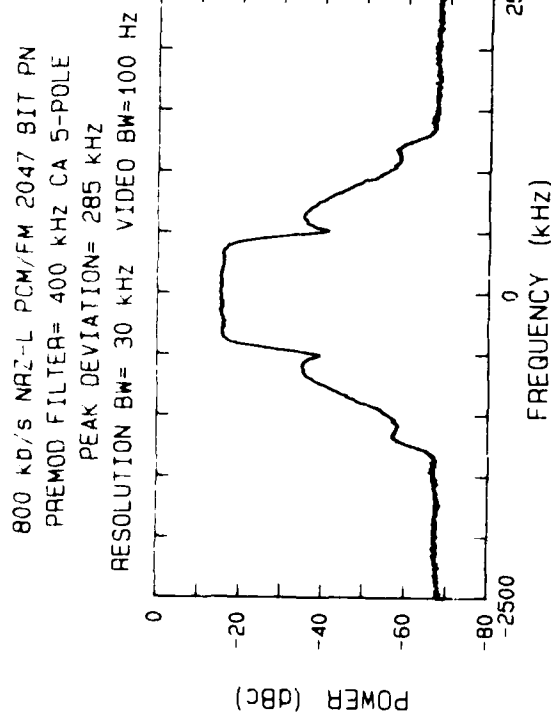


Figure 3.1-31. RF Spectrum PREMOD=400 kHz CA Peak DEV=0.35 Bit Rate.

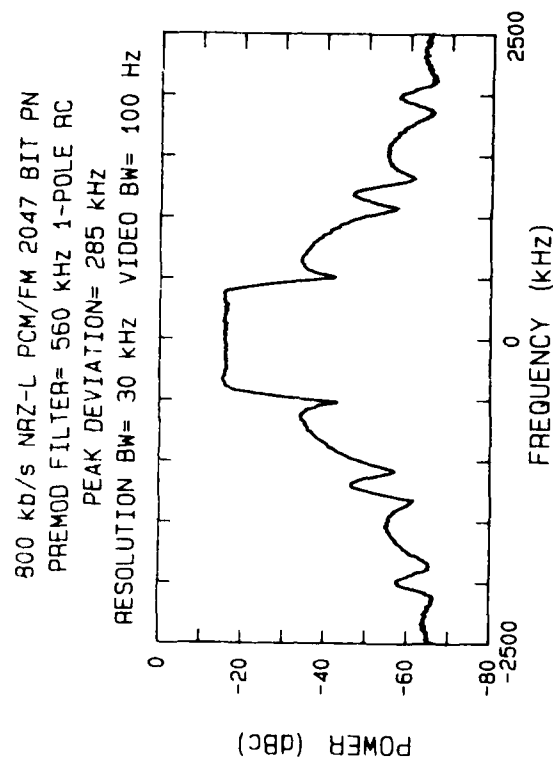


Figure 3.1-33. RF Spectrum PREMOD=560 kHz RC Peak DEV=0.35 Bit Rate.

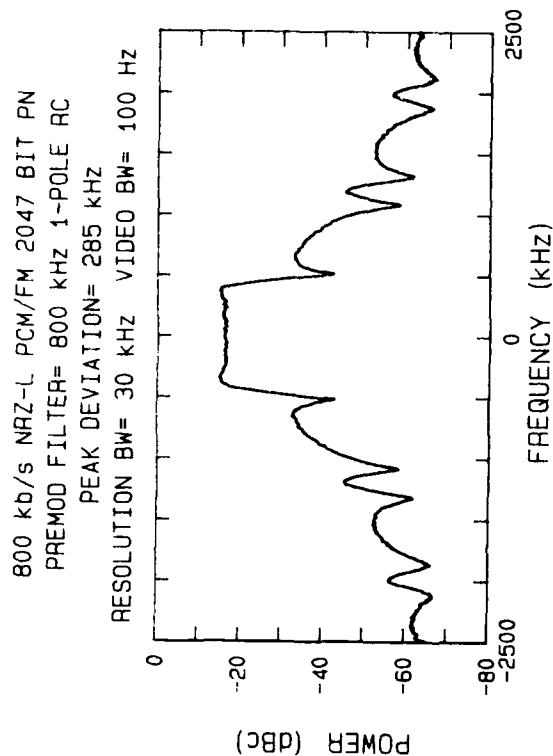


Figure 3.1-32. RF Spectrum PREMOD=800 kHz RC Peak DEV=0.35 Bit Rate.

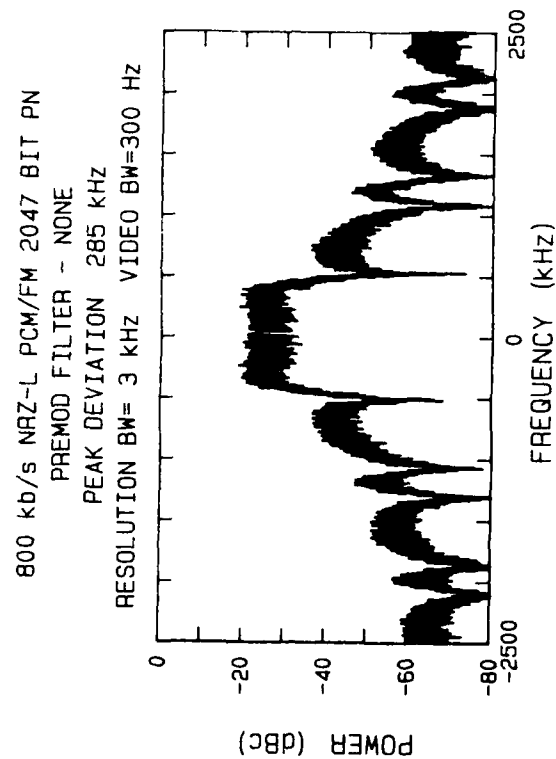


Figure 3.1-34. RF Spectrum PREMOD=None Peak DEV=0.35 Bit Rate (3 kHz).

The data in table 3.1-2 reveal that the 99% power bandwidth is usually narrower with a Bessel (constant delay (CD)) premodulation filter than with a Butterworth (constant amplitude (CA)) filter. The wider bandwidth is partially the result of the much larger overshoot of the Butterworth filter. The frequency deviation caused by the overshoot exceeds the nominal peak deviation (in this case 285 kHz) which is defined as the peak deviation without overshoot. The Bessel filter also attenuates signals below the -3 dB cutoff more than the Butterworth filter; however, outside the passband of the filter characteristic (above the -3 dB cutoff), the opposite is true. The 99% power bandwidth and the percentage of power in a bandwidth equal to the bit rate agree quite closely for the 5-pole Bessel and the 1-pole RC premodulation filters. It should be noted however, that the IRIG -60 dBc bandwidth is significantly narrower for the 5-pole Bessel filter than for the 1-pole RC filter. The reason for the differences in the response of the filters is that the 1-pole RC filter attenuation increases significantly more slowly than the attenuation of the Bessel filter at frequencies above the -3 dB point. The attenuation of the two filters is similar at frequencies below the -3 dB cutoff point.

All of the RF spectra presented in figures 3.1-18 through 3.1-33 were recorded with a spectrum analyzer resolution bandwidth of 30 kHz. The IRIG Standards specify a 3-kHz bandwidth for spectral occupancy measurements. Figure 3.1-34 is similar to figure 3.1-18 except the resolution bandwidth has been decreased to 3 kHz and the video bandwidth increased to 300 Hz. The sweep time in figure 3.1-34 was 15 seconds; while the sweep time in figure 3.1-18 was 5 seconds. In order to increase the statistical accuracy of figure 3.1-34 to the level of accuracy of figure 3.1-18 would require that the sweep time be 500 seconds. Therefore, the 30-kHz resolution bandwidth was chosen for the spectral displays in these descriptions. To convert the spectral amplitudes between the two filter bandwidths, it is necessary to subtract 10 dB ( $10 \log 3/30$ ) from the 30-kHz value if the input is white noise. When the input contains discrete frequency components (delta functions in the frequency domain), the amplitude at the output of both filters would be the same; this assumes only one discrete component within the passband of the widest filter. Therefore, if discrete spectral components are not present, -50 dBc with a 30-kHz spectrum analyzer bandpass filter is essentially the same as -60 dBc with a 3-kHz bandpass filter. In reality, many discrete spectral components are present in this case, but the sum of many discrete spectral components looks like noise as far as the bandpass filter is concerned. In this case, it is not possible to extend the extrapolation to a 100-Hz bandpass filter because the spectral components are spaced every  $800,000/2047$  Hz or approximately 391 Hz apart. Therefore, a 100-Hz bandpass filter would resolve the individual components.

Figures 3.1-35 and 3.1-36 show the spectra that result when the bit stream contains a repeating 16-bit word. The 16-bit word for figure 3.1-35 was "1111000100110100," which is a 15-bit pseudo-noise sequence with a zero added at the end for symmetry. The 16-bit word for figure 3.1-36 was "101000100010000," which is the word from figure 3.1-35 with every other "1" converted to a "0." The spectrum in figure 3.1-36 is obviously not symmetrical. The spectrum in figure 3.1-35 is somewhat symmetrical, but there are significant differences between the upper and lower halves of the spectrum. In general, FM spectra are not symmetrical unless the input to the FM modulator is symmetrical. For example, a single sine wave modulating an FM generator produces a symmetrical RF spectrum.

800 kb/s NRZ-L PCM/FM 16 BIT WORD  
PREMOD FILTER= 800 KHZ CD 5-POLE  
PEAK DEVIATION= 285 KHZ

RESOLUTION BW= 30 KHZ VIDEO BW=100 HZ

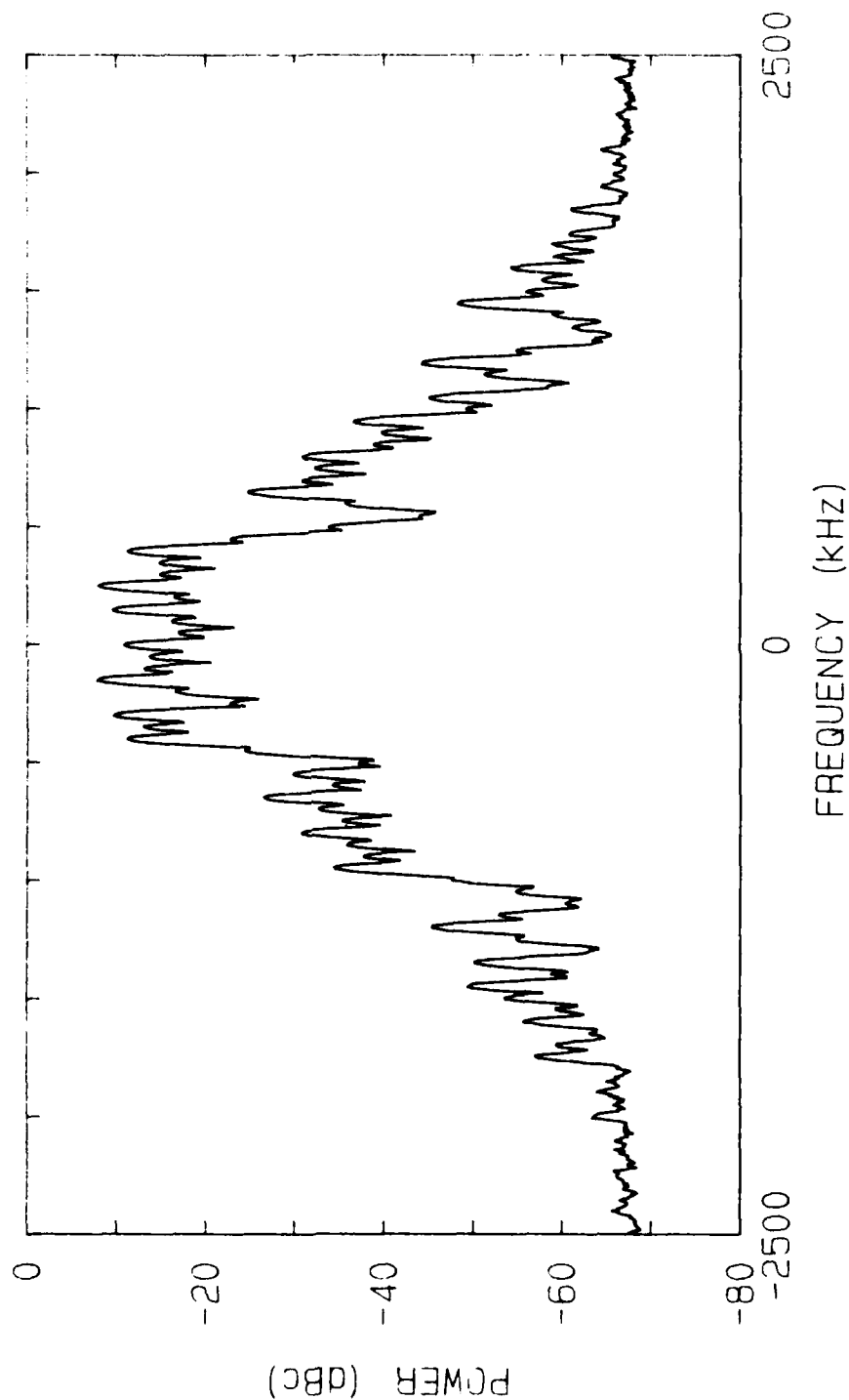


Figure 3.1-35. NRZ PCM/FM RF Spectrum with Repeated 16-Bit Word.

500 KD/s NRZ- PCM/FM 12-'0' 4-'1'  
PREVISE FILTER= 800 KHZ CD 5-POLE

PEAK DEVIATION= 285 KHZ

RESOLUTION BW= 30 KHZ VIDEO BW=100 HZ

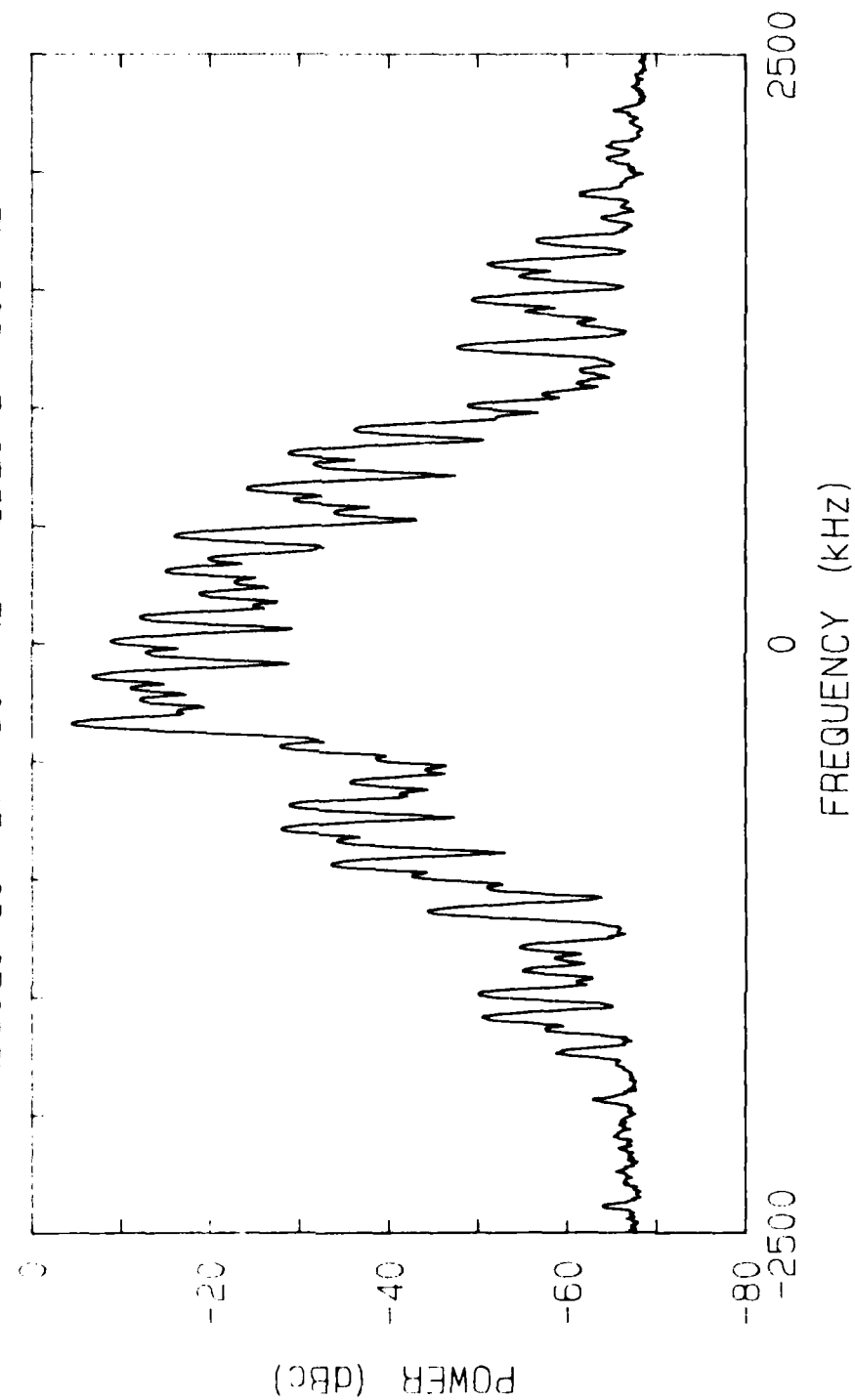


Figure 3.1-36. NRZ PCM/FM RF Spectrum with Repeated 16-Bit Word (3/4 Zeroes).

## 3.2 BIPHASE PCM/FM

### 3.2.1 Introduction

Biphase pulse code modulation/frequency modulation (PCM/FM) is a method used to send digital data over a transmission link. The most commonly used code for biphase PCM/FM is the level (-L) code. This code represents a ONE by a high level for the first half of the bit time and a low level for the second half of the bit time. A ZERO is the exact opposite of a ONE. The advantages of biphase PCM/FM over NRZ PCM/FM include:

1. Biphase has no DC component; therefore, AC-coupled transmitters can be used.
2. Biphase has at least one transition every bit period. This makes bit synchronization easier.

The disadvantages of biphase PCM/FM compared to NRZ PCM/FM include:

1. Biphase PCM/FM requires approximately twice the bandwidth of NRZ PCM/FM.
2. Biphase PCM/FM requires approximately 3 dB more IF SNR in a bandwidth equal to the bit rate for the same BER, compared to NRZ PCM/FM.

### 3.2.2 Selection of Peak Deviation

The optimum peak deviation for biphase PCM/FM is approximately 0.65 times the bit rate; i.e., a 1.0-Mb/s bit stream should have a peak deviation of 650 kHz and a peak-to-peak deviation of 1,300 kHz.<sup>7</sup> This optimum value of peak deviation is valid when using IF bandwidths that are between 1.8 and 4 times the bit rate and for systems where the incidental FM is much less than the peak deviation. If the predetection bandwidth is wider than four times the bit rate, the optimum peak deviation is greater than 0.65 times the bit rate (see figure 3.2-1). If the predetection bandwidth is much wider than the bit rate, biphase PCM/FM will usually be a better choice than biphase PCM/FM because of its better BER versus IF SNR performance. The BER versus IF SNR performance of biphase PCM/FM is shown in figures 3.2-2 and 3.2-3 for peak deviations equal to 0.50, 0.65, and 0.80 times the bit rate and IF bandwidths of two and three times the bit rate. The IF SNR in a bandwidth equal to the bit rate for a  $10^{-4}$  BER was 13.5 dB for an IF bandwidth equal to twice the bit rate and 14.4 dB for an IF bandwidth equal to three times the bit rate with a peak deviation equal to 0.65 times the bit rate.

<sup>7</sup>Tan, C. H., T. T. Tjhung, and H. Singh, "Performance of Narrow-Band Manchester Coded FSK With Discriminator Detection," in *IEEE Transactions on Communications* Vol. COM-31, pp. 659-667 May 1983

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMCD kHz	TYPE	PEAK DEV	BIT DET
+ B10-L PCM/FM	500	3000	1000	CD	325	
o B10-L PCM/FM	500	3000	1000	CD	950	
* B10-L PCM/FM	500	1000	1000	CD	325	

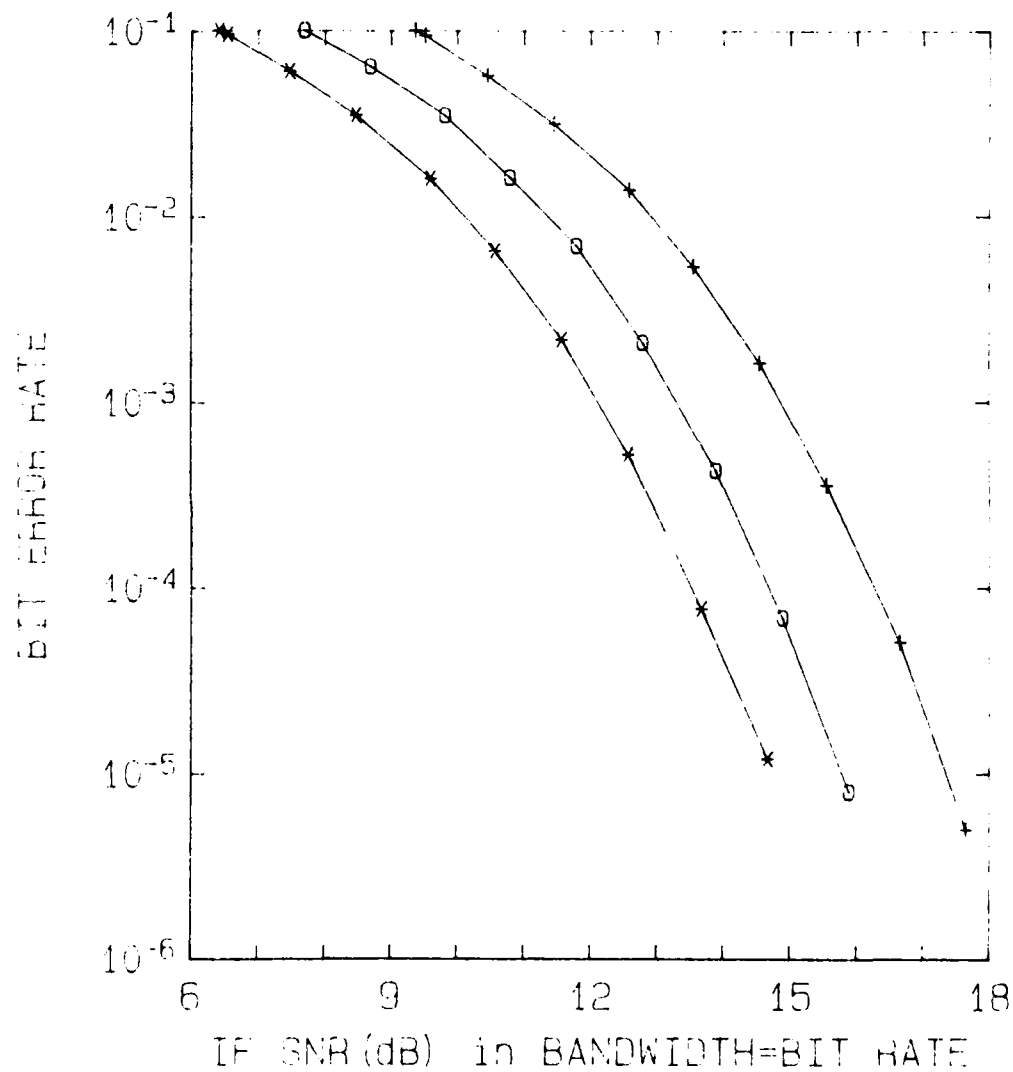


Figure 3.2-1. BER for IF BW = 2 and 6 Times Bit Rate.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	PEAK DEV	BIT DET
+ BIØ-L PCM/FM	500	1000	1000	CD	250
o BIØ-L PCM/FM	500	1000	1000	CD	400
* BIØ-L PCM/FM	500	1000	1000	CD	325

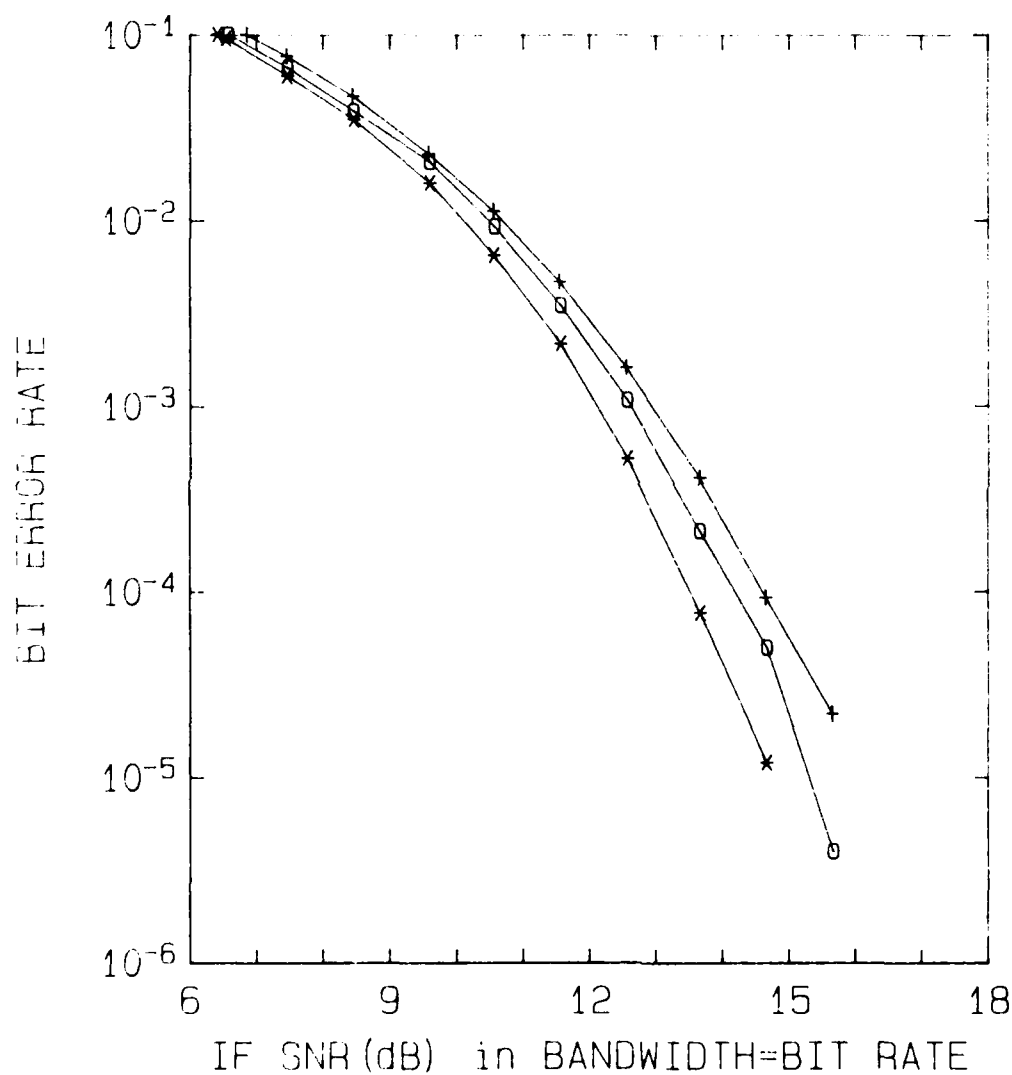


Figure 3.2-2. BER for Peak DEV=0.5, 0.65, and 0.8 Bit Rate.



MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	PEAK DEV	BIT DET
+ BIØ-L PCM/FM	500	1500	700	CD	250
o BIØ-L PCM/FM	500	1500	700	CD	400
* BIØ-L PCM/FM	500	1500	700	CD	325

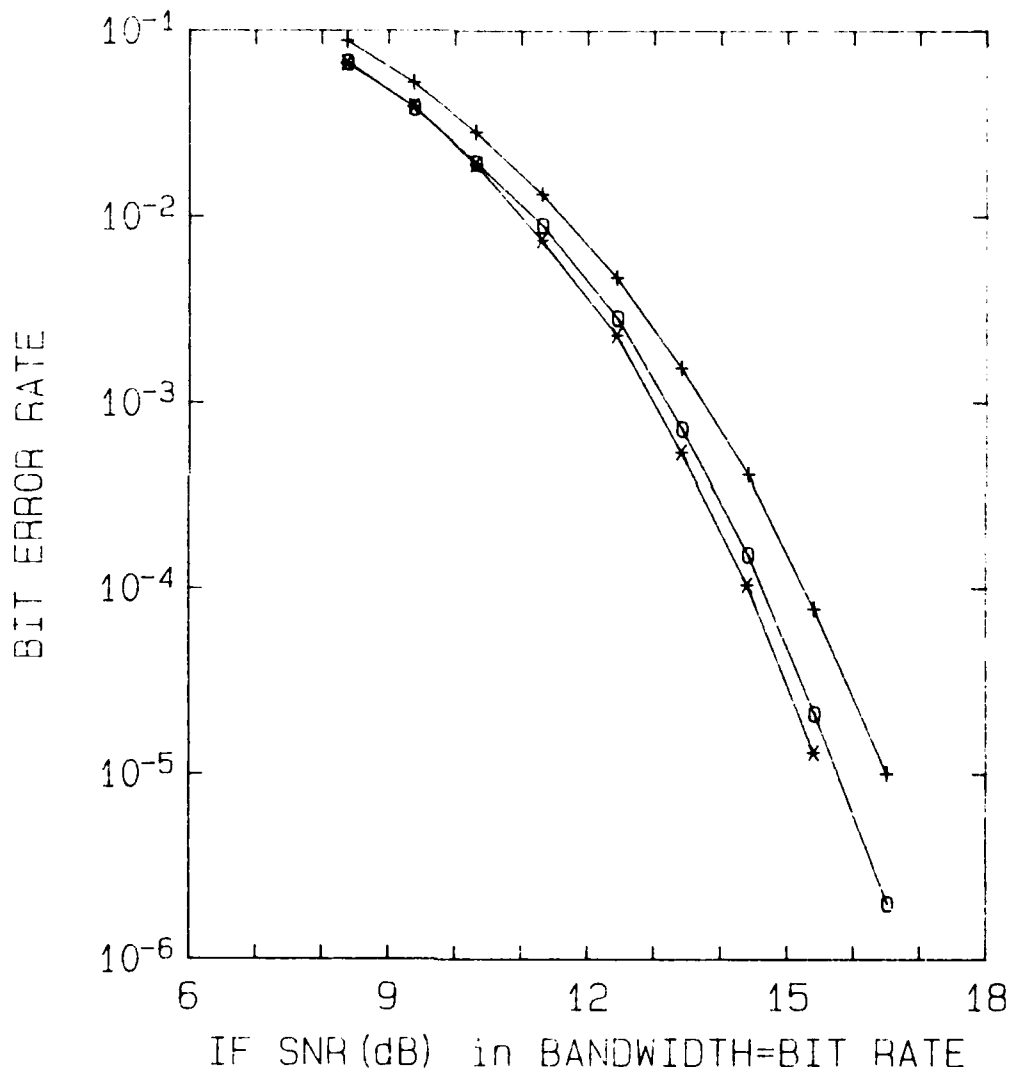


Figure 3.2-3. BER for Peak DEV = 0.5, 0.65, and 0.8 Bit Rate.

### 3.2.3 Selection of Premodulation Filter

The best premodulation filter is the widest filter that allows the RF spectral occupancy requirements to be met. A low-pass filter with a -3 dB bandwidth equal to or greater than 1.4 times the bit rate will not cause a significant increase in the BER (see figure 3.2-4). The use of a premodulation filter bandwidth equal to the bit rate degrades the data quality by at least 1 dB for BERs of  $10^{-4}$  (and lower). The BER versus IF SNR performance is essentially the same with linear phase and constant amplitude premodulation filters.

### 3.2.4 Selection of Receiver IF Bandwidth

The optimum receiver IF bandwidth is equal to approximately two times the bit rate for biphase level PCM/FM. Reference 7 lists an optimum IF bandwidth of 1.8 times the bit rate. The variation of BER with the ratio of IF bandwidth to bit rate is illustrated in figure 3.2-5. The IF bandwidth was fixed at 1,000 kHz (actually measured to be approximately 1,100 kHz) and the bit rate, premodulation filter bandwidth, and peak deviation were varied. The premodulation filter bandwidth was set to twice the bit rate and the peak deviation was set to 0.65 times the bit rate. For BERs between  $10^{-4}$  and  $10^{-5}$ , the performance at 500 and 600 kb/s was essentially the same and better than the performance at 400 and 700 kb/s. The ratio of measured IF bandwidth to bit rate was approximately 2.2 and 1.8 for 500 and 600 kb/s, respectively. This supports the optimum IF bandwidth setting of approximately twice the bit rate. Figure 3.2-6 shows the BER versus IF SNR performance for bandwidths equal to 2, 3, and 6 times the bit rate. The use of excessively wide IF filters with predetection recording should be avoided. The IF filter should not be wider than two times the predetection carrier frequency. Also, the biphase bit rate should not exceed one-half of the predetection carrier frequency.

### 3.2.5 Selection of Demodulator Video Bandwidth

The demodulator video bandwidth should not be set to a value less than the bit rate. There is very little difference in BER performance between video filters with bandwidths between one and three times the bit rate.

### 3.2.6 Selection of PCM Bit Synchronizer Bit Detector

Most PCM bit synchronizers do not offer a choice of bit detector type for biphase signals.

### 3.2.7 RF Spectra

Sample biphase level PCM/FM RF spectra are shown in figures 3.2-7 through 3.2-12. These spectra have spikes at the center frequency and also at multiples of the bit rate on both sides of the center frequency. The occupied bandwidth is six times the bit rate for premodulation filter bandwidths equal to the bit rate and also for a constant amplitude premodulation filter with a bandwidth equal to twice the bit rate for the optimum peak deviation. The occupied bandwidth is equal to eight times the bit rate with a constant delay premodulation filter bandwidth equal to twice the bit rate and the optimum peak deviation. The filters used for these spectral plots were 5-pole low-pass filters.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	PREMOD TYPE	PEAK DEV	BIT DET
+ BI <del>0</del> -L PCM/FM	500	1000	500	CD	325	
o BI <del>0</del> -L PCM/FM	500	1000	700	CD	325	
* BI <del>0</del> -L PCM/FM	500	1000	1000	CD	325	

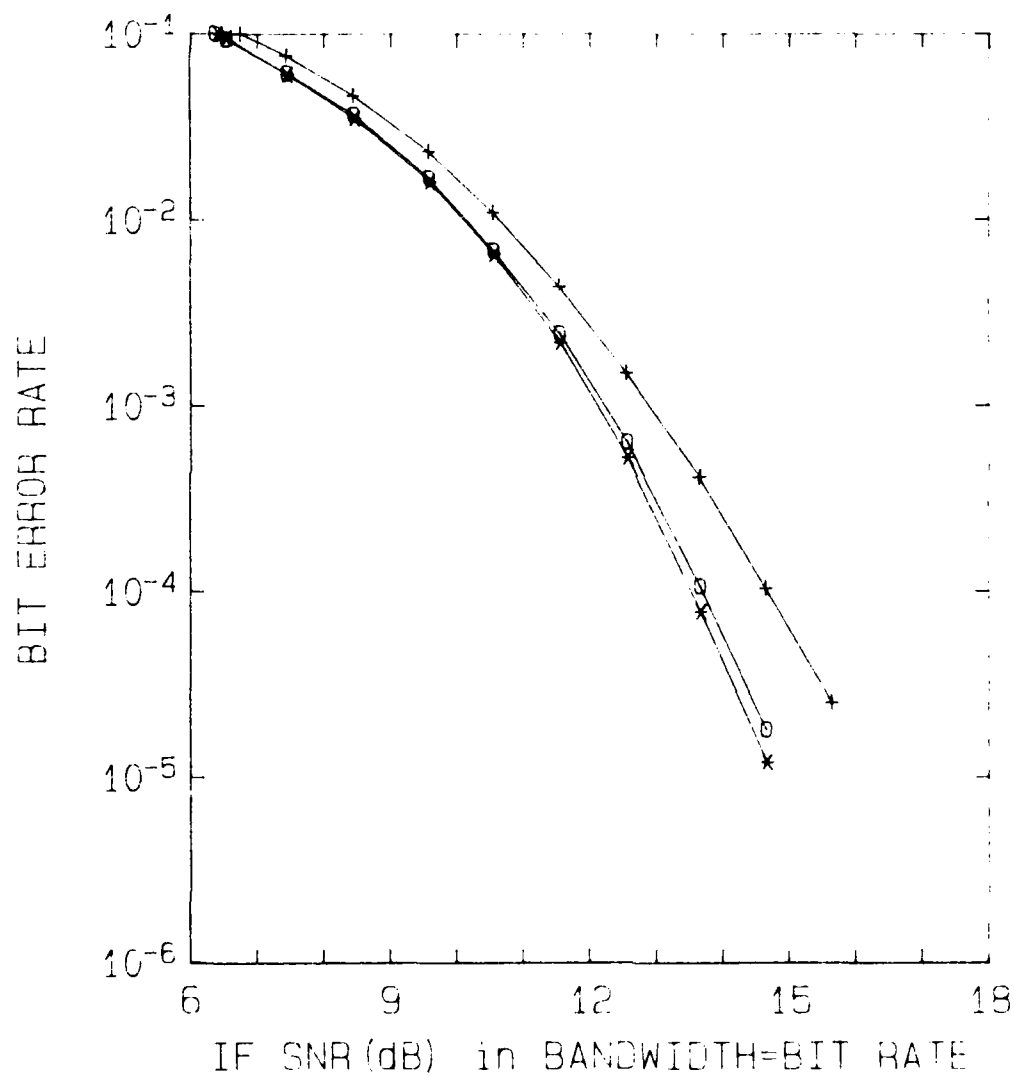


Figure 3.2-4. BER for PREMOD BW = 1, 1.4, and 2 Bit Rate.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
0 BI <del>2</del> -L PCM/FM	700	1000	1400	CD	455	
+ BI <del>2</del> -L PCM/FM	600	1000	1200	CD	390	
o BI <del>2</del> -L PCM/FM	500	1000	1000	CD	325	
* BI <del>2</del> -L PCM/FM	400	1000	800	CD	260	

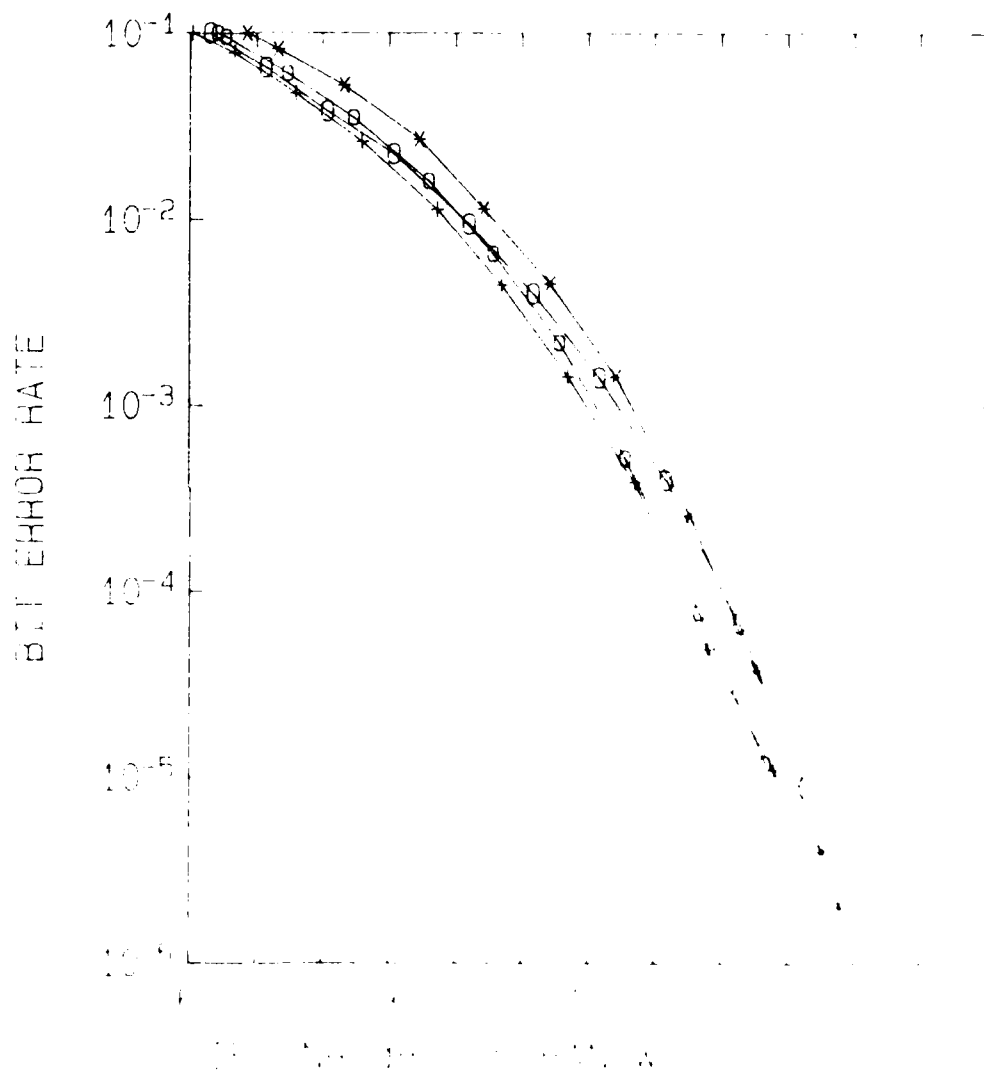


Figure 3.2-1. BER vs. SNR for various modulation schemes.

MODULATION TYPE	BIT RATE kb/s	IF BW KHz	PREMOD KHz TYPE	PEAK DEV	BIT DET
--------------------	------------------	--------------	--------------------	-------------	------------

+ B12-L FM FM	800	3000	1000 CD	325	
0 B12-L FM FM	500	1500	1000 CD	325	
* B12-L FM FM	800	1000	1000 CD	325	



IF BW bit Rate = 2, 3, and 6.

400 kb/s BIPHASE PCM/FM 2047 BIT PN

PREMOD FILTER= 800 kHz CD

PEAK DEVIATION= 260 kHz

RESOLUTION BW= 30 kHz VIDEO BW= 100 Hz

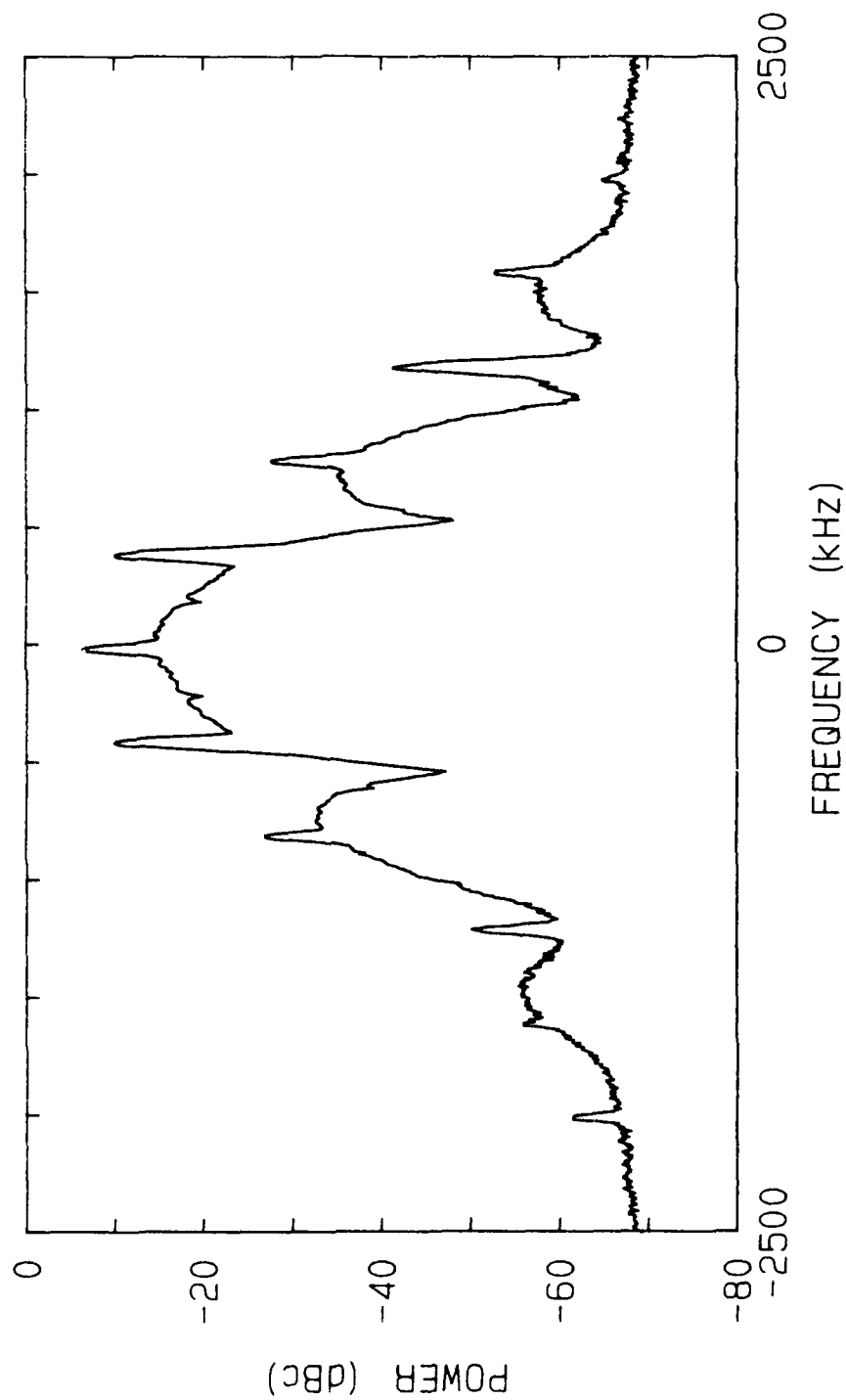


Figure 3.2-7. Biphase PCM/FM RF Spectrum (PREMOD=800 kHz CD, DEV=0.65 Bit Rate).

400 kb/s BIPHASE PCM/FM 2047 BIT PN  
PREMOD FILTER= 800 kHz CD  
PEAK DEVIATION= 200 kHz  
RESOLUTION BW= 30 kHz VIDEO BW= 100 Hz

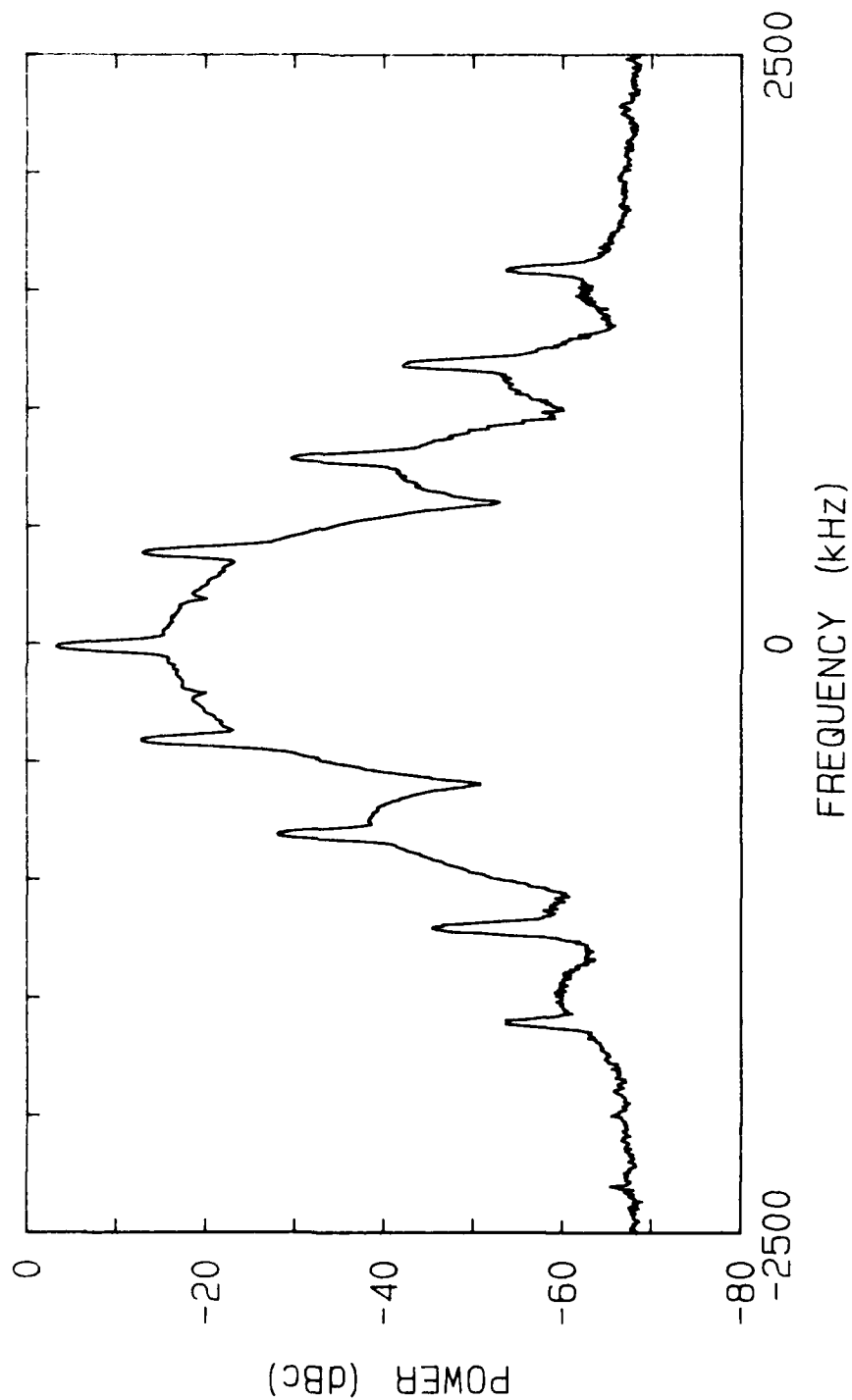


Figure 3.2-8. Biphase PCM/FM RF Spectrum (PREMOD=800 kHz CD, DEV=0.50 Bit Rate).

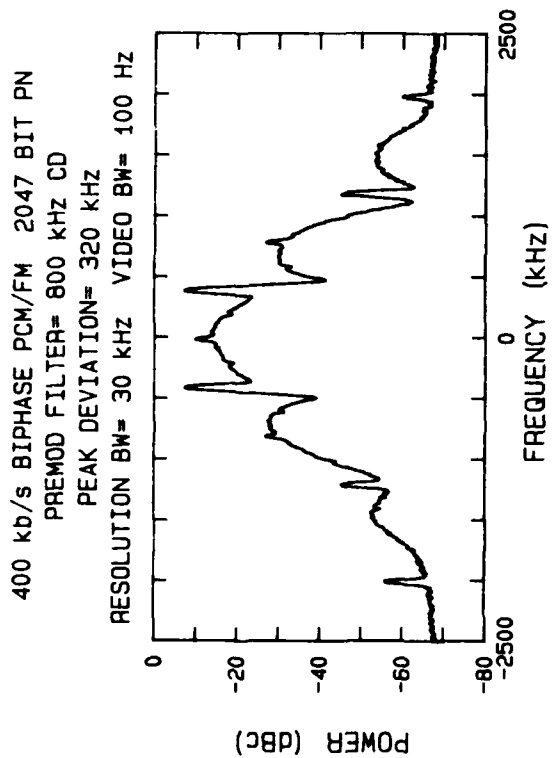


Figure 3.2-9. RF Spectrum PREMOD=800 kHz CD Peak DEV=0.80 Bit Rate.

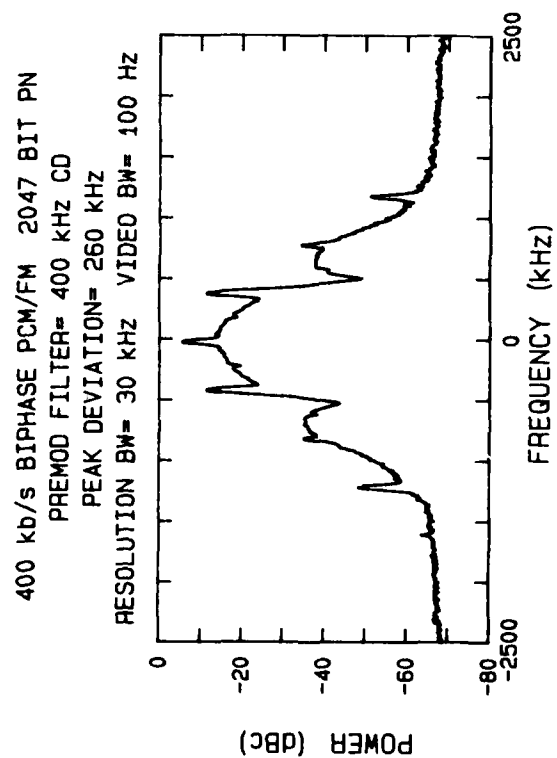


Figure 3.2-11. RF Spectrum PREMOD=400 kHz CD Peak DEV=0.65 Bit Rate.

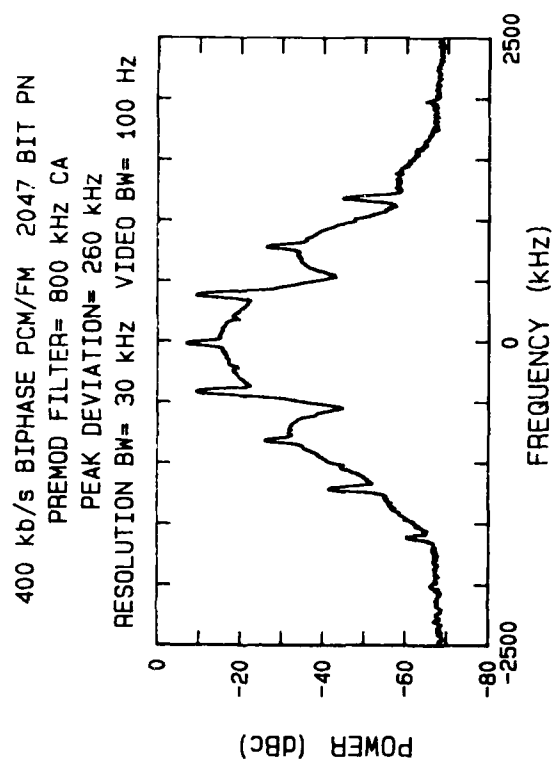


Figure 3.2-10. RF Spectrum PREMOD=800 kHz CA Peak DEV=0.65 Bit Rate.

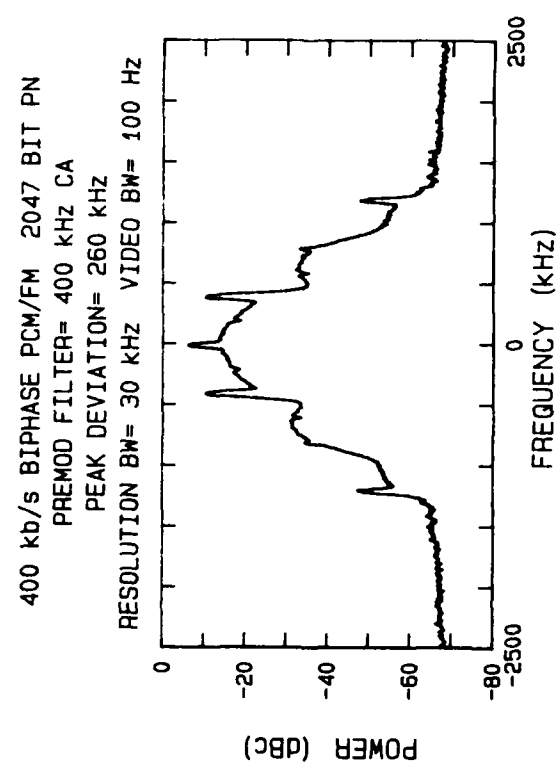


Figure 3.2-12. RF Spectrum PREMOD=400 kHz CA Peak DEV=0.65 Bit Rate.



### 3.3 NRZ PCM/PM

#### 3.3.1 Introduction

Pulse code modulation/phase modulation with 90 degree peak deviation (PCM/PM (90)) is a method of sending digital data over a transmission link where the carrier phase is shifted +90 degrees to represent one state of a binary signal, and shifted -90 degrees to represent the other state of the binary signal. The most commonly used codes for NRZ PCM/PM (90) are the mark (M) and space (S) codes. The use of the mark and space codes is often called differential encoding because the information is contained in the transitions rather than the levels. The mark and space codes are used because the demodulated output signal when a carrier recovery loop is used has a 180° ambiguity because changing the sign of the received signal does not change the sign of the recovered carrier<sup>8</sup>. Since the NRZ-M and NRZ-S codes are polarity insensitive, the unknown polarity does not matter.

Bit errors in NRZ PCM/PM (90) are caused by the effects of additive, white, Gaussian noise plus intersymbol interference, timing errors, etc. This makes it relatively simple to derive an expression for the bit error rate as follows:

$$\text{BER} = 1/2 \operatorname{erfc} \left( (E_b/N_0)^{1/2} \cos \phi \right)$$

Where:

- $E_b$  is the signal energy per bit
- $N_0$  is the noise power spectral density (watts/Hz)
- $\phi$  is the carrier recovery loop tracking error
- erfc is the complementary error function.

Note that this expression assumes unfiltered NRZ-L data and ideal bit detection. The BER for NRZ-M and NRZ-S is approximately twice the BER listed above because each isolated erroneous level causes a transition error on each side of the erroneous level.

#### 3.3.2 Selection of Peak Deviation

The peak carrier deviation that produces the minimum bit error rate is a function of the premodulation filter, the demodulator type and loop bandwidth, and the bit pattern. The bit error rate is relatively insensitive to small changes in the peak deviation. A change in peak deviation from 90 degrees to 100 degrees (or 80 degrees) with no premodulation filtering requires a 0.13 dB (theoretical value) higher SNR to produce the same BER. Figures 3.3-1 through 3.3-5 present BER data versus IF SNR for three different premodulation filter bandwidths and peak deviations of 80, 90, and 100 degrees. Two different PSK demodulators were used. Model A for figures 3.3-1 and 3.3-5 and Model B for figures 3.3-2, 3.3-3, and

<sup>8</sup>Lindsey, W. C. and M. K. Simon, *Telecommunication Systems Engineering*, Prentice-Hall, Inc., Englewood Cliffs, NJ, p64, 1973.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
o NRZ-M PCM/PM	500	3000	1000	CD	80	I/D
+ NRZ-M PCM/PM	500	3000	1000	CD	100	I/D
o NRZ-M PCM/PM	500	3000	1000	CD	90	I/D
* NRZ-M PSK THEORY						

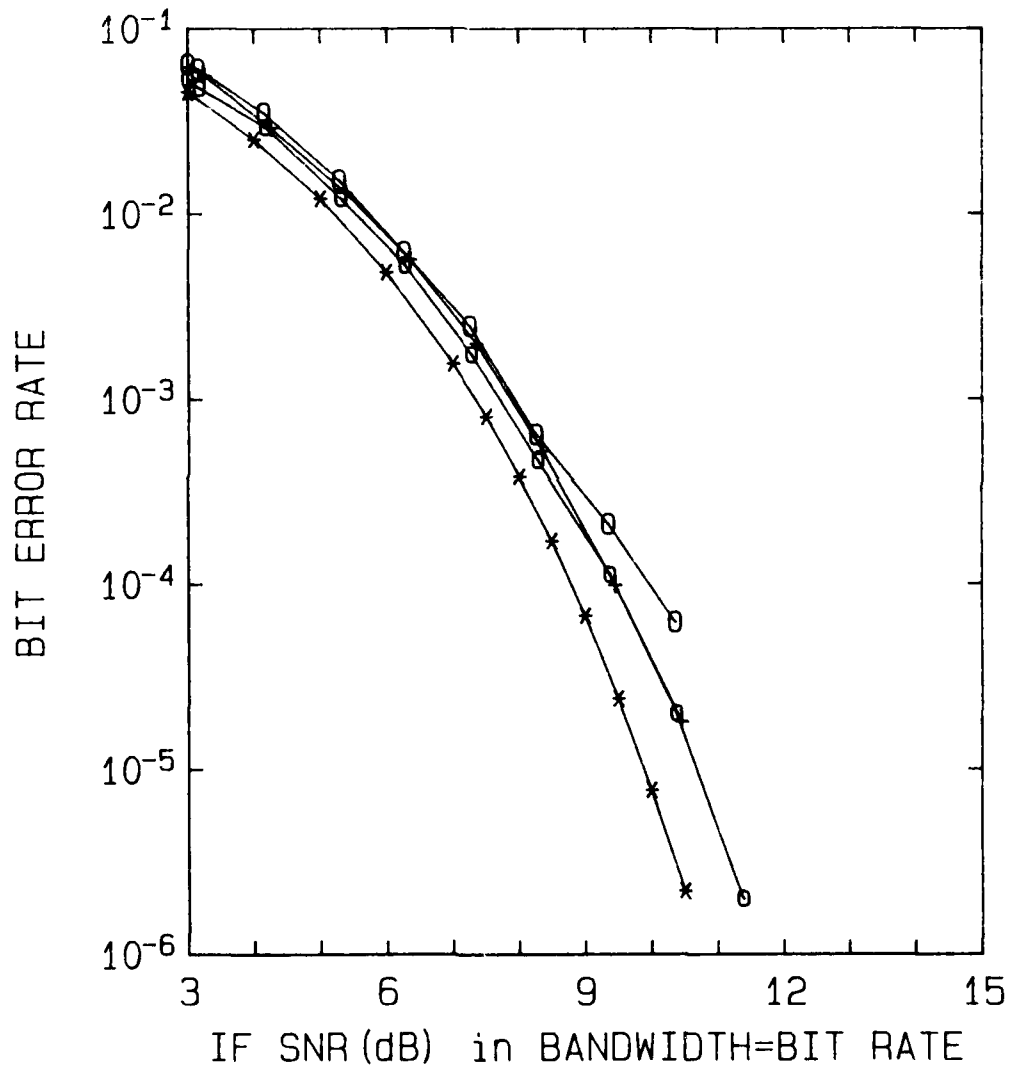


Figure 3.3-1. BER for Peak DEV = 80, 90, and 100 Degrees.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	PREMOD TYPE	PEAK DEV	BIT DET
o NRZ-M PCM/PM	500	3000	1000	CD	80	I/D
+ NRZ-M PCM/PM	500	3000	1000	CD	100	I/D
o NRZ-M PCM/PM	500	3000	1000	CD	90	I/D
* NRZ-M PSK THEORY						

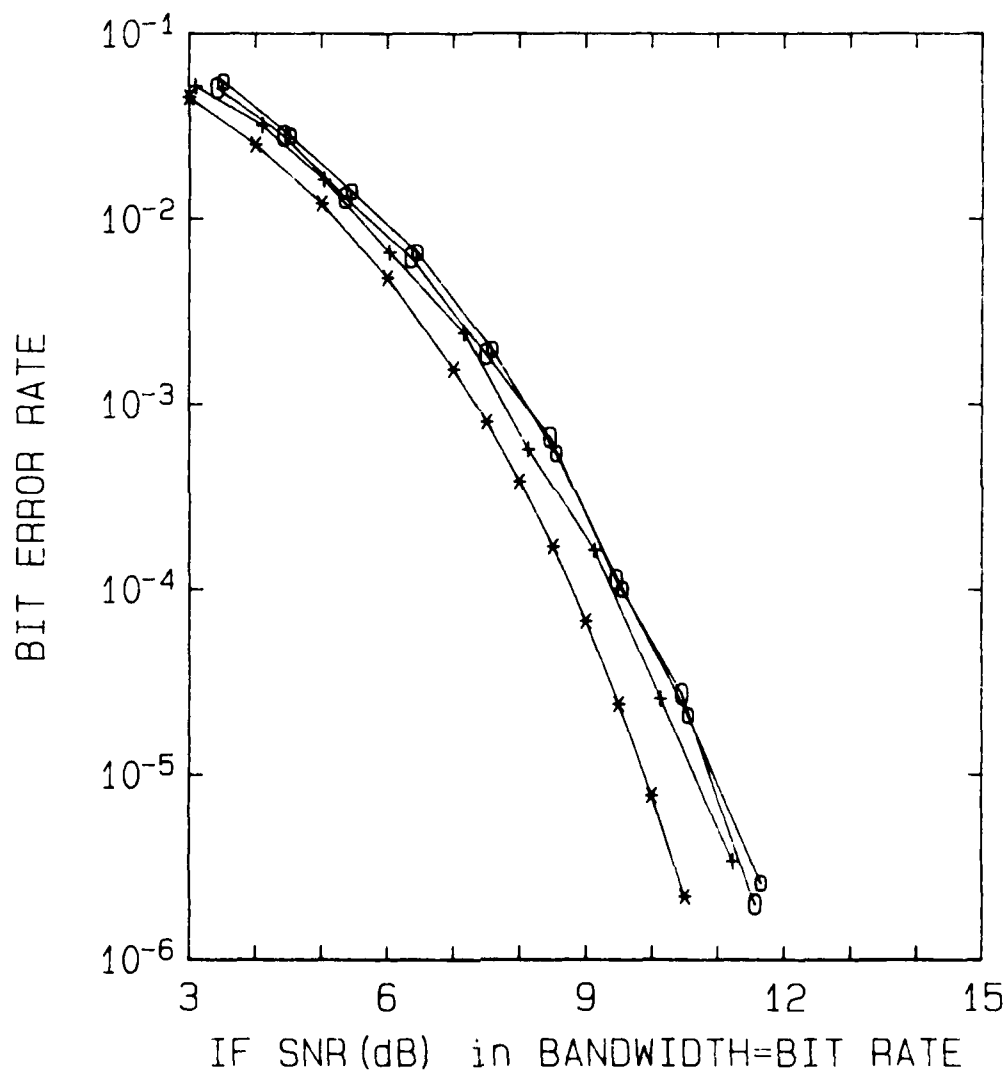


Figure 3.3-2. BER for Peak DEV = 80, 90, and 100 Degrees.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
o NRZ-M PCM/PM	500	3000	500	CD	80	I/D
+ NRZ-M PCM/PM	500	3000	500	CD	100	I/D
o NRZ-M PCM/PM	500	3000	500	CD	90	I/D
* NRZ-M PSK THEORY						

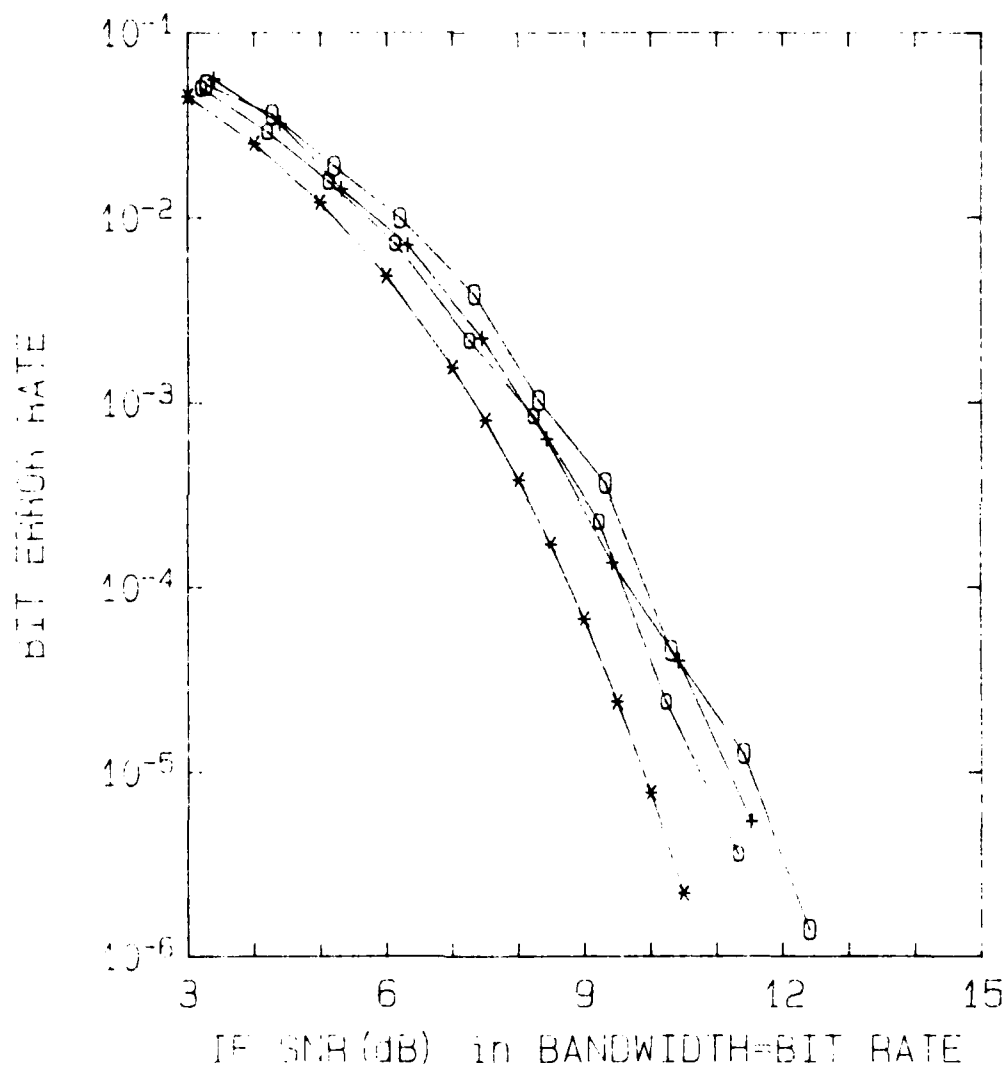


Figure 3.3-3. BER for PREMOD = Bit Rate.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
o NRZ-M PCM/PM	500	3000	350	CD	80	I/C
+ NRZ-M PCM/PM	500	3000	350	CD	100	I/C
o NRZ-M PCM/PM	500	3000	350	CD	90	I/C
* NRZ-M PSK THEORY						

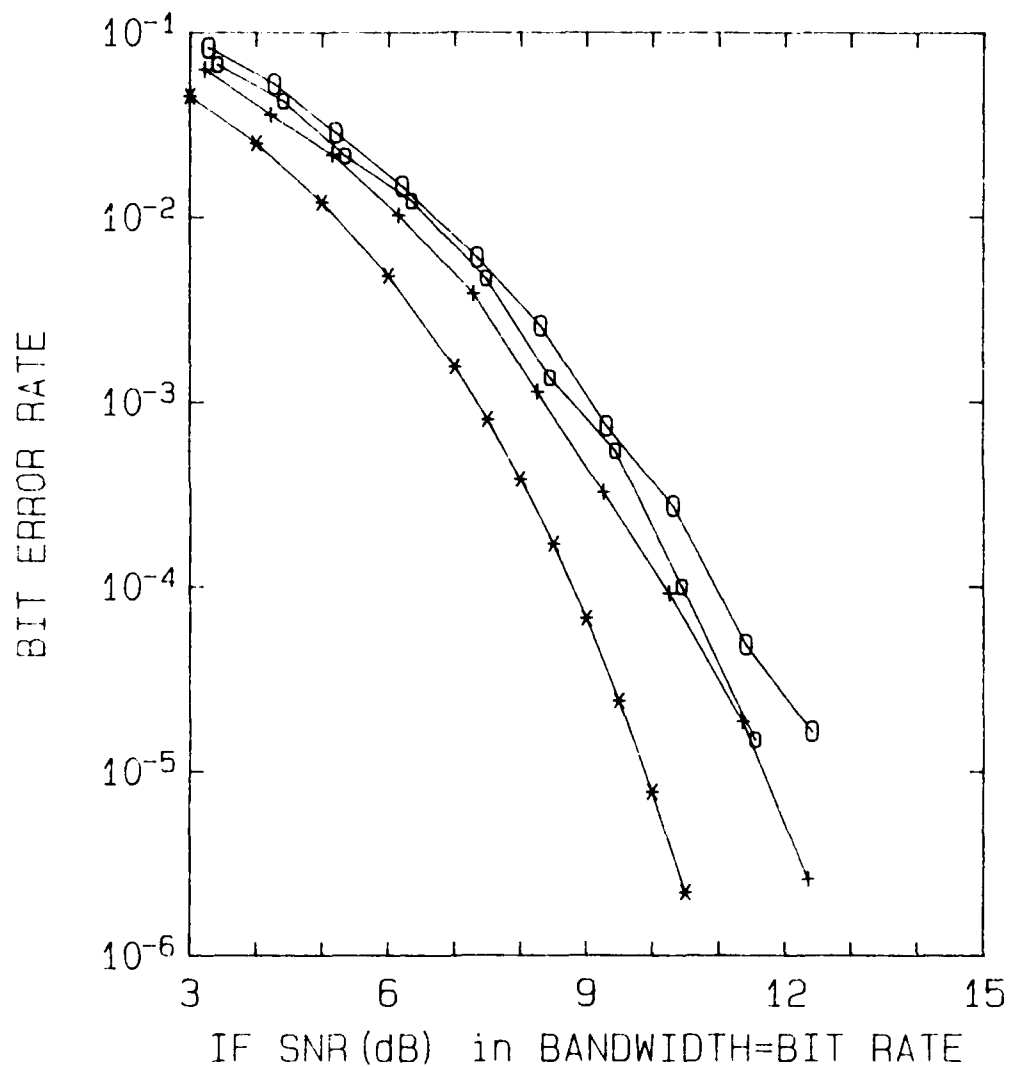


Figure 3.3-4. BER for PREMOD = 0.7 Bit Rate.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
o NRZ-M PCM/PM	500	3000	350	CD	80	F/S
+ NRZ-M PCM/PM	500	3000	350	CD	100	F/S
o NRZ-M PCM/PM	500	3000	350	CD	90	F/S
* NRZ-M PSK THEORY						

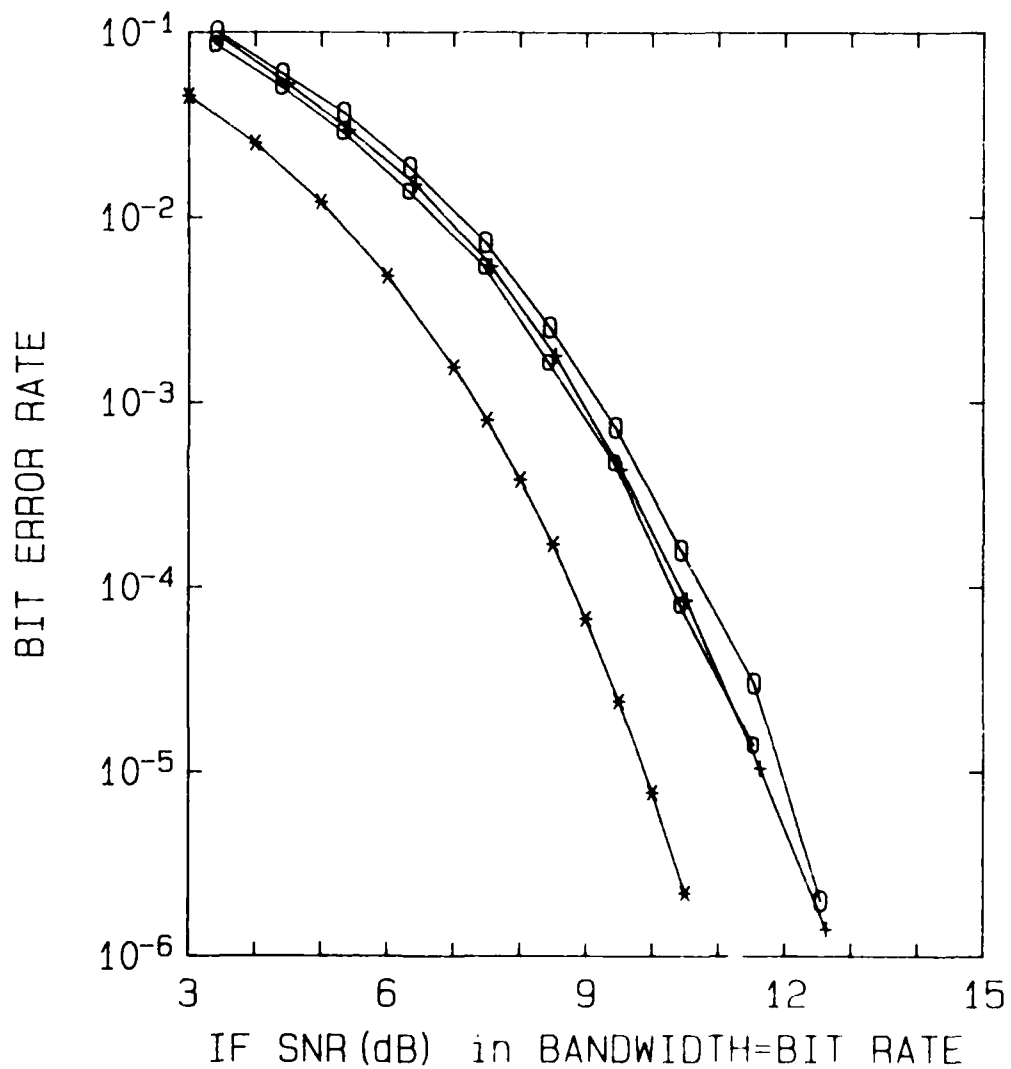


Figure 3.3-5. BER for PREMOD = 0.7 Bit Rate with F/S DET.

3.3-4. There is no apparent difference in the BER performance of PSK demodulator A with either 90 or 100 degrees peak deviation. PSK demodulator B appears to have a slightly lower BER with 100 degrees of peak deviation than with 90 degrees. The performance with 80 degrees of peak deviation is worse than with the other two deviations. The reason for this is that the premodulation filtering of the data reduces the energy in the single bits and therefore a higher deviation is required to make them closer to antipodal.

### 3.3.3 Selection of Premodulation Filter

The best classical low pass premodulation filter to be used with NRZ PCM/PM (90) is a linear phase filter with the widest bandwidth which allows the RF spectral occupancy requirements to be met. The reason for selecting a filter with the widest bandwidth is that premodulation filtering decreases the signal energy per bit without affecting the noise. The signal energy in a bit ( $E_b$ ) is the integral of the signal amplitude ( $S_i(t)$ ) squared over one bit time (T):

$$E_b = \int_0^T S_i^2(t) dt$$

Table 3.3-1 presents the IF SNR in a bandwidth equal to the bit rate required to achieve a BER of  $1 \times 10^{-5}$  for several different premodulation filter bandwidths. The extra SNR required to achieve a BER of  $1 \times 10^{-5}$ , with a bit rate of 500 kb/s and a 3300-kHz IF bandwidth as compared to no premodulation filtering, is 0.5 dB with a 500-kHz linear phase premodulation filter and 1.6 dB with a 250-kHz linear phase premodulation filter. The linear phase premodulation filters cause 0.2 to 0.3 dB less degradation than the constant amplitude filters.

Transversal filters are frequently used in satellite communication systems to minimize the RF spectral occupancy and bit error rate. However, transversal filters will not be discussed in this report.

Table 3.3-1. IF SNR (dB) for  $10^{-5}$  BER With NRZ-M PCM/PM and Various Combinations of Bit Rate, Peak Deviation, IF Bandwidth, and Premodulation Filter.

Bit Rate (kb/s)	Peak Deviation (Degrees)	IF Bandwidth (kHz)	Premodulation BW(kHz)	Type	IF SNR (dB) in BW=Bit Rate for $10^{-5}$ BER
300	90	3300	900	CD	10.7
300	90	3300	300	CD	11.4
500	90	3300		None	10.9
500	99	3300		None	11.2
500	90	1500		None	11.1
500	90	1000		None	11.6
500	90	3300	1000	CD	11.1
500	90	3300	1000	CA	11.3
500	90	3300	500	CD	11.4
500	99	3300	500	CD	11.4
500	90	3300	500	CA	11.7
500	90	3300	250	CD	12.5
500	107	3300	250	CD	12.5
500	90	3300	250	CA	12.8

### 3.3.4 Selection of Receiver IF Bandwidth

The best receiver IF bandwidth is the filter offering the widest bandwidth which rejects all spurious out-of-band signals. The effect of receiver IF bandwidth on BER is illustrated in figure 3.3-6. The spurious signals to be rejected include telemetry signals at other center frequencies and, if the signal is to be predetection-recorded, noise that folds over and back across zero hertz when the signal plus noise is mixed with the local oscillator. An example of the second type is when using a 5-MHz IF bandwidth and a 900-kHz predetection record carrier: the noise spectrum at the  $-3$  dB points would extend from  $f_{IF} - 2.5$  MHz to  $f_{IF} + 2.5$  MHz while the local oscillator frequency would typically be  $f_{IF} + 0.9$  MHz. The noise at  $f_0 + 1.8$  MHz would be translated to 0.9 MHz and be summed with the noise that was translated to 0.9 MHz from  $f_{IF}$  MHz. The net result would be to increase the noise power in the region around the predetection carrier frequency by approximately 3 dB; the exact amount of the increase depends upon the shape of the IF filter. The effect is the same as reducing the transmitted power by this amount. Therefore, the receiver IF bandwidth should not be wider than approximately two times the predetection carrier frequency; that is, a 1.8-MHz IF bandwidth for a 900-kHz predetection carrier. The data presented in figure 3.3-7 show an approximate performance improvement of 0.4 dB when using a linear input to the PSK demodulator compared to using a limited input.

### 3.3.5 Selection of Demodulator Loop Bandwidth

The best loop bandwidth depends on the mission bit rate and the bandwidth of the incidental phase modulation. The loop bandwidth should be wide enough to track out any large amplitude incidental phase modulation. One wideband source of phase modulation is transmission through an ionized gas cloud (plasma). Various rocket booster motors produce ionized gas clouds which cause incidental phase modulation with bandwidths of several kilohertz. However, if the loop bandwidth is wider than approximately 5% of the bit rate, the BER with no incidental phase modulation starts to increase.

### 3.3.6 Selection of Demodulator Video Bandwidth

The best demodulator video bandwidth is largely determined by the bit detector used (see figure 3.3-8). The premodulation filter bandwidth was 1000 kHz for the data in figure 3.3-8. The lowest BER was obtained using an integrate and dump bit detector and the widest video filter. The highest BER occurred when a video filter of one-half the bit rate was used in conjunction with the integrate and dump bit detector. The difference in performance was approximately 2 dB at a  $10^{-5}$  BER. When a filter and sample (F S) bit detector was selected, the highest BER occurred with the widest video filter. The lowest bit error rates with the F S bit detector were achieved with video filters equal to one-half of the bit rate and the bit rate. The reason for the better F S performance with narrower filters in figure 3.3-8 is that the F S bit detector is a matched filter for signals filtered at approximately 0.75 times the bit rate. Using a narrower filter than one-half the bit rate will cause the performance to degrade rapidly.



MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
+ NRZ-M PCM/PM LIN	500	1000	1600	RC	90	I/D
o NRZ-M PCM/PM LIN	500	6000	1600	RC	90	I/D
* NRZ-M PSK THEORY						

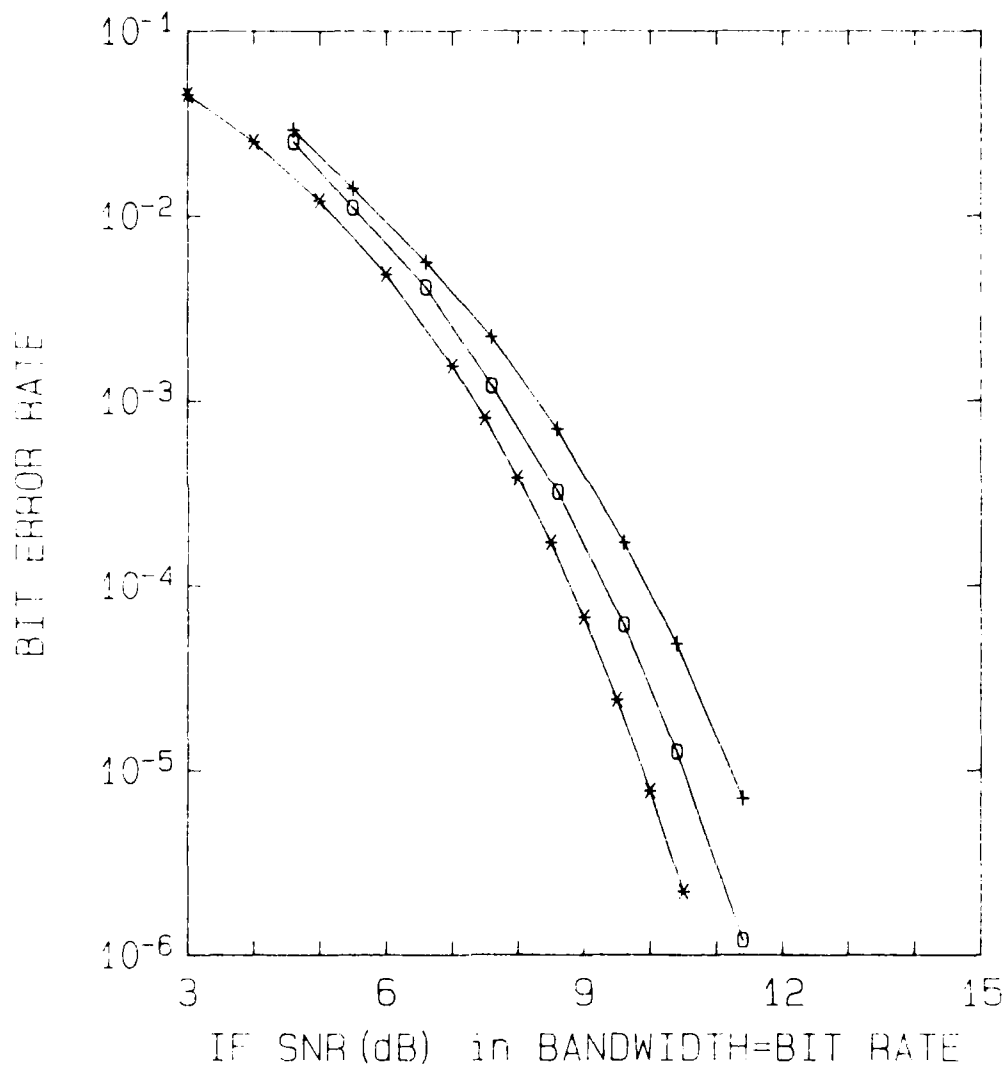


Figure 3.3-6. BER for IF BW/Bit Rate = 2 and 12.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	PEAK TYPE . DEV	BIT DET
--------------------	------------------	--------------	---------------	--------------------	------------

+	NRZ-M PCM/PM LTD	500	6000	1600 RC	90	I/D
o	NRZ-M PCM/PM LIN	500	6000	1600 RC	90	I/D
*	NRZ-M PSK THEORY					

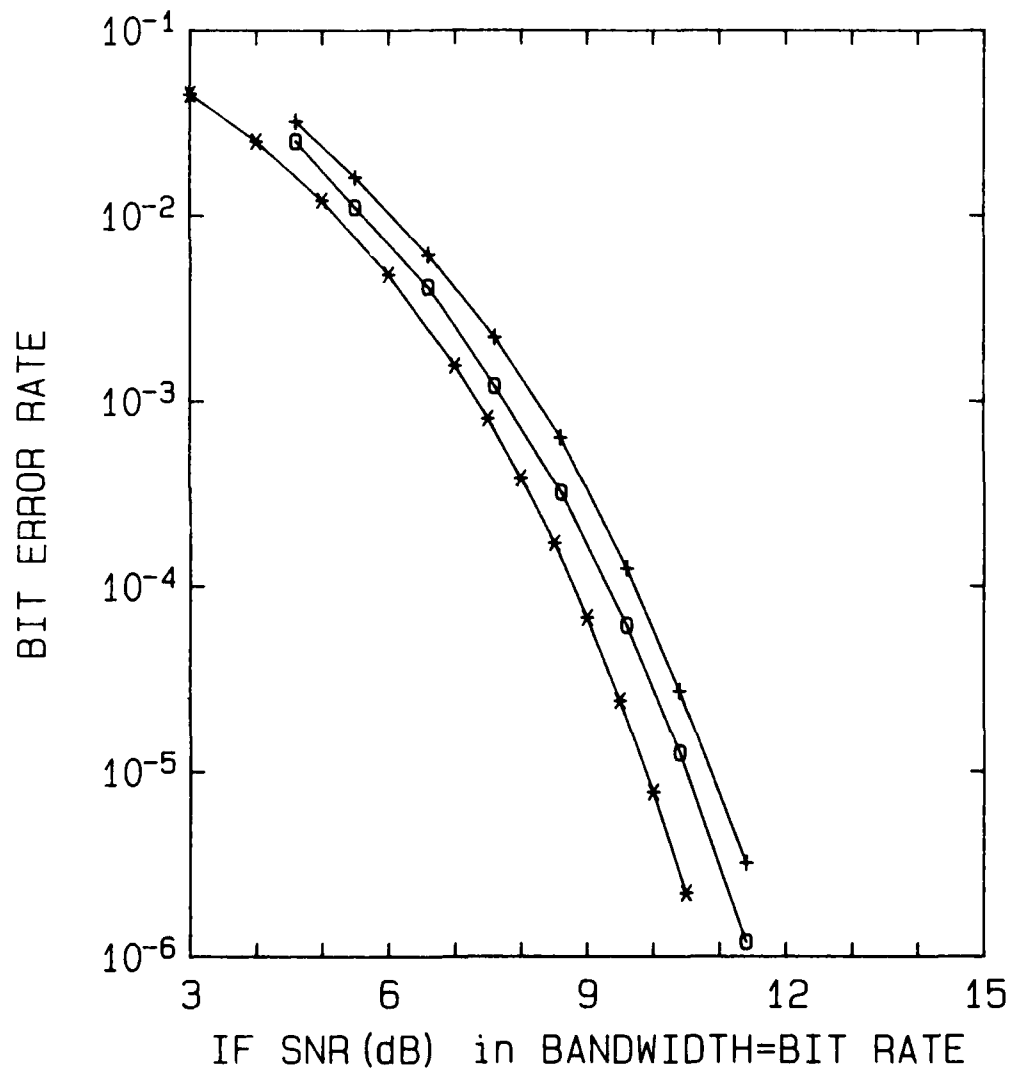


Figure 3.3-7. BER for Linear and Limited IF Signals.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
x NRZ-M PCM/PM	500	4000	250		90	F/S
X NRZ-M PCM/PM	500	4000	250		90	I/D
o NRZ-M PCM/PM	500	4000	500		90	F/S
+ NRZ-M PCM/PM	500	4000	500		90	I/D
o NRZ-M PCM/PM	500	4000	1000		90	F/S
* NRZ-M PCM/PM	500	4000	1000		90	I/D

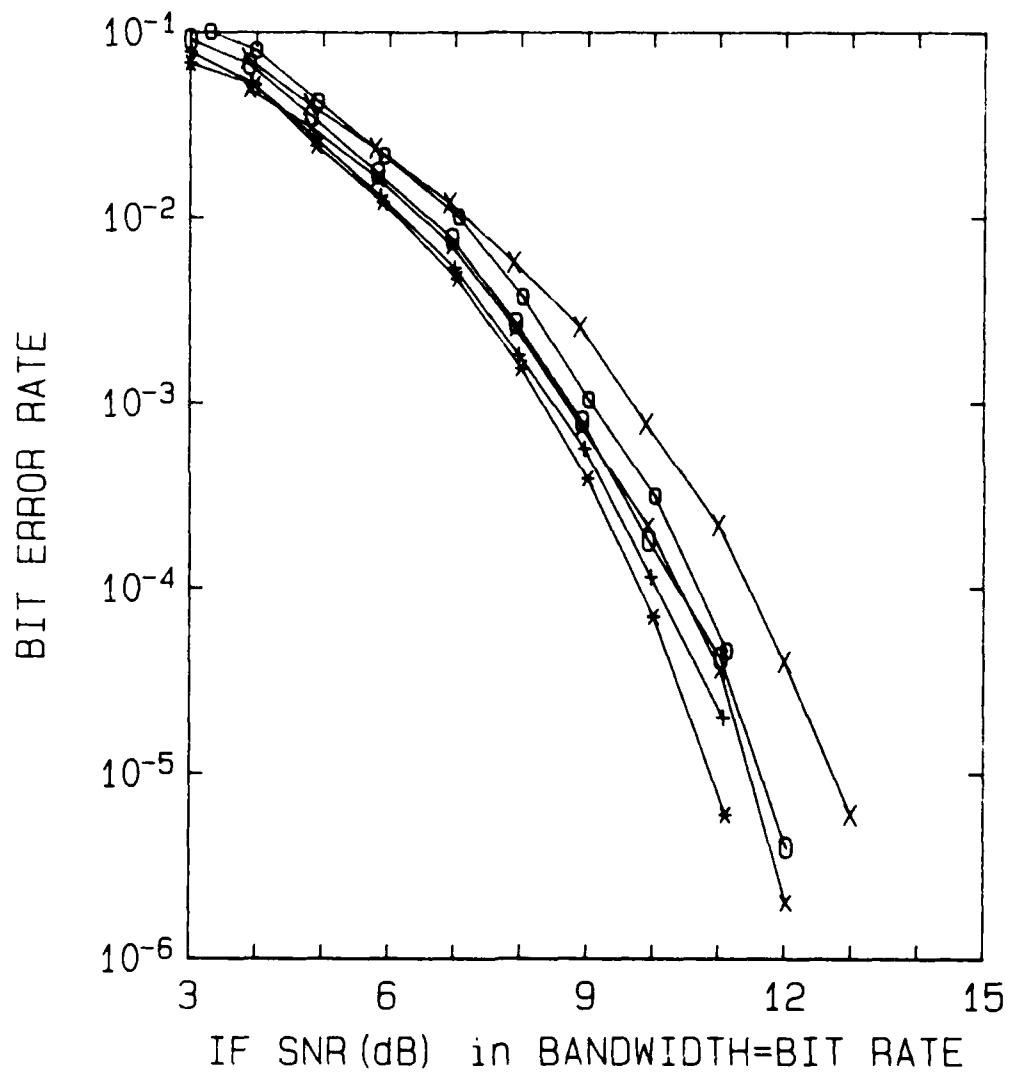


Figure 3.3-8. BER for Video BW/Bit Rate = 0.5, 1, and 2.

### 3.3.7 Selection of PCM Bit Synchronizer Bit Detector

The best PCM bit synchronizer bit detector when using NRZ PCM/PM (90) depends on the amount of filtering performed on the signal prior to the bit synchronizer. When the premodulation and video filter are wider than a value corresponding to the bit rate and the IF bandwidth is set to a value which is equal to at least twice the data bit rate, then the integrate and dump (I/D) bit detector will probably provide the lower bit error rate. When the bandwidth of the premodulation and/or video filters are narrower than 0.7 times the data bit rate and/or the IF bandwidth is less than 1.4 times the bit rate, the filter and sample (F/S) bit detector will probably provide the lower bit error rate. If the total filtering is between the values previously stated, then the I/D bit detector is probably the better choice. This is illustrated in figure 3.3-8. When the narrowest filter is twice the bit rate, the I/D detector performs approximately 1 dB better than the F/S detector at BERs between  $10^{-4}$  and  $10^{-5}$ . When the narrowest filter is one-half the bit rate, the F/S detector performs approximately 1 dB better than the I/D detector.

### 3.3.8 RF Spectra and Carrier Level

The optimum peak deviation for unfiltered NRZ PCM/PM is 90 degrees. This deviation produces a carrier null (see figures 3.3-9, 3.3-10, and 3.3-11). As the bit rate is increased from 50 kb/s to 500 kb/s and 800 kb/s, the depth of the carrier null decreases and discrete frequency components appear in the spectrum. These components are caused by the finite rise and fall times of the PCM bit stream and the finite bandwidth of the phase modulator in the RF generator. When a premodulation filter is used, a peak deviation of 90 degrees will no longer produce a carrier null (refer to figure 3.3-12). The peak deviation required to produce a carrier null depends on the premodulation filter bandwidth, the filter type and number of poles, as well as the bit pattern of the PCM data. When using a 2047-bit pseudo-noise bit stream at 800 kb/s and an 800-kHz 5-pole linear phase premodulation filter, the minimum carrier level occurs at a peak deviation of 99 degrees (refer to figure 3.3-13). A different peak deviation produces the minimum carrier level for other bit patterns for this bit rate and filter. For example, with a bit pattern containing all ones and an NRZ-M code, the carrier is only suppressed 10.6 dB for a peak deviation of 90 degrees (refer to figure 3.3-14), but is suppressed by 30.4 dB for a peak deviation of 111 degrees (refer to figure 3.3-15). This is the maximum suppression for any deviation under the conditions stated above. However, when the bit pattern is changed to a 2047-bit pseudo-noise sequence, the carrier is only suppressed by 11 dB for a peak deviation of 111 degrees (refer to figure 3.3-16). The attenuation of 11 dB is less than the 11.4 dB of carrier suppression produced for a peak deviation of 90 degrees under these conditions. With a 400-kHz 5-pole linear phase premodulation filter, the carrier is suppressed 8.6 dB (refer to figure 3.3-17) for a peak deviation of 90 degrees with a 2047-bit pseudo-noise sequence. The minimum carrier level occurs with a peak deviation of 113 degrees under the above conditions (refer to figure 3.3-18). Figures 3.3-19 and 3.3-20 show the RF spectra with constant amplitude premodulation filters. The occupied bandwidth of 800 kb/s NRZ-M PCM/PM is determined by the spectral spikes and is equal to eight, six, and four times the bit rate for premodulation filters of 800 kHz CD, 800 kHz CA, and 400 kHz CD respectively.

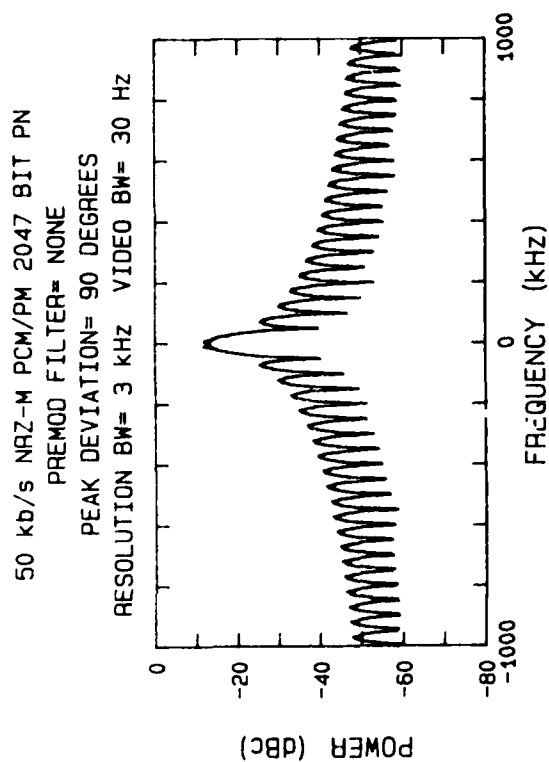


Figure 3.3-9. RF Spectrum 50 kb/s NRZ-M PCM/PM.

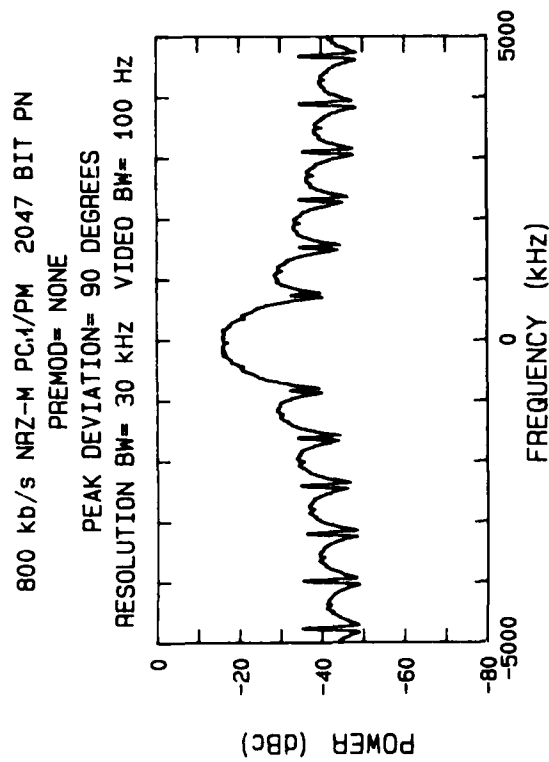


Figure 3.3-11. RF Spectrum 800 kb/s NRZ-M PCM/PM.

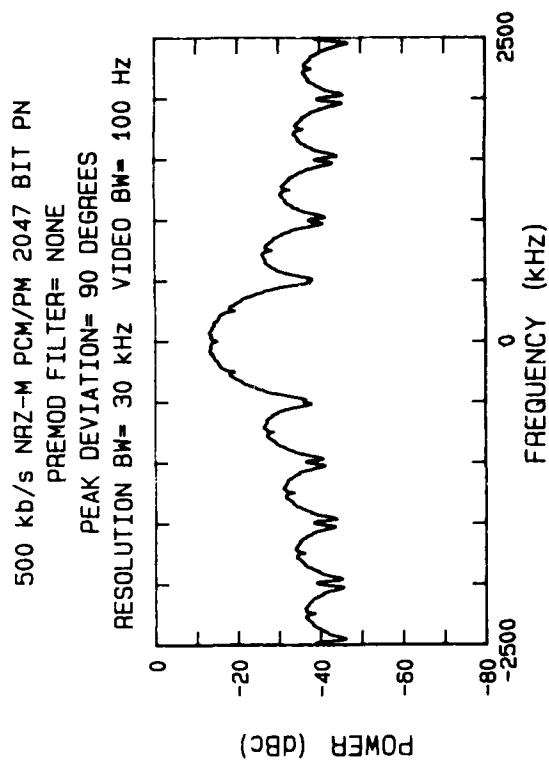


Figure 3.3-10. RF Spectrum 500 kb/s NRZ-M PCM/PM.

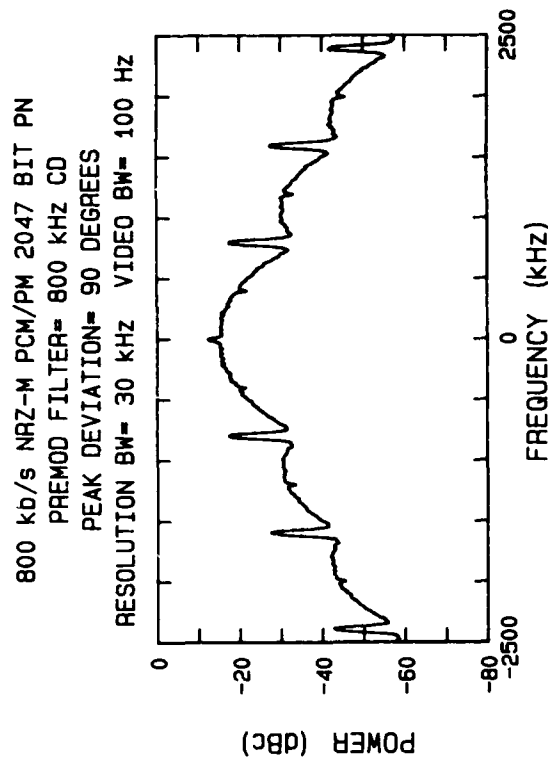


Figure 3.3-12. RF Spectrum PREMOD=800 kHz CD Peak Dev=90 Degrees.

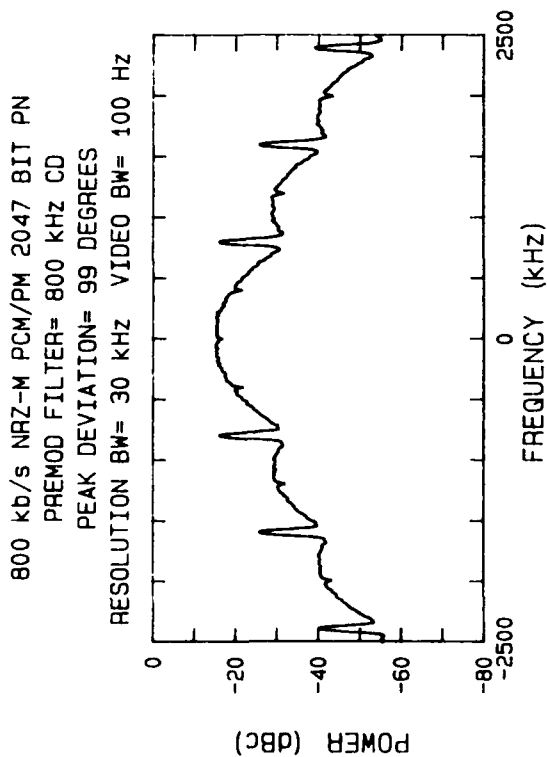


Figure 3.3-13. RF Spectrum PREMOD=800 kHz CD Peak DEV=99 Degrees.

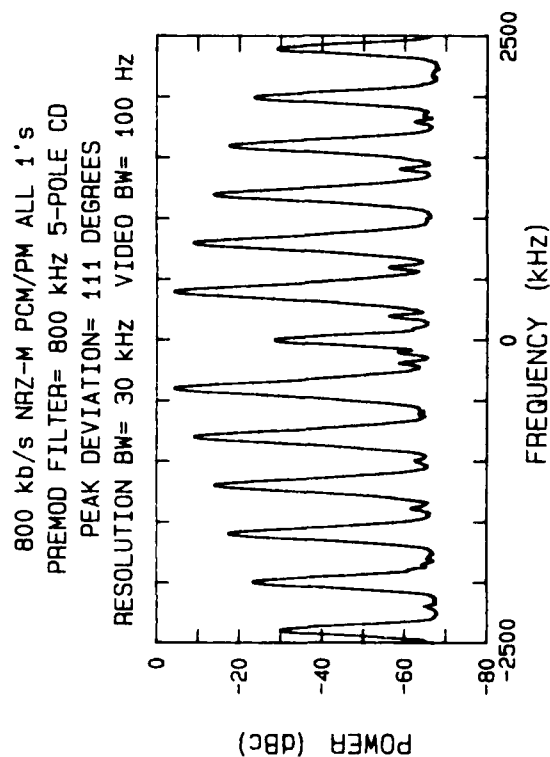


Figure 3.3-15. RF Spectrum PREMOD=800 kHz CD Peak DEV=111 DEG (1s).

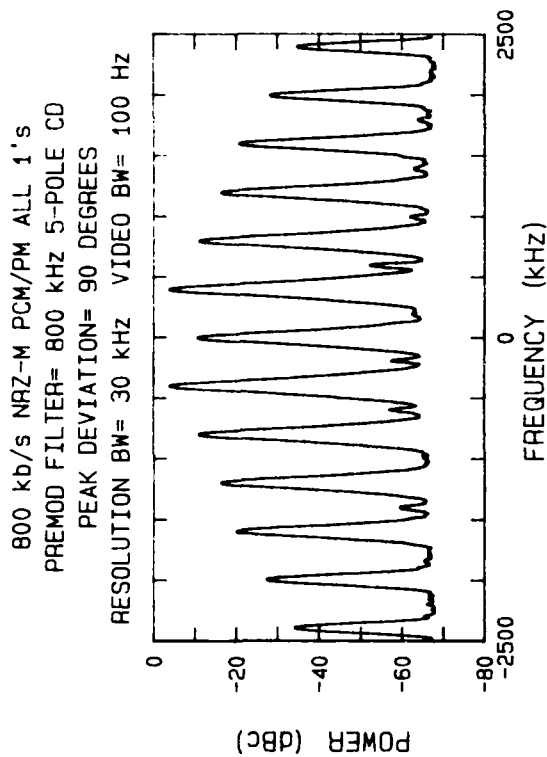


Figure 3.3-14. RF Spectrum PREMOD=800 kHz CD Peak DEV=90 Degrees (1s).

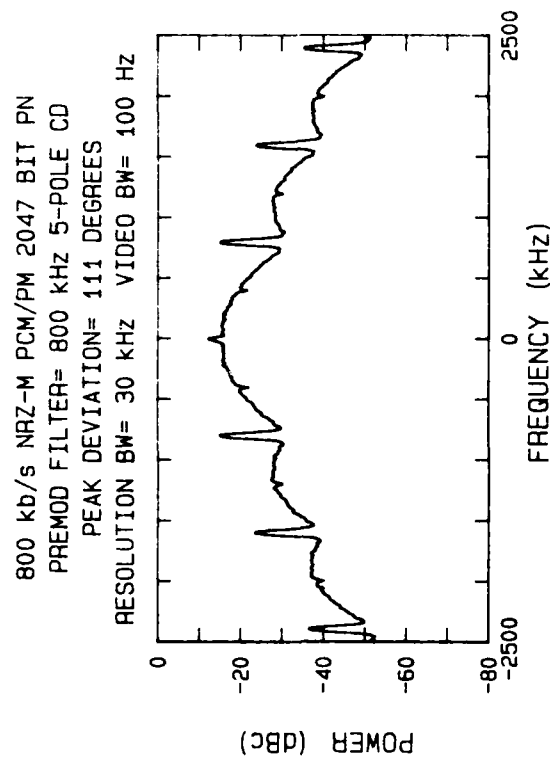


Figure 3.3-16. RF Spectrum PREMOD=800 kHz CD Peak DEV=111 Degrees.

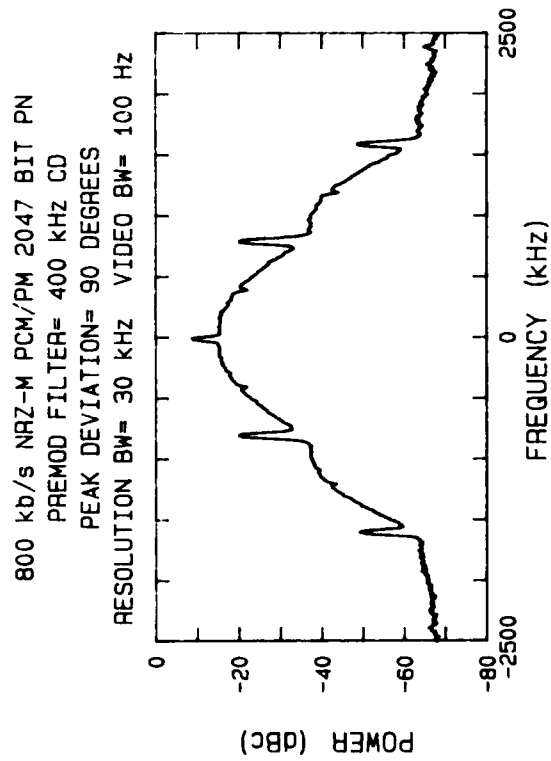


Figure 3.3-17. RF Spectrum PREMOD=400 kHz CD Peak DEV=90 Degrees.

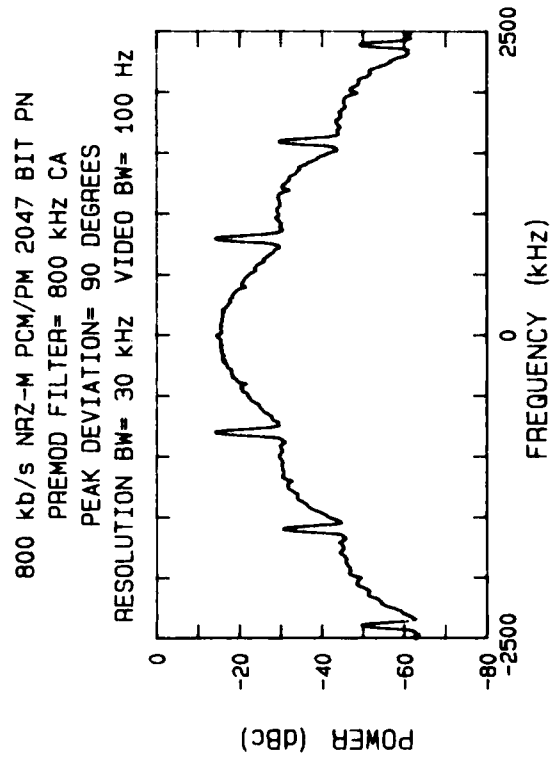


Figure 3.3-19. RF Spectrum PREMOD=800 kHz CA Peak DEV=90 Degrees.

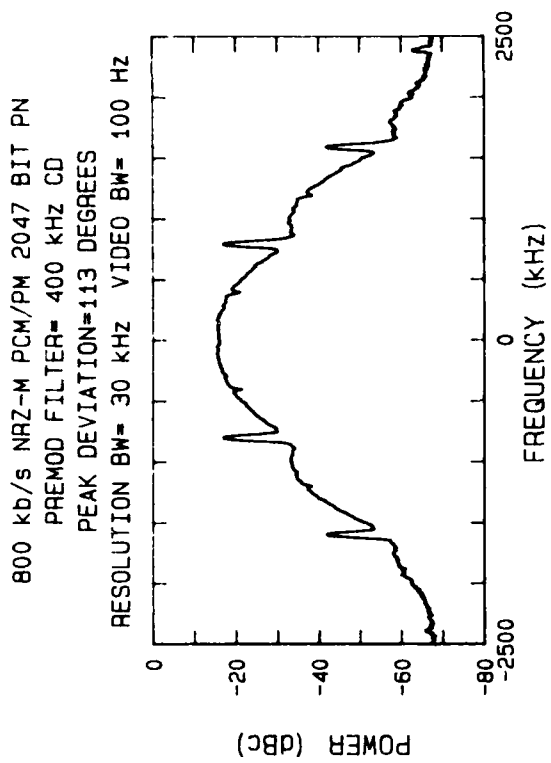


Figure 3.3-18. RF Spectrum PREMOD=400 kHz CD Peak DEV=113 Degrees.

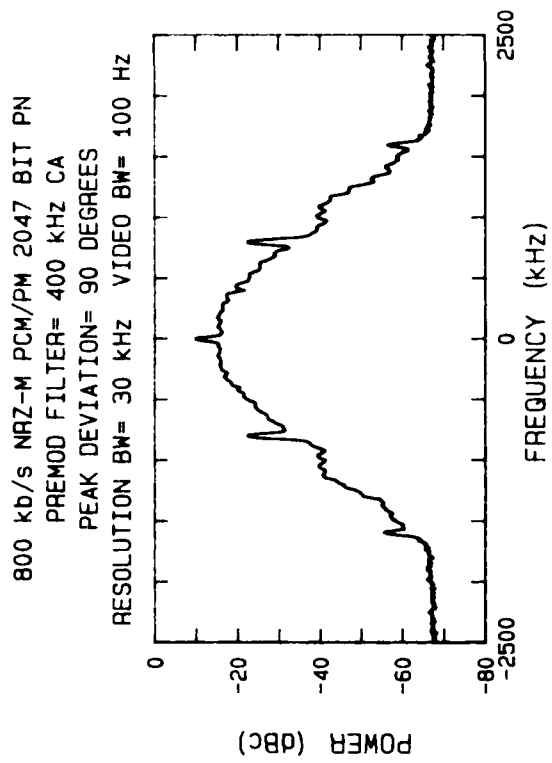


Figure 3.3-20. RF Spectrum PREMOD=400 kHz CA Peak DEV=90 Degrees.

### 3.4 BIPHASE PCM/PM

#### 3.4.1 Introduction

There are two major types of biphasic PCM/PM telemetry signals:

1. Signals with a peak deviation less than 90 degrees.
2. Signals with a peak deviation of approximately 90 degrees.

If the peak deviation is less than 90 degrees, a signal component is always present at the unmodulated carrier frequency. The percentage of the total power contained in this component is determined by the peak deviation, premodulation filtering, phase modulator bandwidth, and the PCM signal bit pattern. If there is no filtering, the remnant carrier power is proportional to  $\cos^2(\Delta\theta)$  and the demodulator output signal power is proportional to  $\sin^2(\Delta\theta)$  where  $\Delta\theta$  is the peak deviation. Therefore, the use of a peak deviation of 60 degrees results in a signal power loss of at least 1.25 dB compared to the use of a 90-degree peak deviation. The signal loss for a 75-degree peak deviation is only 0.3 dB with no filtering.

If there is sufficient carrier power present, a phase-locked loop (PLL) can be used to track the carrier component and therefore provide a reference signal to the phase demodulator. As the percentage of the total power remaining in the carrier is increased, the demodulated signal amplitude will be reduced proportionately. However, if the carrier component is too small, the PLL will not be able to maintain accurate phase lock at low SNRs. Therefore, a trade-off must be made between carrier power and signal power. Peak carrier deviations between 60 degrees and 75 degrees are usually used for biphasic PCM/PM with a carrier-tracking phase demodulator. However, if a premodulation filter bandwidth of twice the bit rate or less is used, peak deviations of 90 degrees can be used successfully with a carrier-tracking demodulator. The carrier is attenuated by approximately 12 dB with a linear phase premodulation filter at twice the bit rate and a peak deviation of 90 degrees (see figure 3.4-1). If a peak deviation of 90 degrees is used with a carrier-tracking demodulator, the system designer must make sure that the actual peak deviation cannot produce a carrier null under worst case combinations of deviation sensitivity and bit stream amplitude.

When a peak deviation of approximately 90 degrees is used, a PSK demodulator can be used to demodulate the signal with or without a carrier null. A PSK demodulator reconstructs a carrier signal and uses this signal to coherently detect the modulation. The two most common types of PSK demodulators use a Costas loop or a squaring loop to reconstruct the carrier signal. Both techniques have a 180-degree phase ambiguity problem which means that the polarity (inverted or normal) of the detected signal is unknown. If carrier lock is lost; the detected signal, after lock is reacquired, has a 50% chance of being inverted compared to the signal before carrier lock was lost. Therefore, the mark and space versions of biphasic are usually used when a PSK demodulator is used. The carrier-tracking demodulator does not have a polarity reversal problem and therefore biphasic level is usually used in biphasic PCM/PM systems when sufficient carrier level is present to allow the demodulator to track the carrier. The bit error rate for biphasic level is approximately one-half of the bit error rate for biphasic mark and biphasic space.



400 kb/s BIPHASE PCM/PM 2047 BIT PN

PREMOD FILTER= 800 kHz 5-POLE CD

PEAK DEVIATION= 90 DEGREES

RESOLUTION BW= 30 kHz VIDEO BW= 100 Hz

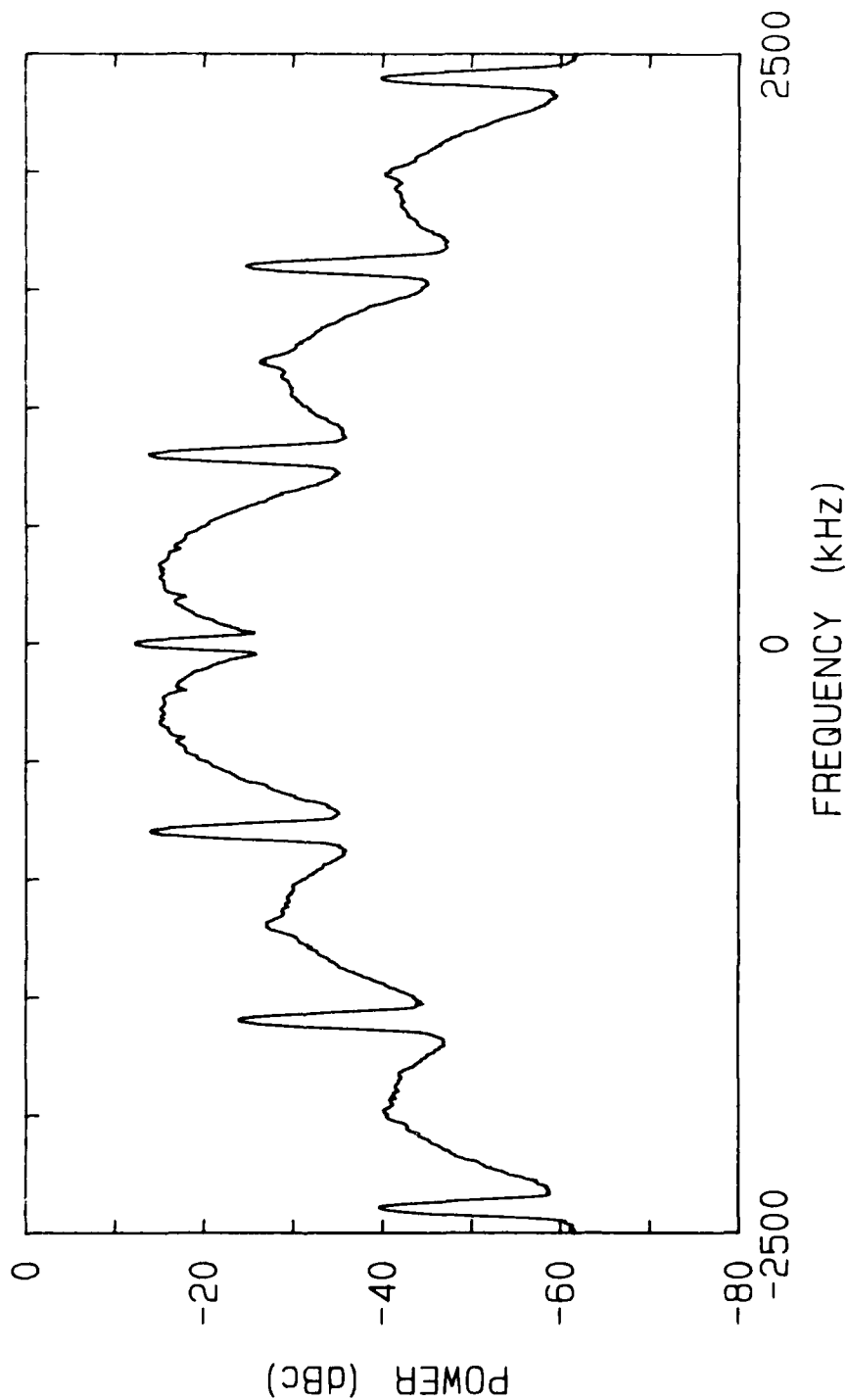


Figure 3.4-1. 400 kb/s Biphase PCM/PM RF Spectrum (PREMOD=800 kHz CD, DEV=90 Degrees).

### 3.4.2 Selection of Peak Deviation

Bit error rate data is presented in figure 3.4-2 for peak deviations of 60, 75, and 90 degrees. The bit rate was 500 kb/s, the IF bandwidth was 4000 kHz, and a 1000-kHz 5-pole constant delay premodulation filter was used. This data shows that a 75-degree peak deviation performed about 1.2 dB better than a 60-degree peak deviation under these test conditions. This difference is slightly larger than the 0.95 dB predicted for non-filtered data. The additional degradation is due to the fact that the premodulation filtering reduces the effective amplitude per bit. This reduces the effective deviation which causes a reduction in  $\sin^2(\Delta\theta)$ . The reduction in  $\sin^2$  is larger for small  $\Delta\theta$  than for large  $\Delta\theta$  with the same proportional reduction in  $\Delta\theta$ .

Comparing biphasic level PCM/PM with peak deviations of 75 degrees and 90 degrees, we find that a peak deviation of 90 degrees performs 0.3 to 0.4 dB better than a peak deviation of 75 degrees. The carrier level was -12 dBc with a 90-degree peak deviation and -7 dBc with a 75-degree peak deviation. Therefore, carrier lock will be lost 5 dB sooner with a 90-degree peak deviation than with a 75-degree peak deviation. However, under these test conditions, the PCM bit synchronizer (loop bandwidth of 0.3%) lost lock before a PM demodulator with a 1-kHz loop bandwidth did. A Costas loop demodulator provided the same BER performance as the PM demodulator, but the unknown polarity when using biphasic level would present a problem for many applications. Switching to biphasic mark causes the BER to approximately double. This is equivalent to a 0.3-dB penalty at a  $10^{-5}$  BER, a 0.5-dB penalty at a  $10^{-3}$  BER, a 0.9-dB penalty at a  $10^{-2}$  BER, and a 2-dB penalty at a BER of  $10^{-1}$ . Therefore, biphasic mark with a 90-degree peak deviation should perform much the same as biphasic level with a 75-degree peak deviation at a BER of  $10^{-5}$ . This is also shown in figure 3.4-2. Biphasic level with a 75-degree peak deviation has a measurably lower BER than biphasic mark with a 90-degree peak deviation for BERs larger than  $10^{-3}$ .

Bit error rate data is presented in figure 3.4-3 for a premodulation filter equal to the bit rate and peak deviations of 60, 75, and 90 degrees. Again, a peak deviation of 75 degrees performs approximately 1.2 dB better than a deviation of 60 degrees. However, under these conditions, a 90-degree peak deviation and biphasic level coding perform approximately 1 dB better than a 75-degree peak deviation at a BER of  $10^{-5}$ . A 90-degree peak deviation and biphasic mark coding perform better than a 75-degree peak deviation and biphasic level coding for BERs less than  $10^{-2}$ .

### 3.4.3 Selection of Premodulation Filter

The data presented in figures 3.4-4, 3.4-5, 3.4-6, and 3.4-7 show that the bit error performance is essentially the same for constant amplitude and constant delay filters having the same bandwidth. These data also show that the BER penalty for using a premodulation filter with a bandwidth equal to the bit rate instead of a premodulation filter equal to twice the bit rate is  $1.5 \pm 0.5$  dB when the IF bandwidth is at least three times the bit rate. The penalty is approximately 1.8 dB with a 60-degree peak deviation, 1.5 dB with a 75-degree peak deviation, and 1.0 dB with a 90-degree peak deviation for an IF bandwidth of eight times the bit rate. With an IF bandwidth equal to twice the bit rate, the penalty for using a premodulation bandwidth equal to the bit rate is  $1.2 \pm 0.2$  dB. The penalty for using a premodulation filter equal to twice the bit rate is approximately 0.3 dB when compared to no premodulation filtering.

MODULATION TYPE	BIT RATE IF BW kb/s kHz	PREMOD kHz TYPE	PEAK DEV	BIT DET
0 BIØ-L PCM/PM	500 4000	1000 CD	60	
+ BIØ-L PCM/PM	500 4000	1000 CD	75	
o BIØ-L PCM/PM	500 4000	1000 CD	90	
* BIØ-M PCM/PM	500 4000	1000 CD	90	

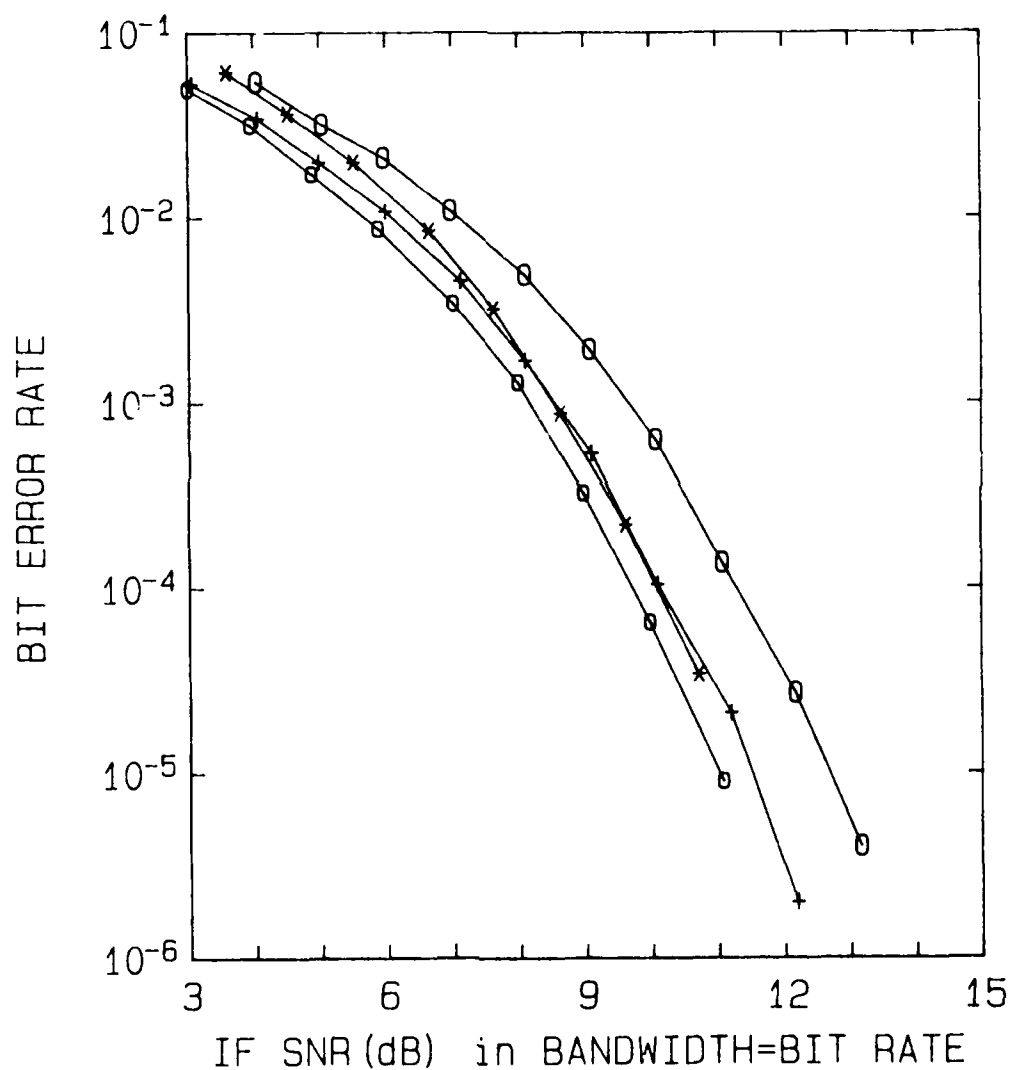


Figure 3.4-2. BER for Peak DEV = 60, 75, and 90 Degrees.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
0 BIØ-L PCM/PM	500	4000	500	CD	60	
+ BIØ-L PCM/PM	500	4000	500	CD	75	
o BIØ-L PCM/PM	500	4000	500	CD	90	
* BIØ-M PCM/PM	500	4000	500	CD	90	

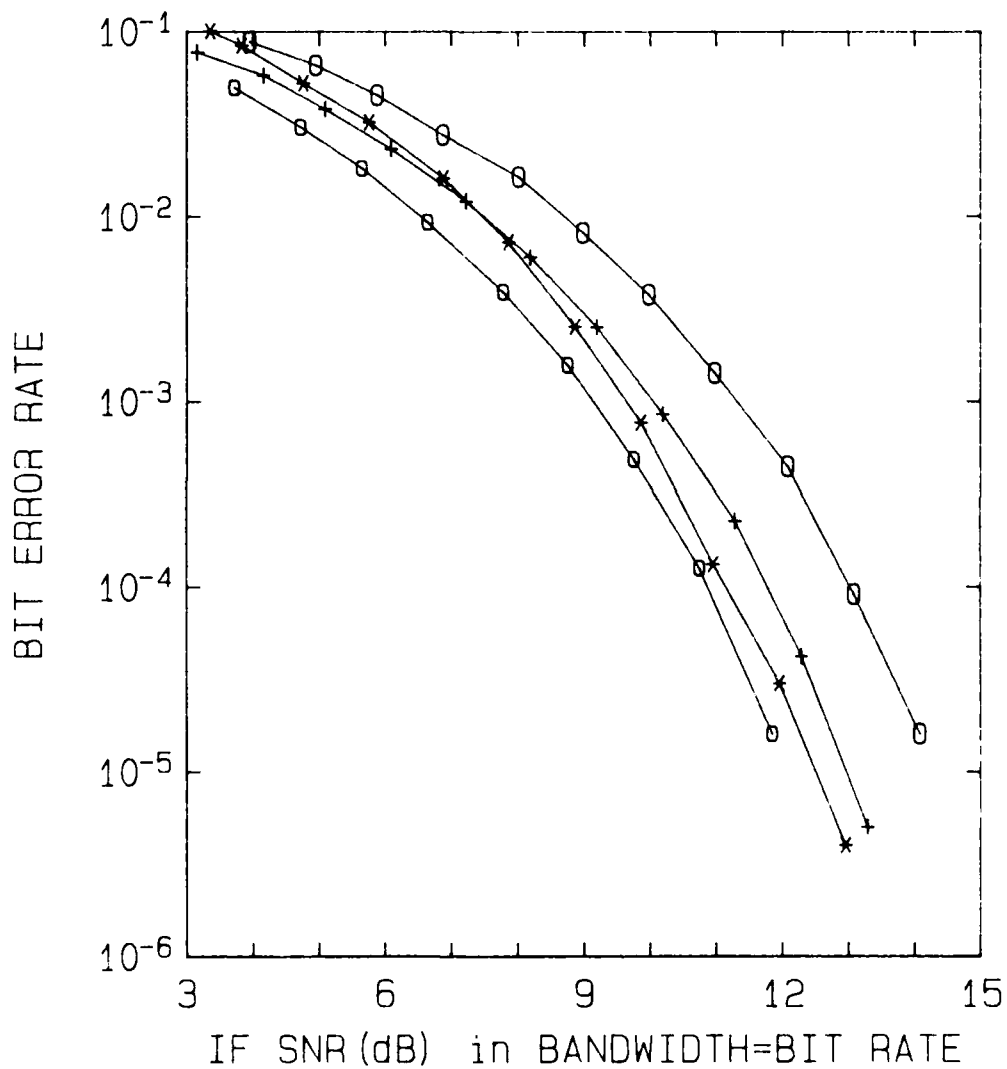


Figure 3.4-3. BER for Peak DEV = 60, 75, and 90 Degrees.

MODULATION TYPE .	BIT RATE IF BW kb/s	kHz	PREMOD kHz TYPE	PEAK DEV	BIT DET
0 BIØ-L PCM/PM	500	4000	500 CA	60	
+ BIØ-L PCM/PM	500	4000	500 CD	60	
o BIØ-L PCM/PM	500	4000	1000 CA	60	
* BIØ-L PCM/PM	500	4000	1000 CD	60	

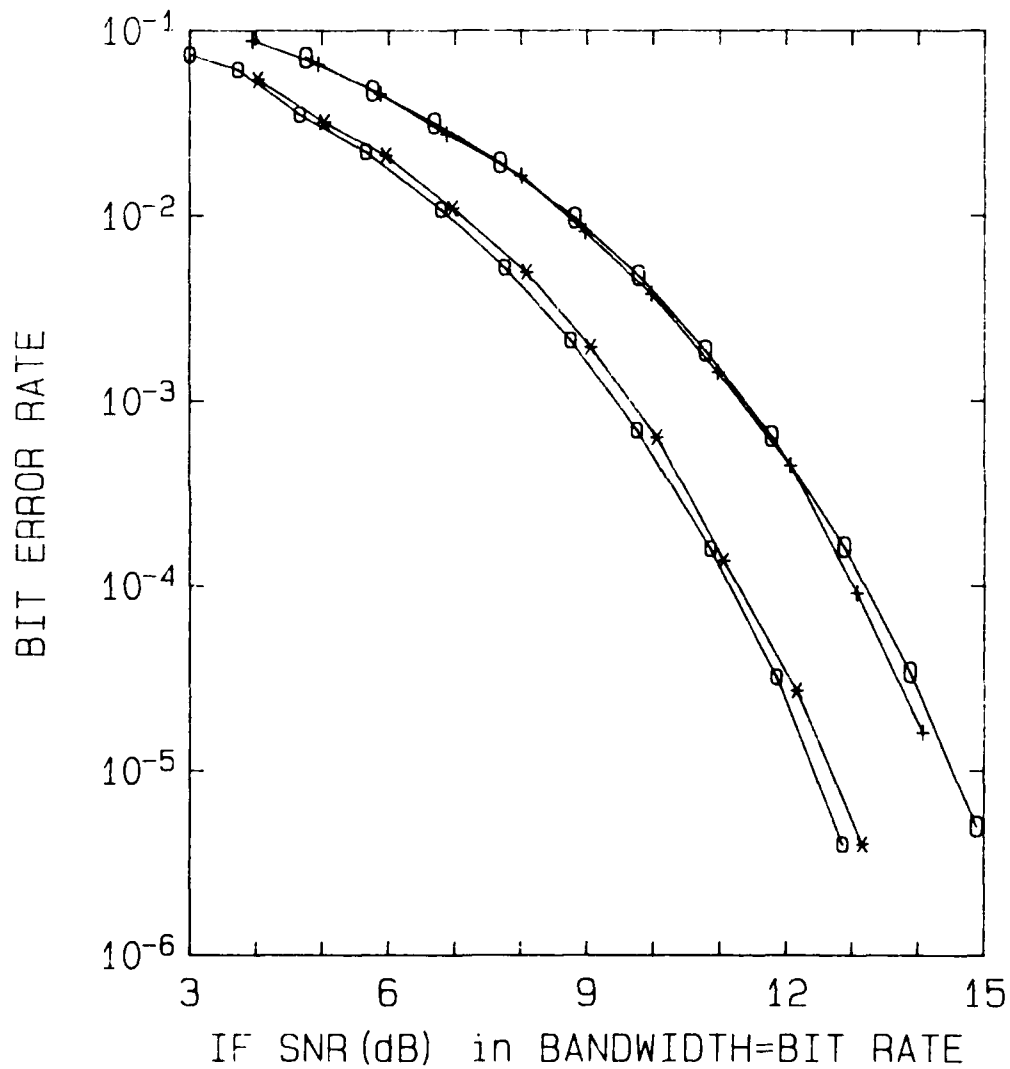


Figure 3.4-4. BER for Peak DEV=60 DEG and PREMOD=1 and 2 Bit Rate.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
0 BIØ-L PCM/PM	500	4000	500	CA	75	
+ BIØ-L PCM/PM	500	4000	500	CD	75	
o BIØ-L PCM/PM	500	4000	1000	CA	75	
* BIØ-L PCM/PM	500	4000	1000	CD	75	MON

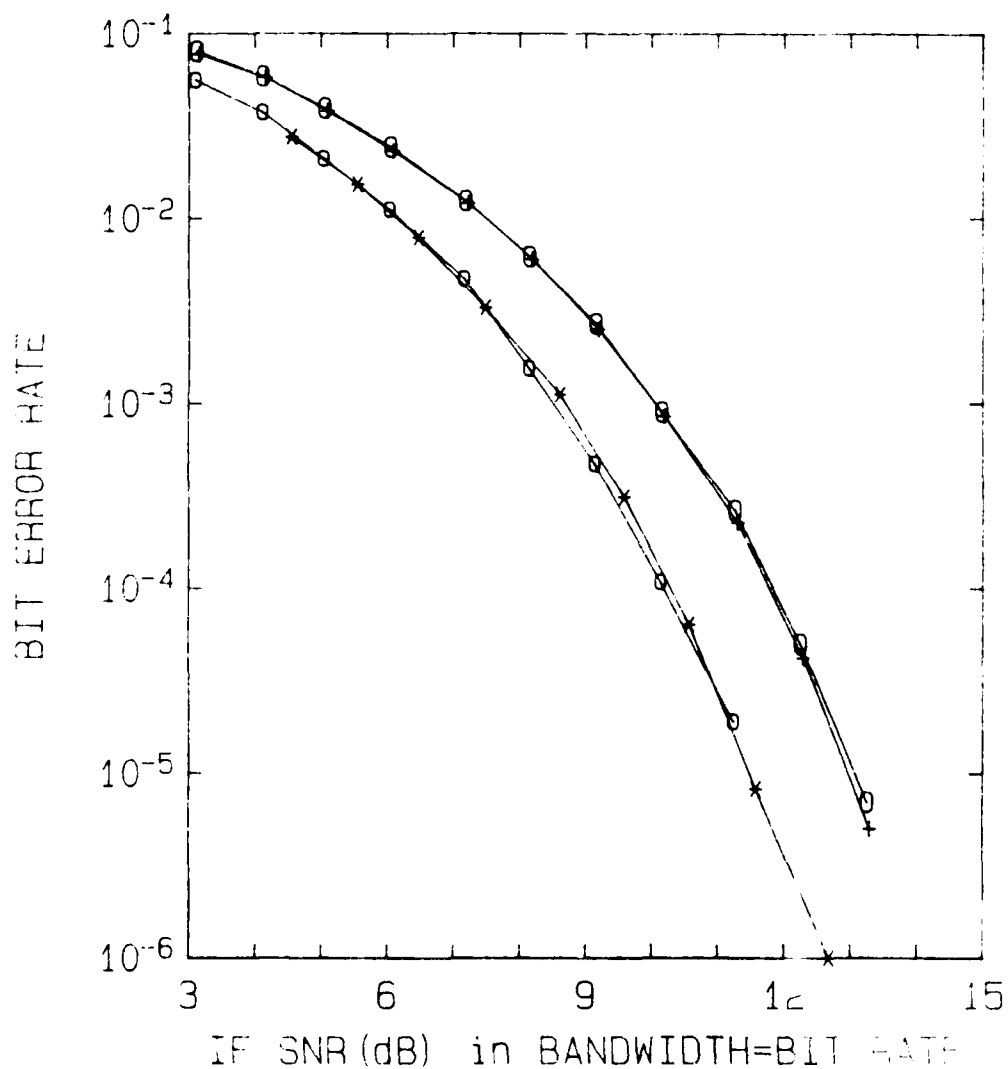


Figure 3.4-5. BER for Peak DEV=75 DEG and PREMOD=1 and 2 Bit Rate.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
0 BIØ-M PCM/PM	500	4000	500	CA	90	
+ BIØ-M PCM/PM	500	4000	500	CD	90	
o BIØ-M PCM/PM	500	4000	1000	CA	90	
* BIØ-M PCM/PM	500	4000	1000	CD	90	

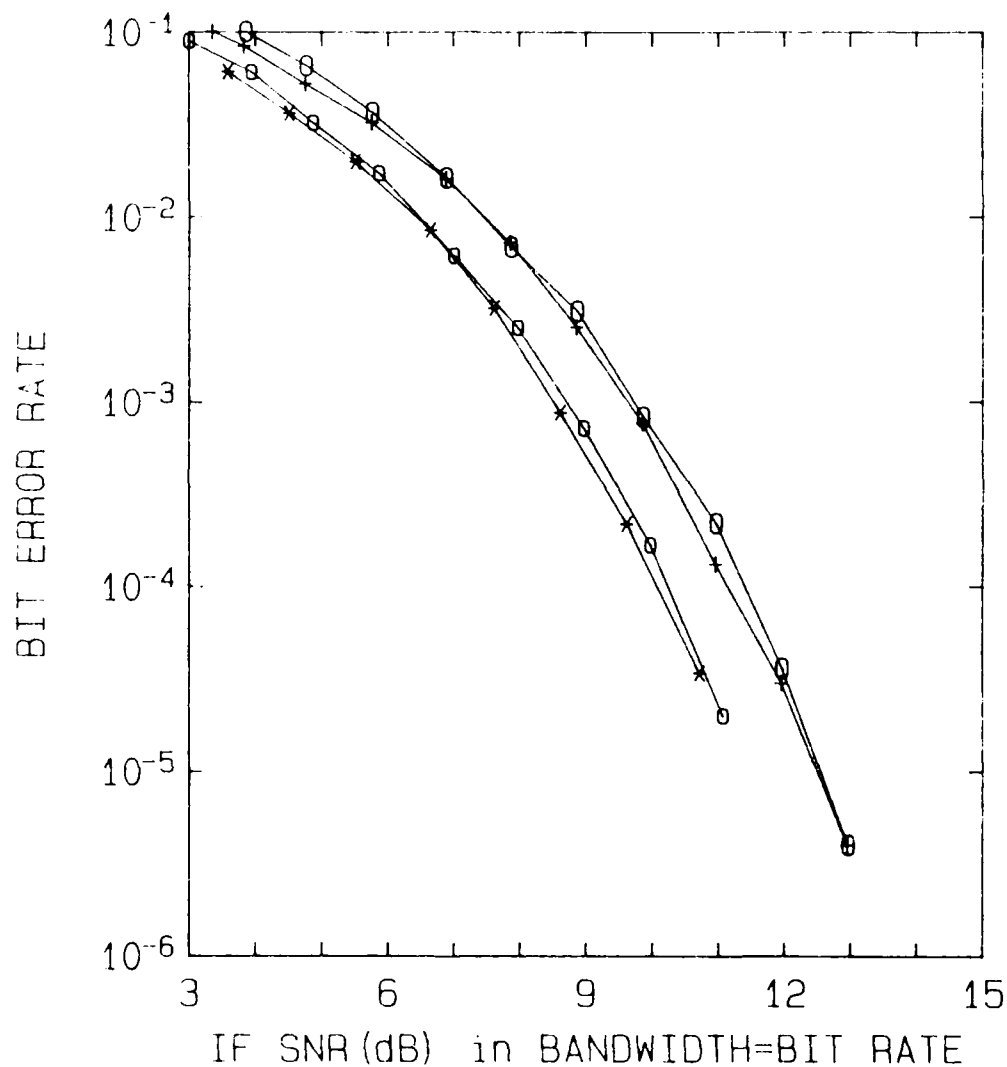


Figure 3.4-6. BER for Peak DEV=90 DEG and PREMOD=1 and 2 Bit Rate.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
0 B10-L PCM/PM	500	1500	500	CA	75	
+ B10-L PCM/PM	500	1500	500	CD	75	
o B10-L PCM/PM	500	1500	1000	CA	75	
* B10-L PCM/PM	500	1500	1000	CD	75	

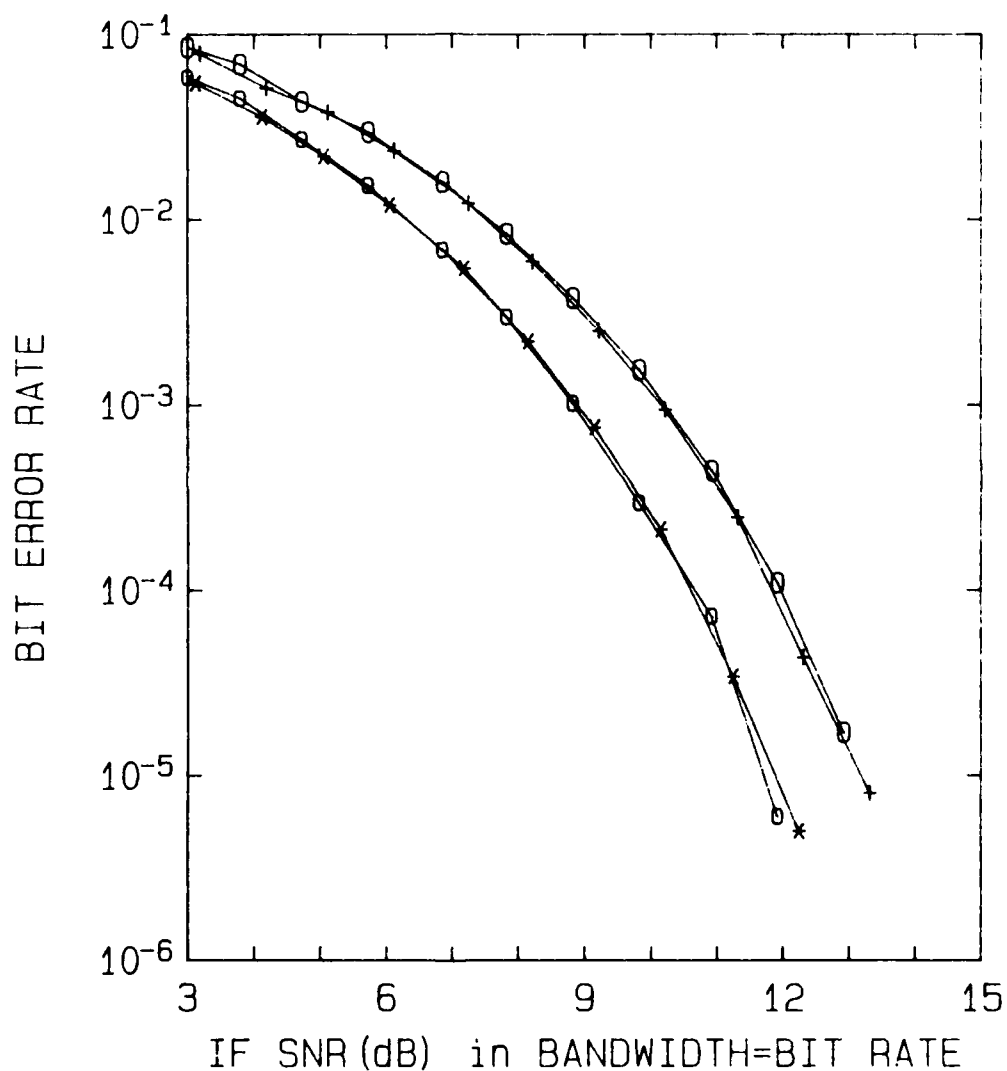


Figure 3.4-7. BER for IF BW=3 Bit Rate and PREMOD=1 and 2 Bit Rate.



Figure 3.4-8 shows a biphase level PCM signal which has been low-pass filtered at twice the bit rate. Figure 3.4-9 shows a biphase level PCM eye pattern with a low pass filter at 1.4 times the bit rate.

#### **3.4.4 Selection of Receiver IF Bandwidth**

The effect of different IF filter bandwidths on the bit error rate is shown in figures 3.4-10, 3.4-11, and 3.4-12. These data show that an IF bandwidth of eight times the bit rate performs approximately the same as an IF bandwidth of twenty times the bit rate. An IF bandwidth of three times the bit rate causes an SNR penalty of approximately 0.5 dB when compared to an IF bandwidth of eight times the bit rate. An IF bandwidth of two times the bit rate causes an SNR penalty of approximately 1.3 dB when compared to an IF bandwidth of eight times the bit rate.

#### **3.4.5 Selection of Demodulator Loop Bandwidth**

The best loop bandwidth is a function of the mission bit rate and the bandwidth of the incidental phase modulation. The loop bandwidth should be wide enough to track out any large amplitude incidental phase modulation. The BER with no incidental phase modulation starts to increase if the loop bandwidth is wider than approximately 2% of the bit rate for a PM demodulator and 5% of the bit rate for a PSK demodulator.

#### **3.4.6 RF Spectra**

Radio frequency spectra are presented in figures 3.4-13 through 3.4-26 for 400 kb/s pseudo-random biphase PCM/PM with various premodulation filters and peak deviations of 60, 75, and 90 degrees. Figures 3.4-13 and 3.4-14 show the spectra that result with no premodulation filter. The IRIG criteria of 60 dB below the unmodulated carrier is not met in a 20-MHz bandwidth under these conditions. The occupied bandwidth is approximately eight times the bit rate for premodulation filters whose bandwidth is equal to the bit rate and twelve to sixteen times the bit rate for premodulation filters whose bandwidth is equal to twice the bit rate. The sideband levels are higher for larger peak deviations and generally higher with constant delay (CD) premodulation filters than with constant amplitude (CA) premodulation filters.

250 kb/s Biphasse-Level PCM  
FILTER=500 KHz 5-POLE LINEAR PHASE

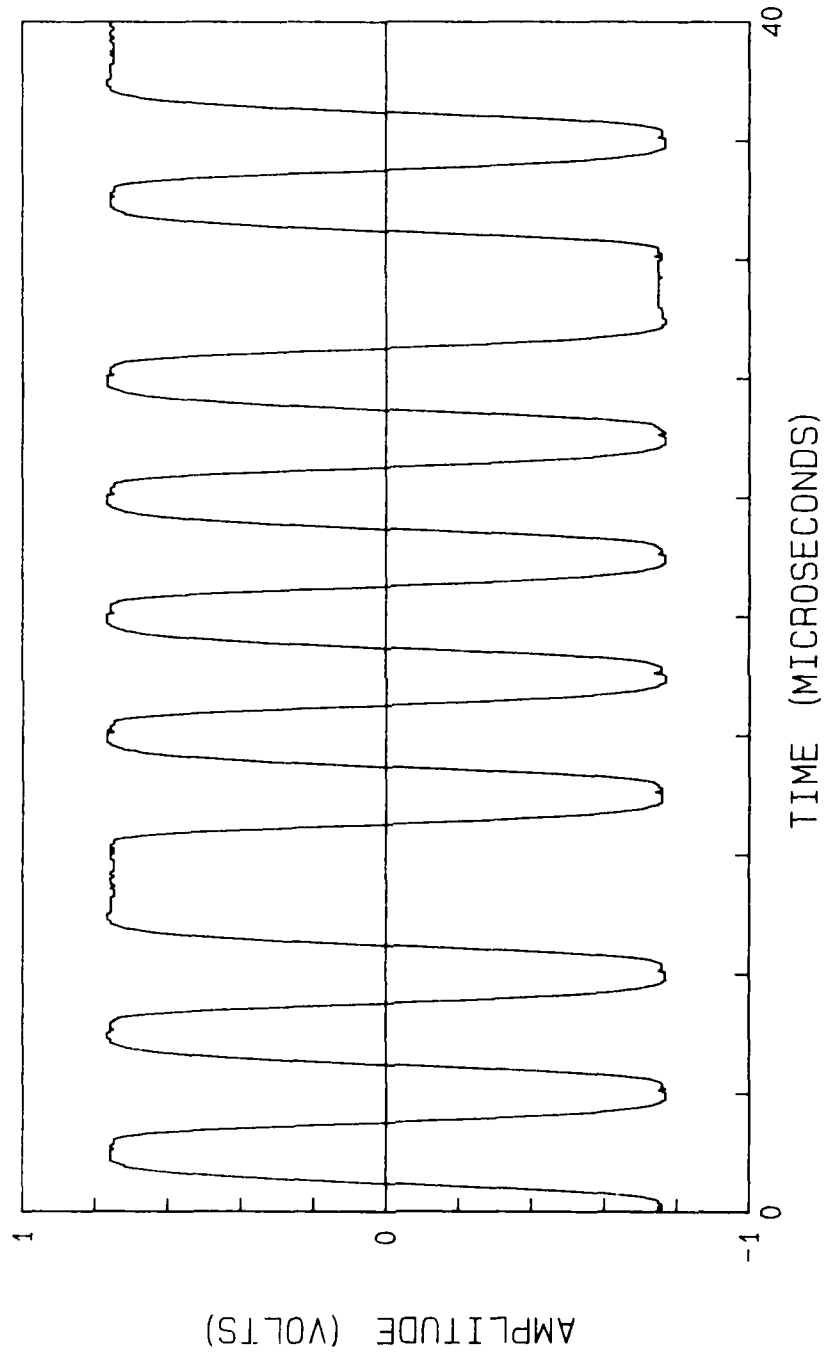


Figure 3.4-8. Biphasse Signal with PREMOD BW=2 Times Bit Rate (CD)

500 kb/s Biphase-Level PCM  
FILTER=700 KHz 5-POLE CD

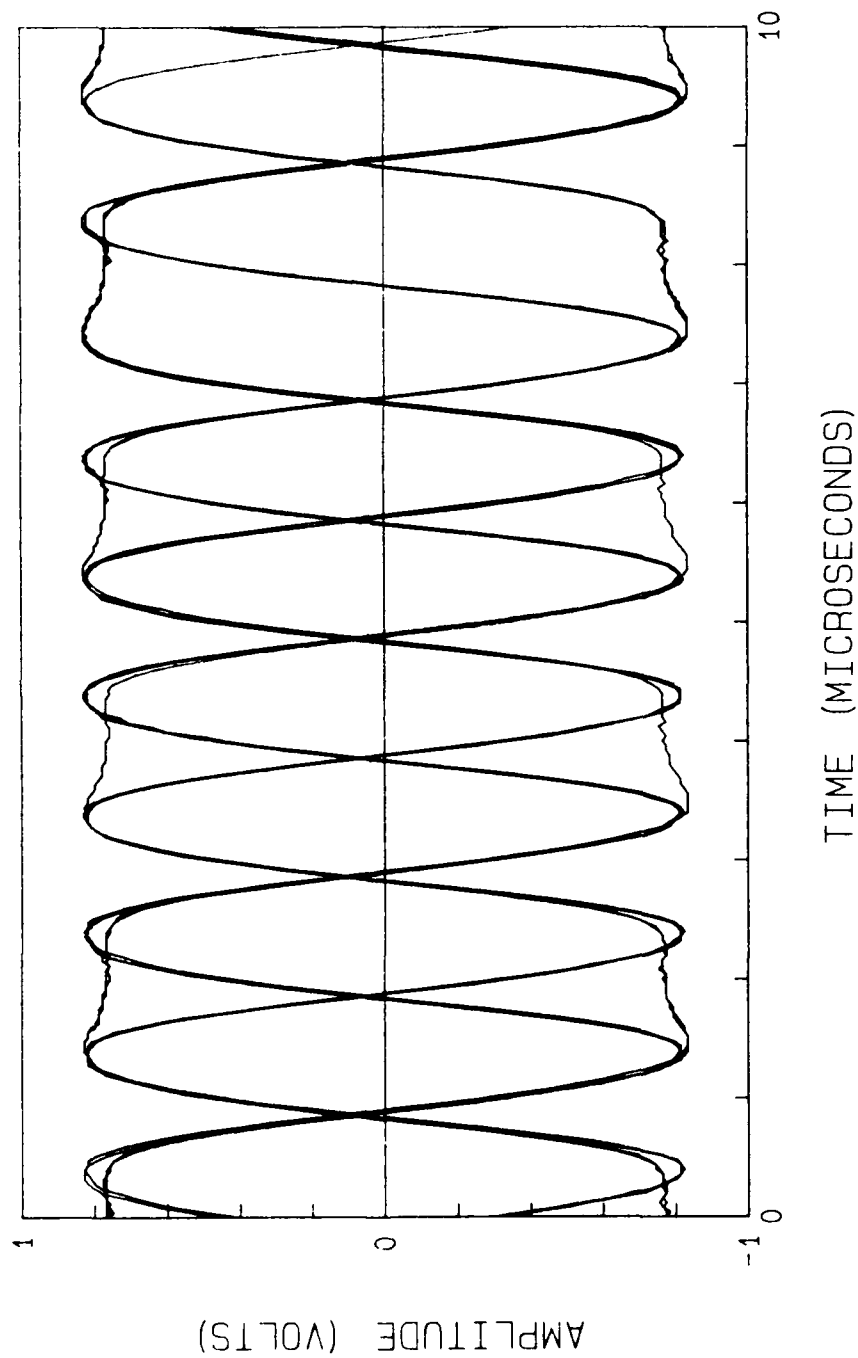


Figure 3.4-9. Biphase Eye Pattern with PREMOD BW=1.4 Bit Rate.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
--------------------	------------------	--------------	---------------	------	-------------	------------

+	BIØ-L PCM/PM	500	1000	1000	CD	60
o	BIØ-L PCM/PM	500	1500	1000	CD	60
*	BIØ-L PCM/PM	500	4000	1000	CD	60

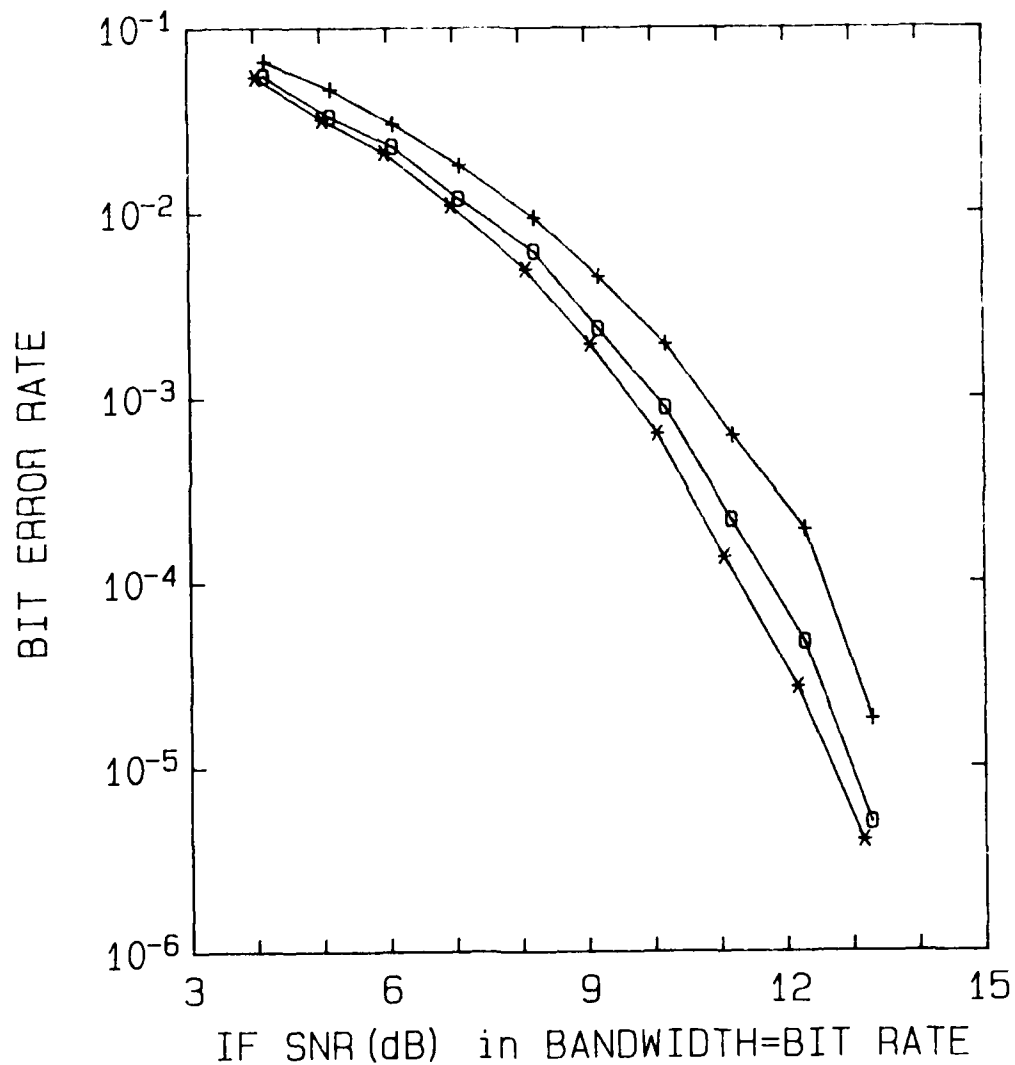


Figure 3.4-10. BER for Peak DEV=60 DEG, IF BW/Bit Rate=2, 3, and 8.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	PEAK DEV	BIT DET
0 BIØ-L PCM/PM	500	1000	1000	CD	75
+ BIØ-L PCM/PM	500	1500	1000	CD	75
o BIØ-L PCM/PM	500	4000	1000	CD	75
* BIØ-L PCM/PM	500	10000	1000	CD	75

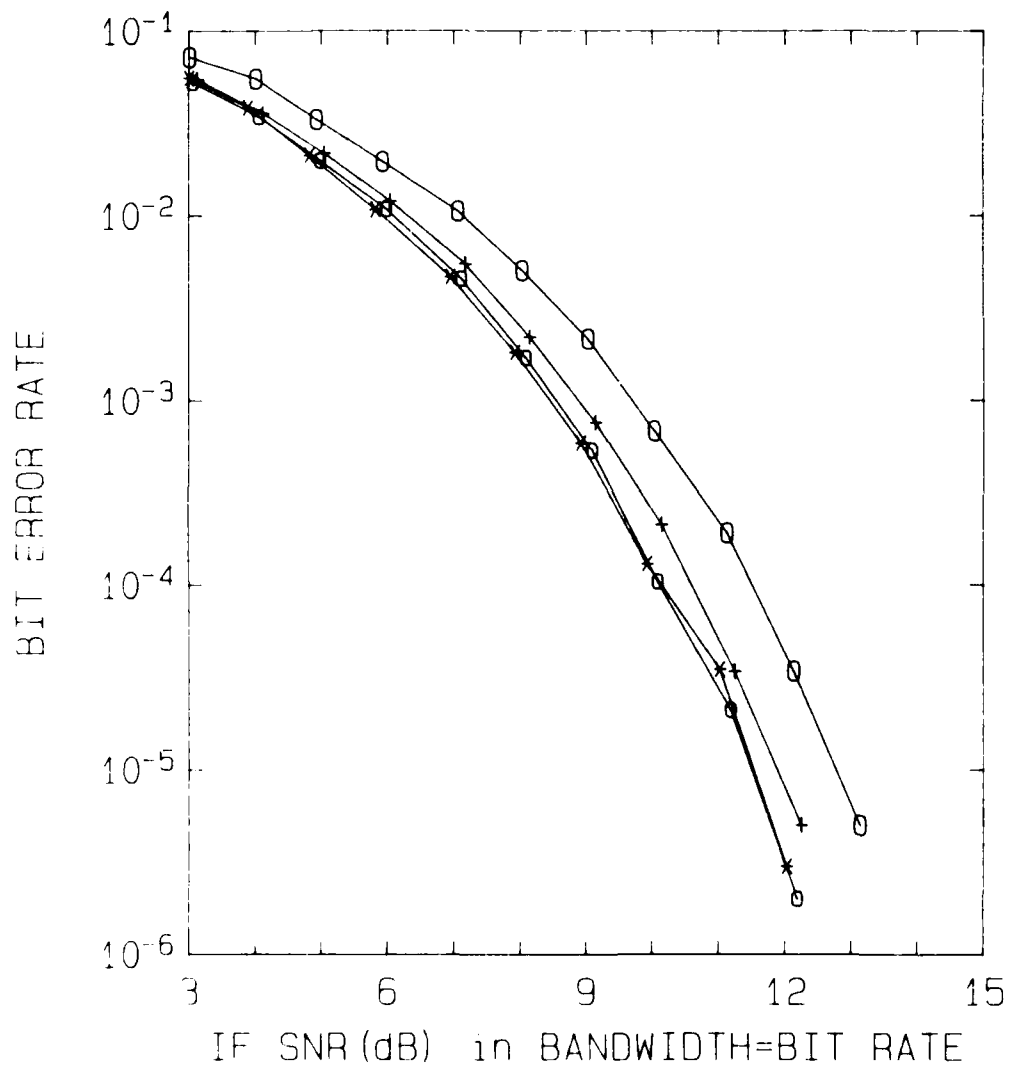


Figure 3.4-11. BER for Peak DEV=75 DEG, IF BW/Bit Rate=2, 3, 8, and 20.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
0 BIØ-M PCM/PM	500	1000	1000	CD	90	
+ BIØ-M PCM/PM	500	1500	1000	CD	90	
o BIØ-M PCM/PM	500	4000	1000	CD	90	
* BIØ-M PCM/PM	500	10000	1000	CD	90	

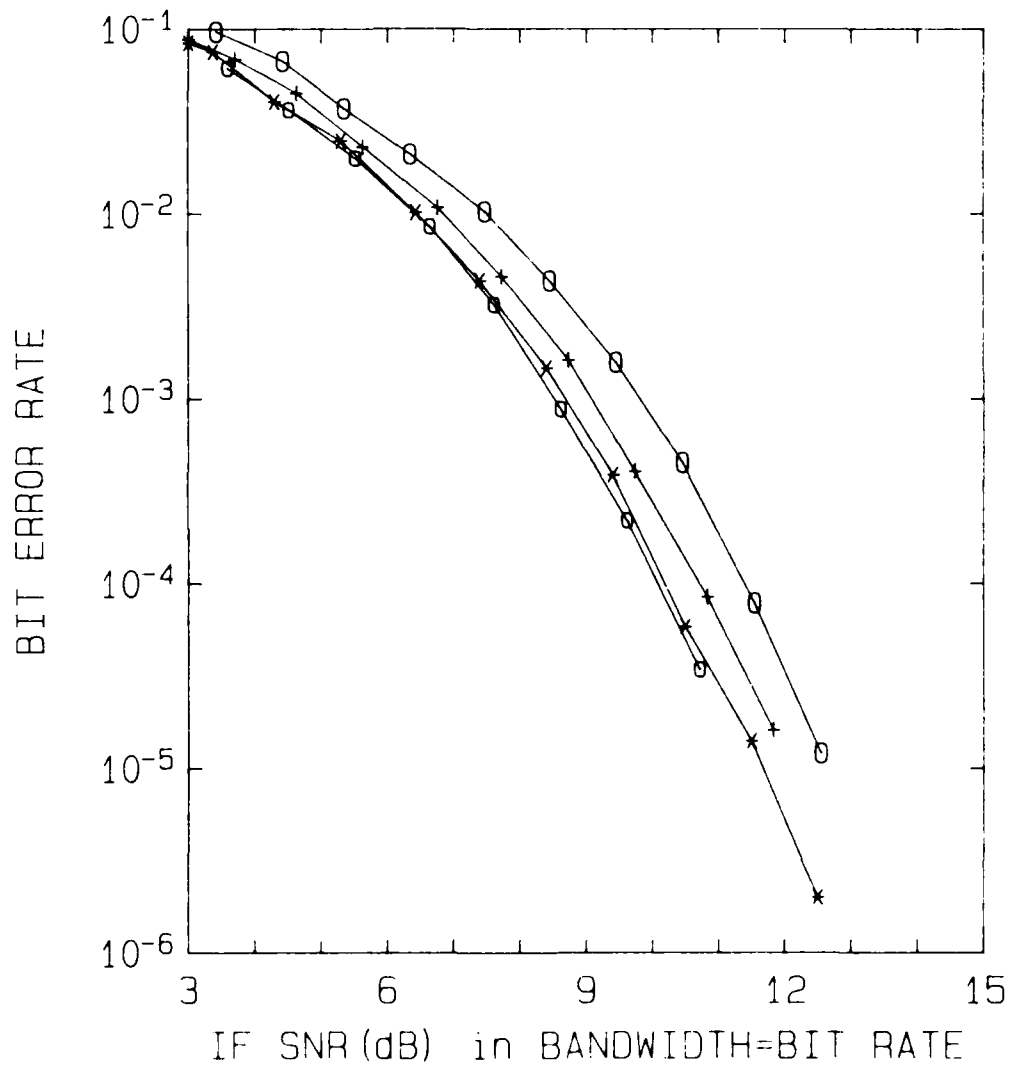


Figure 3.4-12. BER for Peak DEV=90 DEG, IF BW/Bit Rate=2, 3, 8, and 20.

400 kb/s BIPHASE PCM/PM 2047 BIT PN  
PREMOD FILTER= NONE  
PEAK DEVIATION= 75 DEGREES  
RESOLUTION BW= 30 kHz VIDEO BW= 100 Hz

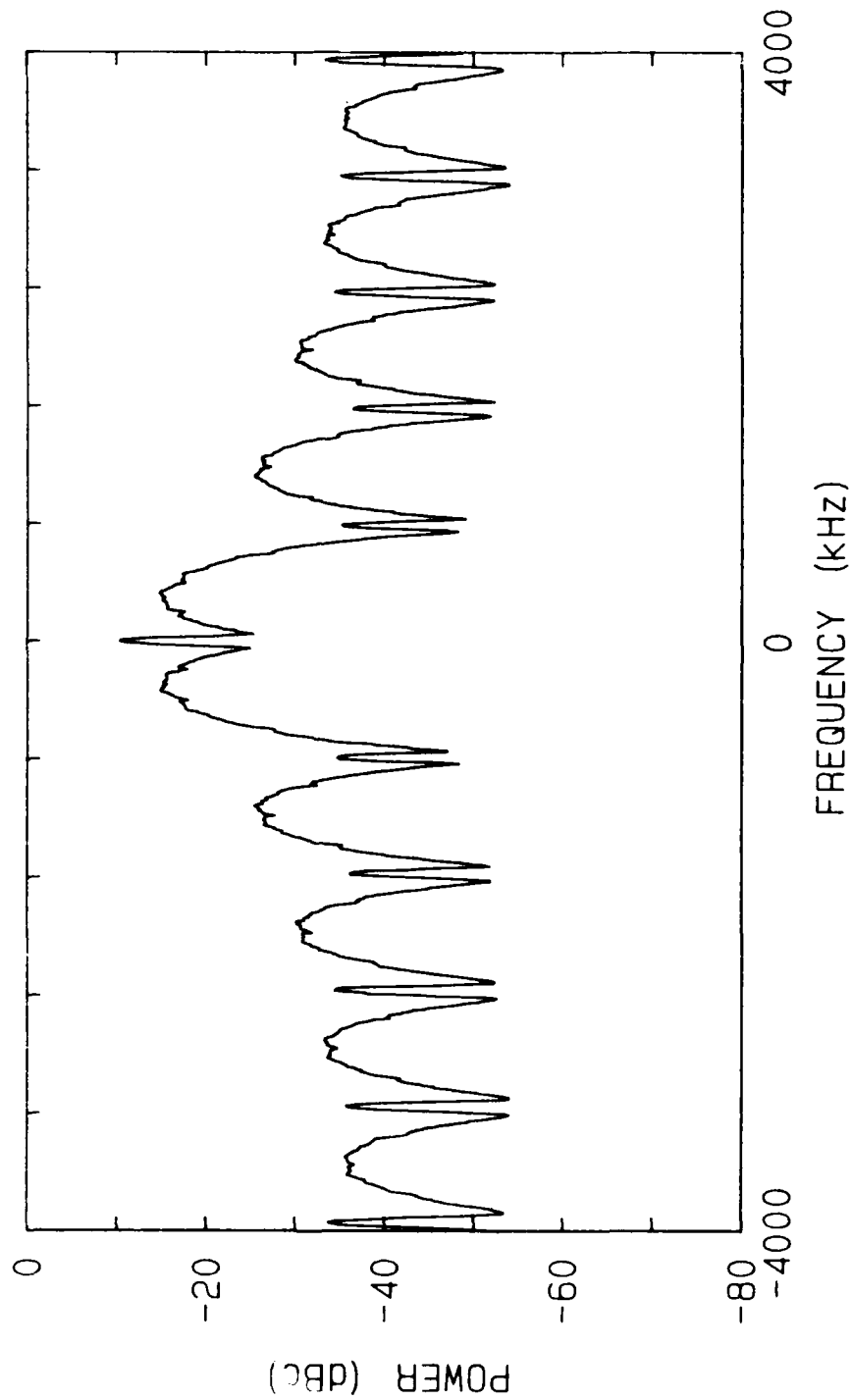


Figure 3.4-13. 400 kb/s Biphase PCM/PM RF Spectrum (PREMOD=None, DEV=75 Degrees) .

400 kb/s BIPHASE PCM/PM 2047 BIT PN  
PREMOD FILTER= NONE  
PEAK DEVIATION= 75 DEGREES  
RESOLUTION BW= 30 kHz VIDEO BW= 100 Hz

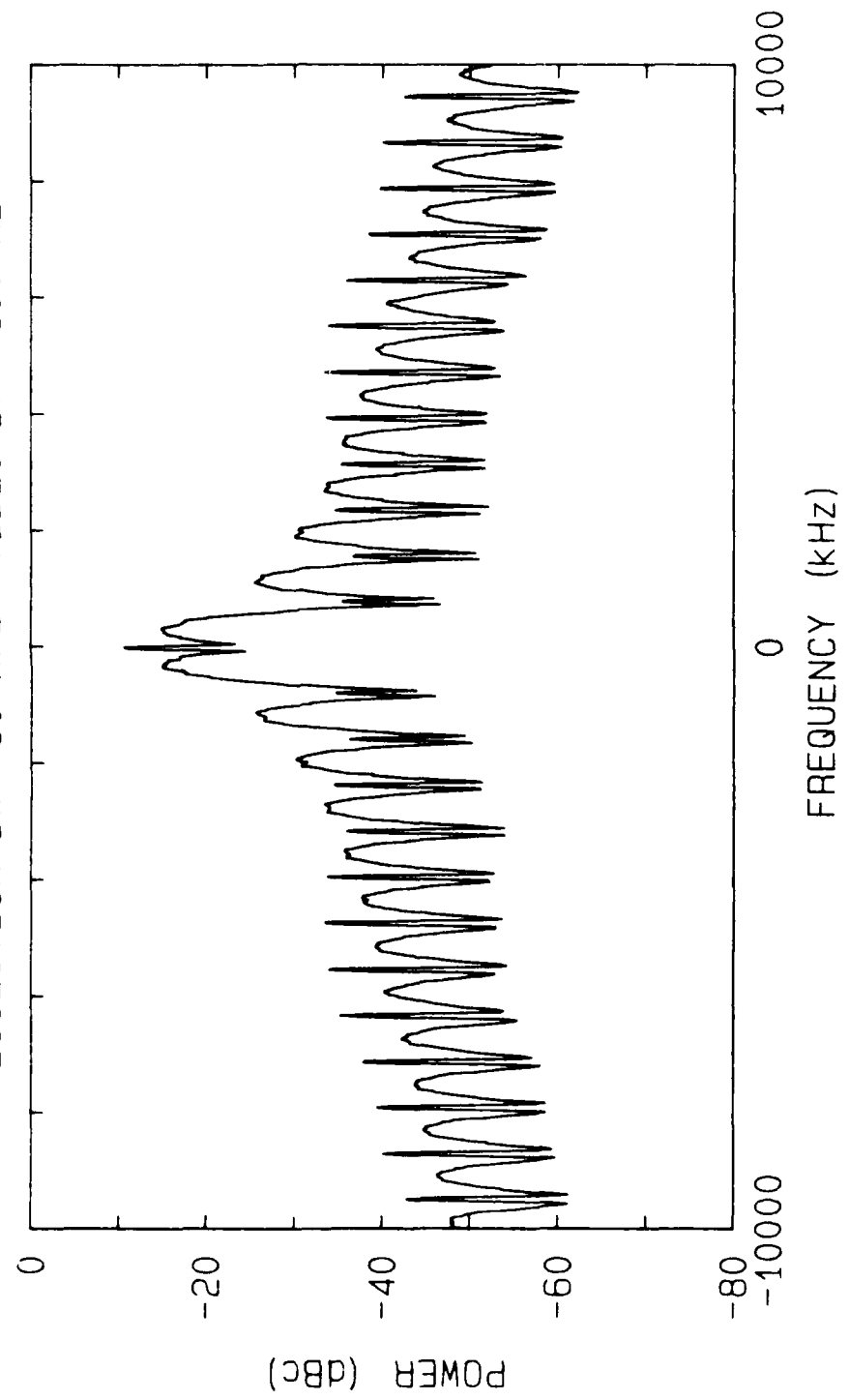


Figure 3.4-14. 400 kb/s Biphase PCM/PM RF Spectrum (20 MHz Bandwidth).



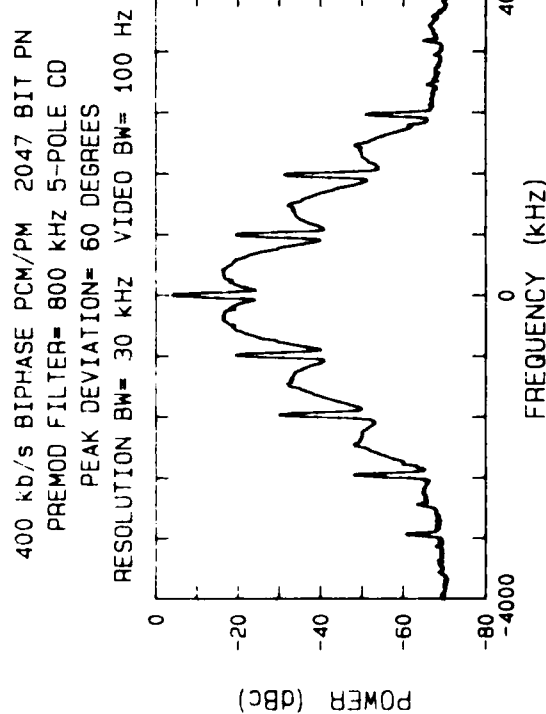


Figure 3.4-15. RF Spectrum PREMOD=800 kHz CD Peak DEV=60 Degrees.

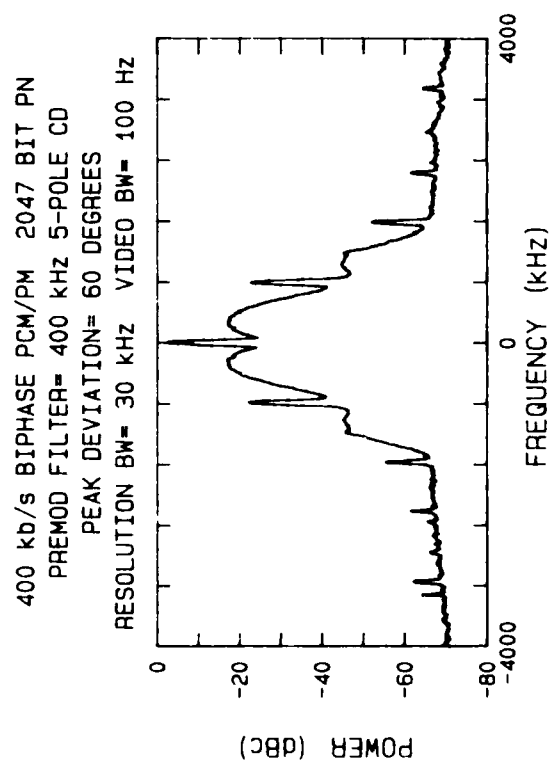


Figure 3.4-17. RF Spectrum PREMOD=400 kHz CD Peak DEV=60 Degrees.

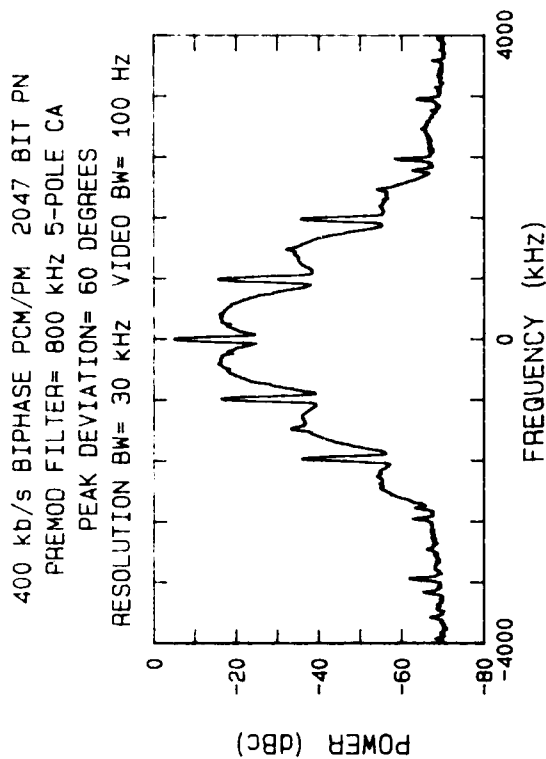


Figure 3.4-16. RF Spectrum PREMOD=800 kHz CA Peak DEV=60 Degrees.

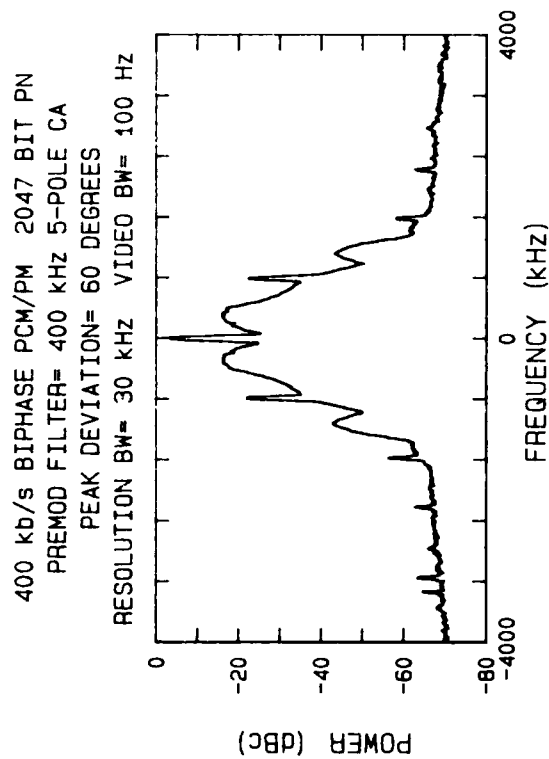


Figure 3.4-18. RF Spectrum PREMOD=400 kHz CA Peak DEV=60 Degrees.

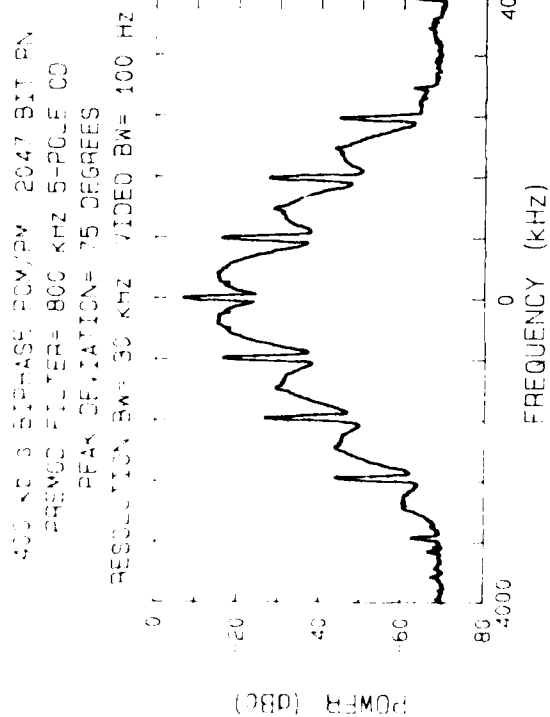


Figure 3.4-19. RF Spectrum PREMOD=800 kHz CD Peak DEV=75 Degrees.

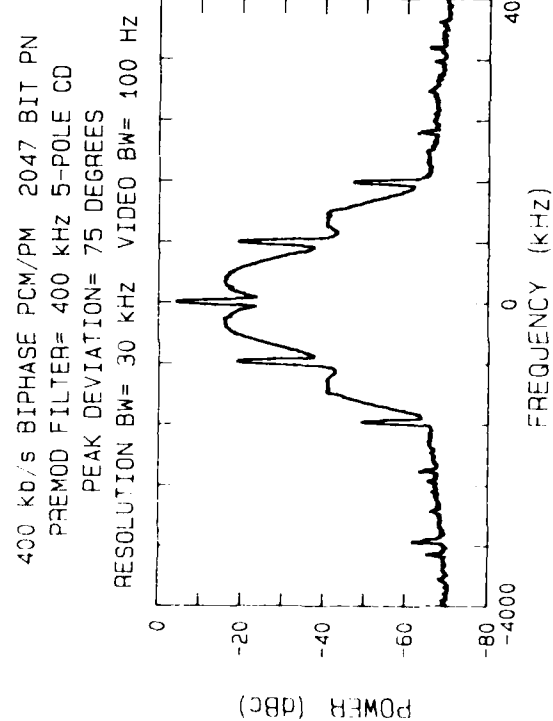


Figure 3.4-21. RF Spectrum PREMOD=400 kHz CD Peak DEV=75 Degrees.

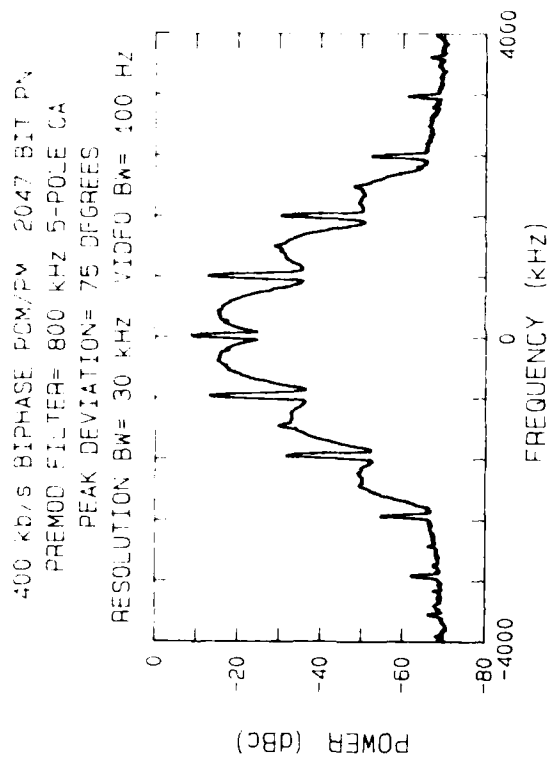


Figure 3.4-20. RF Spectrum PREMOD=800 kHz CA Peak DEV=75 Degrees.

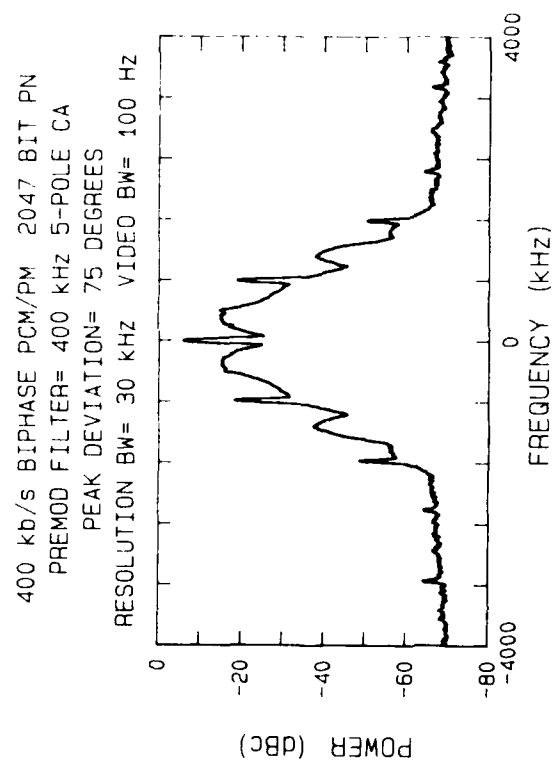


Figure 3.4-22. RF Spectrum PREMOD=400 kHz CA Peak DEV=75 Degrees.

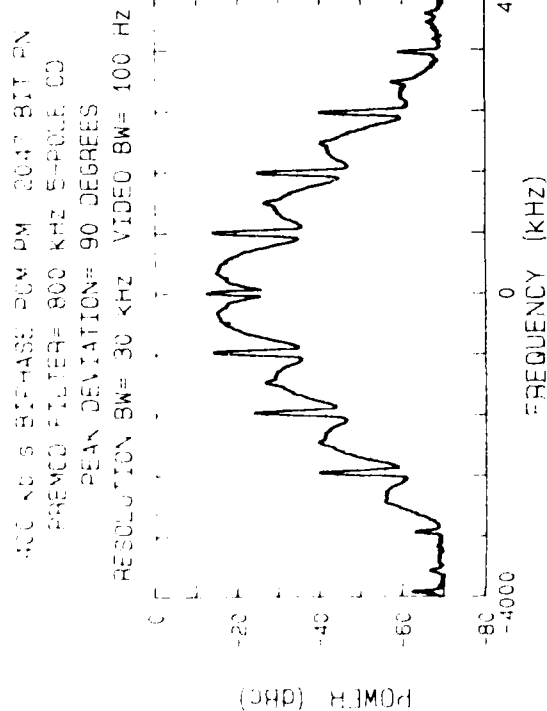


Figure 3.4-23. RF Spectrum PREMOD=800 kHz CO Peak DEV=90 Degrees.

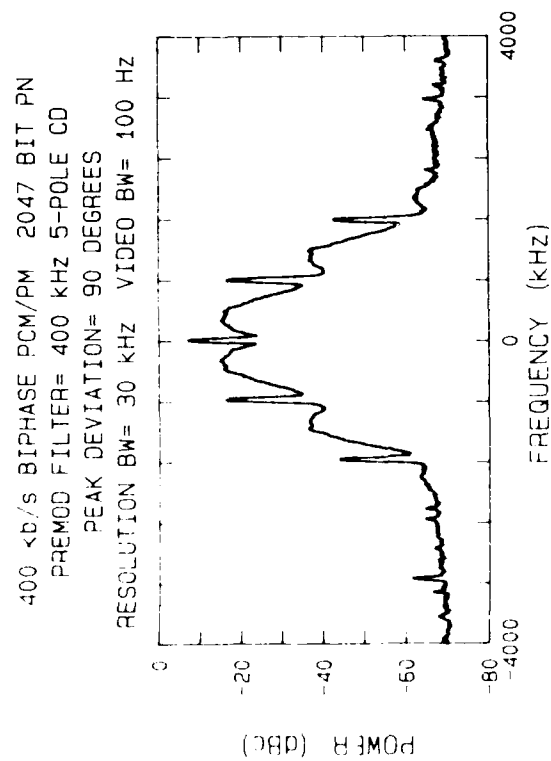


Figure 3.4-25. RF Spectrum PREMOD=400 kHz CO Peak DEV=90 Degrees.

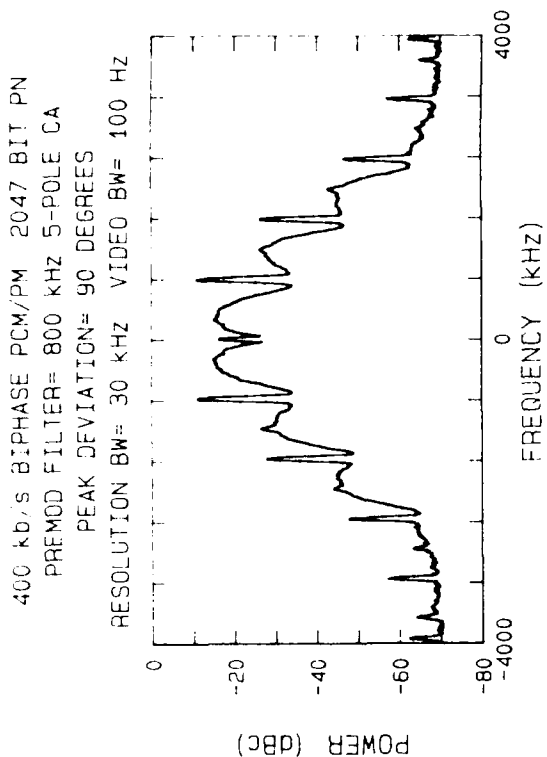


Figure 3.4-24. RF Spectrum PREMOD=800 kHz CA Peak DEV=90 Degrees.

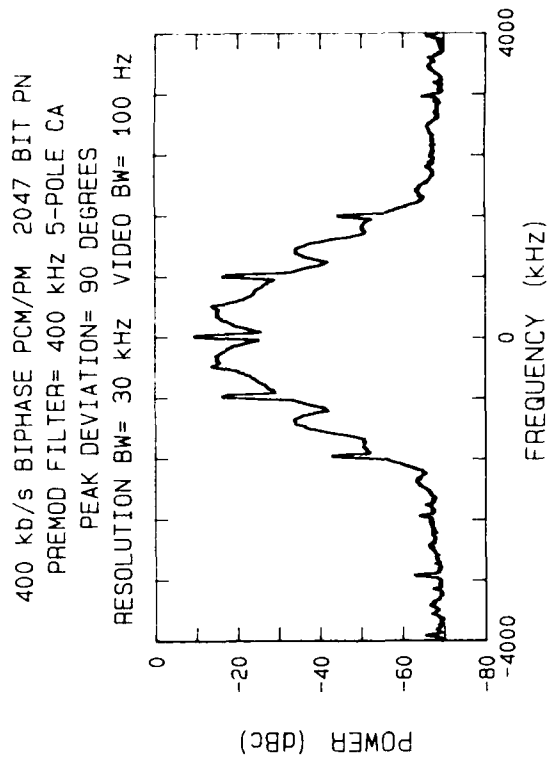


Figure 3.4-26. RF Spectrum PREMOD=400 kHz CA Peak DEV=90 Degrees.

### 3.5 PHASE SHIFT KEYING

Phase shift keying (PSK) is a method for transmitting digital data in which the carrier is multiplied by +1 if one state of a binary digital signal is to be transmitted, and -1 if the other state is to be transmitted. This produces two signals which are exact opposites of each other (antipodal). The multiplication is usually accomplished using a double-balanced mixer. The usual implementation is as a differential PSK (DPSK) signal where the information is contained in the phase changes (amplitude inversions) rather than in the absolute phase values. This solves the polarity inversion problem at the demodulator output (see section 3.3). DPSK involves the use of an NRZ-M or NRZ-S waveform instead of an NRZ-L waveform. The performance of PSK is very similar to the performance of PCM/PM(90). The major differences include:

1. If the signals applied to the double-balanced mixer are properly adjusted, the spectral spikes can be minimized or eliminated entirely. Therefore, the occupied bandwidth of a PSK signal may be narrower than the occupied bandwidth of a PCM/PM (90) signal.
2. A PSK signal where the modulating signal has been filtered does not have a constant amplitude (see figure 3.5-1). If this PSK signal is passed through a device with a non-linear amplitude response, the occupied bandwidth increases. Therefore, if the carrier is amplitude modulated before the final amplifier stage, the final amplifier must be operated in the linear region. This reduces gain and efficiency. The other option for spectral control is to use a bandpass filter after the final amplification. Small, low loss, stable, narrow band, inexpensive filters are difficult to build at 2 GHz.
3. The insertion loss of double-balanced mixers is typically 6 to 7 dB. This means that the signal must be amplified more to make up for this loss.
4. The modulator for PSK is simpler than the modulator for PCM/PM.

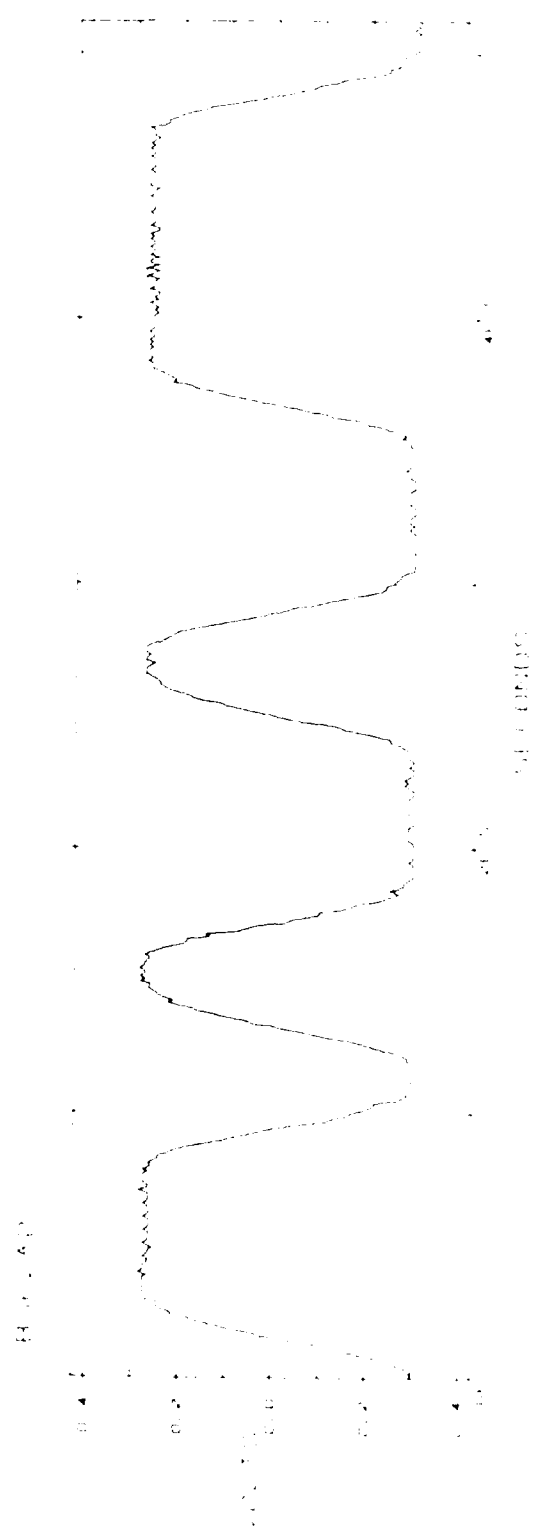
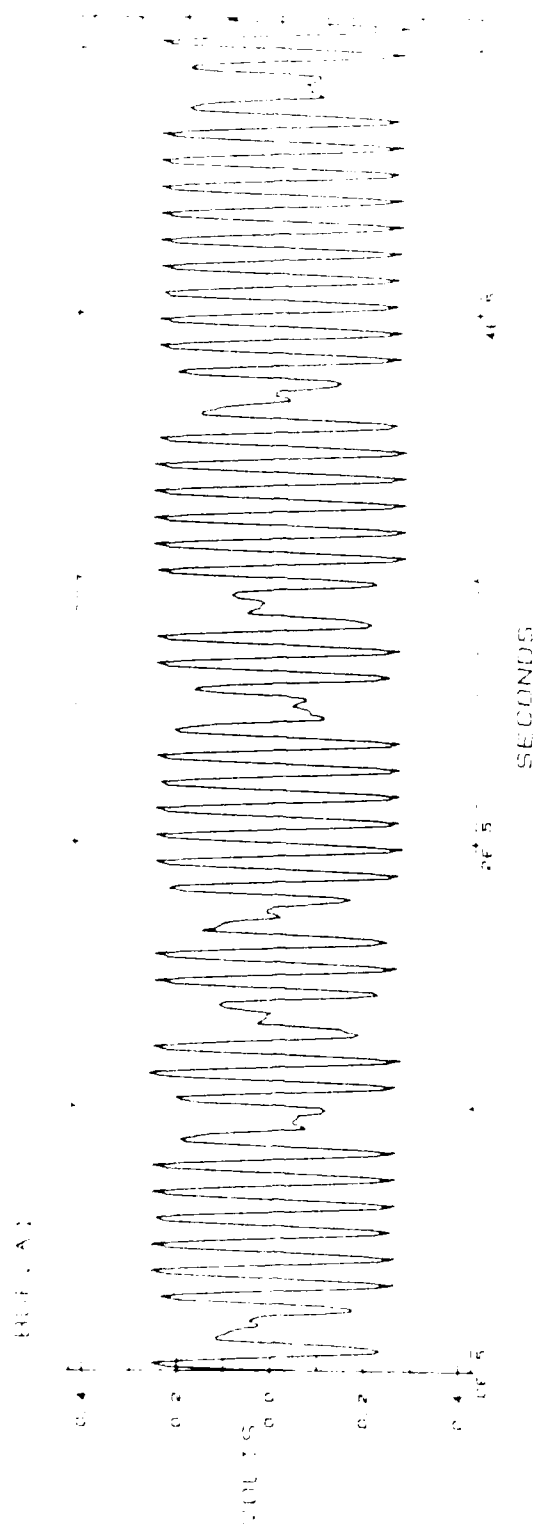


Figure 3.1-1. PPS Waveform (Upper Trace) and PPS Signal.

### 3.6 PULSE AMPLITUDE MODULATION/FREQUENCY MODULATION

#### 3.6.1 Introduction

The terms pulse amplitude modulation (PAM) and frequency modulation (FM) indicate a modulation technique<sup>9,10,11,12</sup> in which the analog information signal is periodically sampled and the samples are used to frequency modulate the carrier signal. The NRZ-PAM/FM technique is easily employed in analog systems designs since it only requires a commutator (electronic switch) to produce the amplitude levels. PAM is the simplest form of time-division multiplexing (TDM) for analog source signals because the samples of data are transmitted without conversion to another form. A very important requirement of PAM, as with any TDM system, is that the decommutator be correctly synchronized with the commutator. As a result, it is necessary to include synchronization signals in the commutated data. The IRIG Telemetry Standards specify that the synchronization pattern for NRZ-PAM shall be, in the order given: zero scale for a period  $T$ , full scale for a period  $3T$ , and a level not to exceed 50% of full scale for a period  $T$ , where  $T = 1/(\text{PAM channel rate})$ . The channel immediately following this pattern is defined to be channel 1. Data channels cannot be properly sorted out until the decommutator recognizes the synchronization pattern, thus identifying the time space allotted to each data channel.

There are two major sampling methods for NRZ-PAM. These methods are frequently referred to as flat-top and natural sampling. These methods are illustrated in figures 3.6-1 and 3.6-2, respectively. The difference between the methods is that a sample-and-hold circuit is part of the commutator circuitry with flat-top sampling. When natural sampling is used, the signal variations during the sampling time are passed on as part of the PAM signal (figure 3.6-2).

#### 3.6.2 RF Deviation

The most commonly used values for NRZ-PAM peak RF deviation are 125 kHz for PAM channel rates below 50 kCh/s and 2.5 times the PAM channel rate for rates above 50 kCh/s, e.g., a 100 kCh/s PAM signal would typically use a 250 kHz peak deviation. A peak deviation of 2.5 times the channel rate will result in a raw decommutator output rms noise level of approximately 2% of full scale for a 12 dB IF SNR and a receiver IF bandwidth between 1.2 and 2 times the peak-to-peak PAM RF deviation (this assumes that the rms value of incidental FM is less than 1% of the peak-to-peak deviation). The peak-to-peak transmitter deviation should be at least 50 times the peak incidental FM expected for frequencies between 50 kHz and the PAM channel rate.

<sup>9</sup>Taub, H. and D. L. Schilling. *Principles of Communication Systems*. McGraw-Hill, New York, pp 162-179, 1971.

<sup>10</sup>Gregg, W. D. *Analog and Digital Communication*. John Wiley and Sons, New York, pp 267-294, 1977.

<sup>11</sup>Downing, J. J. *Aerospace Telemetry, Volume I*. (ed. by H. L. Stiltz). Prentice-Hall, Englewood Cliffs, NJ, pp 83-141, 1961.

<sup>12</sup>Hochman, D. *Handbook of Telemetry and Remote Control*. (ed. by E. L. Gruenberg). McGraw-Hill, New York, pp 9-2 to 9-198, 1967.

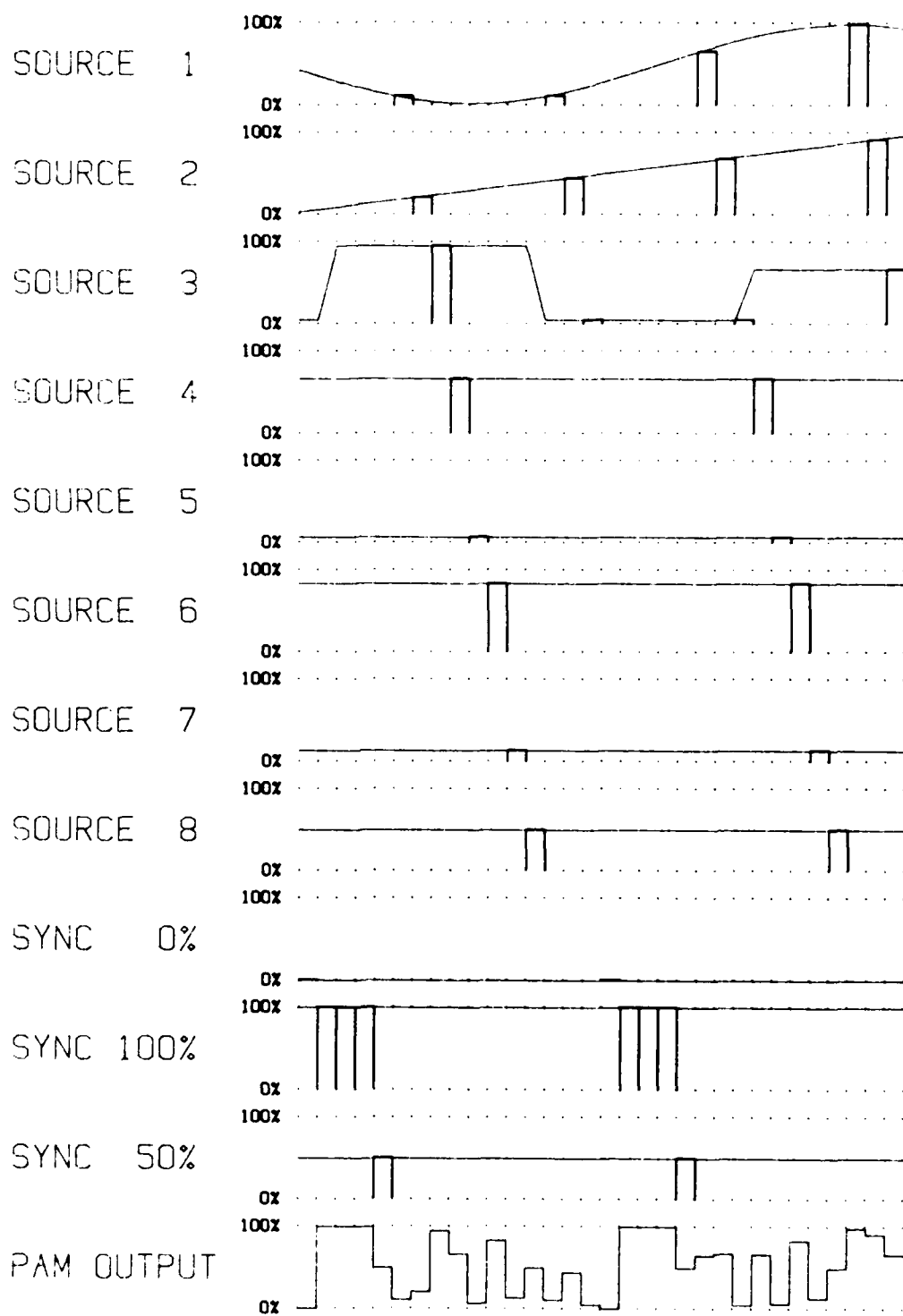


Figure 3.6-1. NRZ PAM Signal with Flat-Top Sampling.

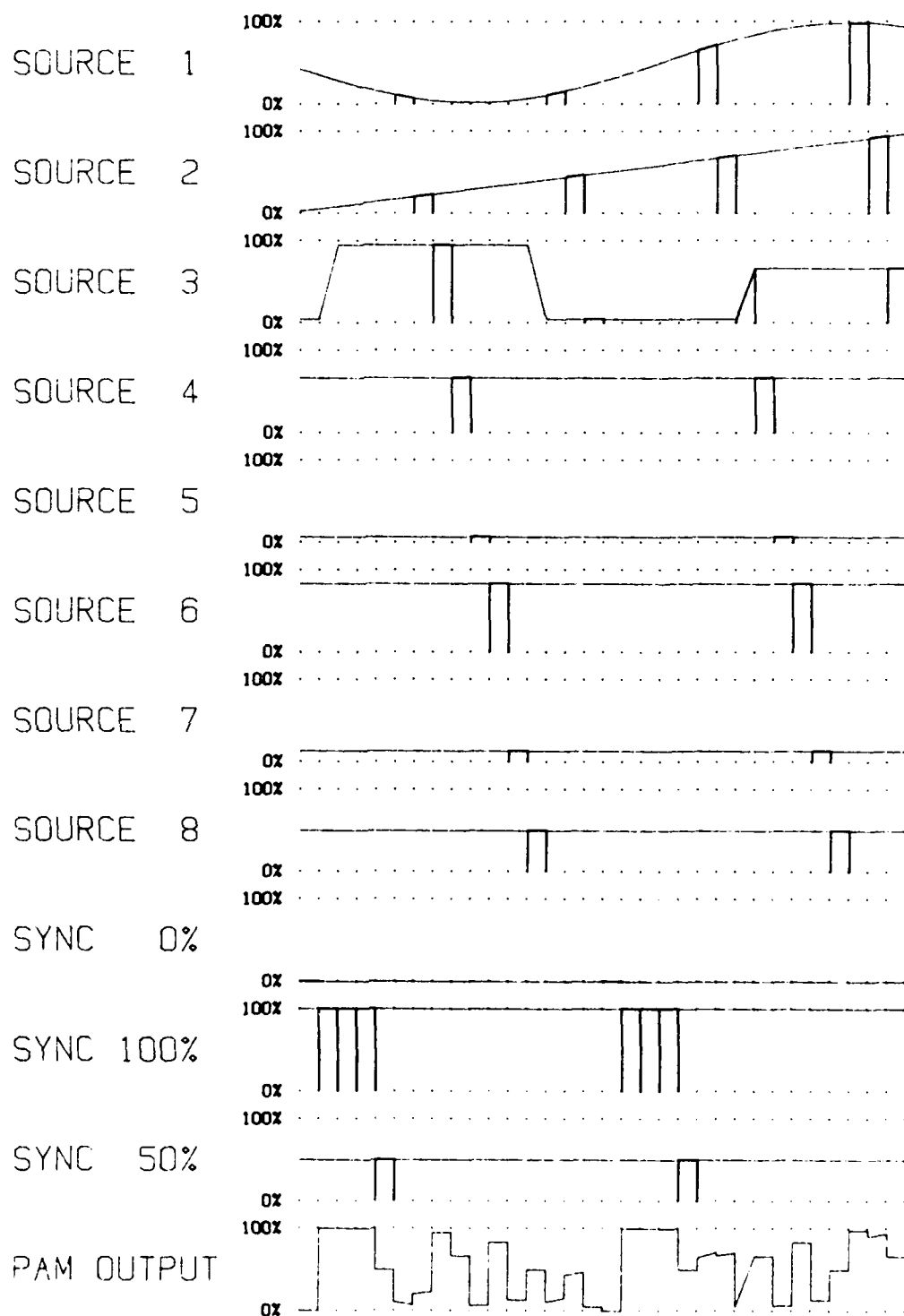


Figure 3.6-2. NRZ PAM Signal with Natural Sampling.



### 3.6.3 Premodulation Filter

The recommended premodulation filter bandwidth for NRZ PAM is twice the PAM channel rate<sup>13</sup>. The filter should be a 4- to 6-pole linear phase low-pass filter. A 1-pole RC filter can also be used. The primary disadvantage of a 1-pole filter is that the PAM baseband and RF spectra roll off more slowly.

### 3.6.4 SNR at Output of NRZ PAM Demodulator

An equation which can be used to calculate the signal-to-noise ratio (SNR) at the output of a PAM demodulator will be described in this section. It has been assumed that the receiver is above FM threshold and that all noise is due to wideband, white, Gaussian noise at the demodulator input. This equation will relate the rms noise to full scale signal (peak-to-peak). In other words, if the rms value of the noise is 1% of full scale (100 mV rms noise for 0 V to 10 V output) the SNR will be 40 dB ( $20 \log (10/0.1)$ ). Other publications have used various definitions of SNR. A common one is to define the signal as the rms value of a full scale sine wave. The definition used in this section gives SNRs which are 9 dB greater than the rms sine wave definition. The full scale signal definition is used here because most error analysis is done as a percentage of full scale. This section will also show plots of the effects of noise on DC signals and triangle waves for various SNRs.

A typical PAM demodulator can be modeled as a linear phase low-pass filter followed by a synchronized sample and hold. The typical low-pass filter bandwidth is equal to the PAM channel rate. Therefore, the output SNR (in dB) can be calculated using the normal equation for low-pass filtered FM above FM threshold:

$$(S/N)_{PAM} = SNR_{IF} + F_{CORR} + 20 \log \left\{ \frac{(12 B_{IF})^{1/2} \Delta f}{(B_{LPF})^{3/2}} \right\}$$

where:

$F_{CORR}$  is the correction factor due to non-ideal filters  
 $SNR_{IF}$  is the IF SNR  
 $B_{IF}$  is the IF equivalent noise power bandwidth  
 $B_{LPF}$  is the low-pass filter bandwidth  
 $\Delta f$  is the peak deviation.

Typical values for  $F_{CORR}$  are -3 to -6 dB depending on the number of poles in the filter and the accuracy of the -3 dB point.

<sup>13</sup>Heberling, E. D. *An Experimental Evaluation of the Characteristics of PAM-NRZ/FM Telemetry Systems*. Naval Ordnance Laboratory Corona, Corona, California, September 1967. (NOLC Report 741).

Assume:

25 kCh/s PAM

$B_{IF} = 640$  kHz equivalent noise power bandwidth

$\Delta f = 125$  kHz peak deviation

$SNR_{IF} = 15$  dB IF SNR

$F_{CORR} = -6$  dB filter correction factor

then:

$$(S/N)_{PAM} = 15 - 6 + 20 \log \left\{ \frac{[12 (640)]^{1/2} 125}{(25)^{3/2}} \right\} = 47.9 \text{ dB}$$

The measured SNR under these conditions varied between 47 and 48 dB. The calculated SNRs agree well with the measured SNRs for IF SNRs between approximately 12 and 20 dB. This is illustrated in figure 3.6-3. At higher IF SNRs, other sources of noise are also significant. The maximum PAM output SNR was approximately 60 dB for the hardware and test parameters used in this test. At IF SNRs below 12 dB, the noise at the input to the PAM demodulator includes "pop" noise. Therefore, the SNR is much lower than predicted by the equations. The PAM demodulator also has trouble keeping track of the proper time to sample the signal. The PAM output SNR decreased by 3 dB when the IF SNR decreased from 15 to 12 dB, by 9 dB when the IF SNR decreased from 12 to 9 dB, and by 15 dB when the IF SNR decreased from 9 to 6 dB.

The PAM output SNR is also lower for signals near 0% or 100% of full scale than for signals near 50% of full scale when the IF SNR is below 12 dB. This is shown in figure 3.6-4. There are two main reasons for this degradation:

1. The number of noise pops is proportional to the difference between the signal frequency and the average noise frequency.
2. The receiver IF filter usually attenuates signals deviated towards bandedge more than signals in the center of the bandpass.

The receiver bandpass filter used for the data shown in figure 3.6-4 was skewed towards a frequency higher than the center frequency. Therefore, the average noise frequency was between 50% and 100% of full scale. This caused the 0% full scale signal to have the most noise pops and the lowest SNR.

Sample unfiltered PAM demodulator output noise time domain plots are presented in figures 3.6-5 through 3.6-13. In these figures, the PAM channel rate was 25 kCh/s, the peak deviation was 125 kHz, and the receiver IF bandwidth was approximately 640 kHz. These figures show the increase in noise as the IF SNR is decreased. Figure 3.6-10 shows the effects of the average noise frequency being higher than the receiver center frequency. The largest noise spikes in figure 3.6-10 go towards 100% of full scale. The reason for this is that the average noise frequency is greater than the 50% full scale signal frequency. Figures 3.6-11 through 3.6-13 show the effects of noise on a triangular modulation signal for IF SNRs of 12, 9, and 6 dB respectively.

The calculations presented above assume that there is no additional filtering at the channel outputs of the PAM demodulator. The noise consists of a series of pulses with duration equal to the time between samples of the signal being monitored and amplitude equal to the error between the actual output and the correct value. The

normalized power is equal to the rms error squared. This produces a noise power spectrum which takes the form of:

$$k \sin^2(\pi f/f_s) / (\pi f/f_s)^2$$

where  $f_s$  is the sampling rate of the signal and  $k$  is proportional to the rms error squared.

We can now calculate the S/N at the output of a low-pass filter following the raw decommutated output (output gate). The filter improvement was calculated by numerically integrating the product of the noise power spectrum and the filter response. This was done for a 4-pole Bessel filter and a 1-pole RC filter for various filter cutoffs relative to the sample rate (see table 3.6-1).

**Table 3.6-1. SNR improvement for various low-pass filters after docummutated output (compared to raw decommutated output).**

SAMPLE RATE/ FILTER CUTOFF	SNR IMPROVEMENT (dB)	
	4-POLE BESSEL	1-POLE RC
1	0.7	0.7
5	4.1	3.65
10	6.9	5.9
20	9.8	8.5
40	12.7	11.3

Measured improvements were within 0.5 dB of the values in Table 3.6-1 for IF SNRs above 8 dB. The data in Table 3.6-1 shows that if we sample a function 1000 times per second and use a 100 Hz RC filter on the output we reduce the noise by nearly 6 dB compared to no filter.

### 3.6.5 Other Sources of Error in PAM

There are several other sources of error (differences between source signal and decommutated output) in a PAM system. These sources are usually insignificant at low IF SNRs but may be dominant at high IF SNRs. The sources include:

1. Incidental FM in either transmitter or receiver
2. Nonlinearities in either transmitter modulator or receiver demodulator
3. Crosstalk with adjacent PAM channels
4. Tape recorder flutter
5. Crosstalk with other signals modulating the same transmitter
6. Gain and offset errors in the vehicle signal conditioner
7. Noise in the vehicle instrumentation package, telemetry receiver, or PAM decommutator.

Because of the many sources of error, PAM systems are usually specified to have absolute accuracies between 2 and 5 percent of full scale.

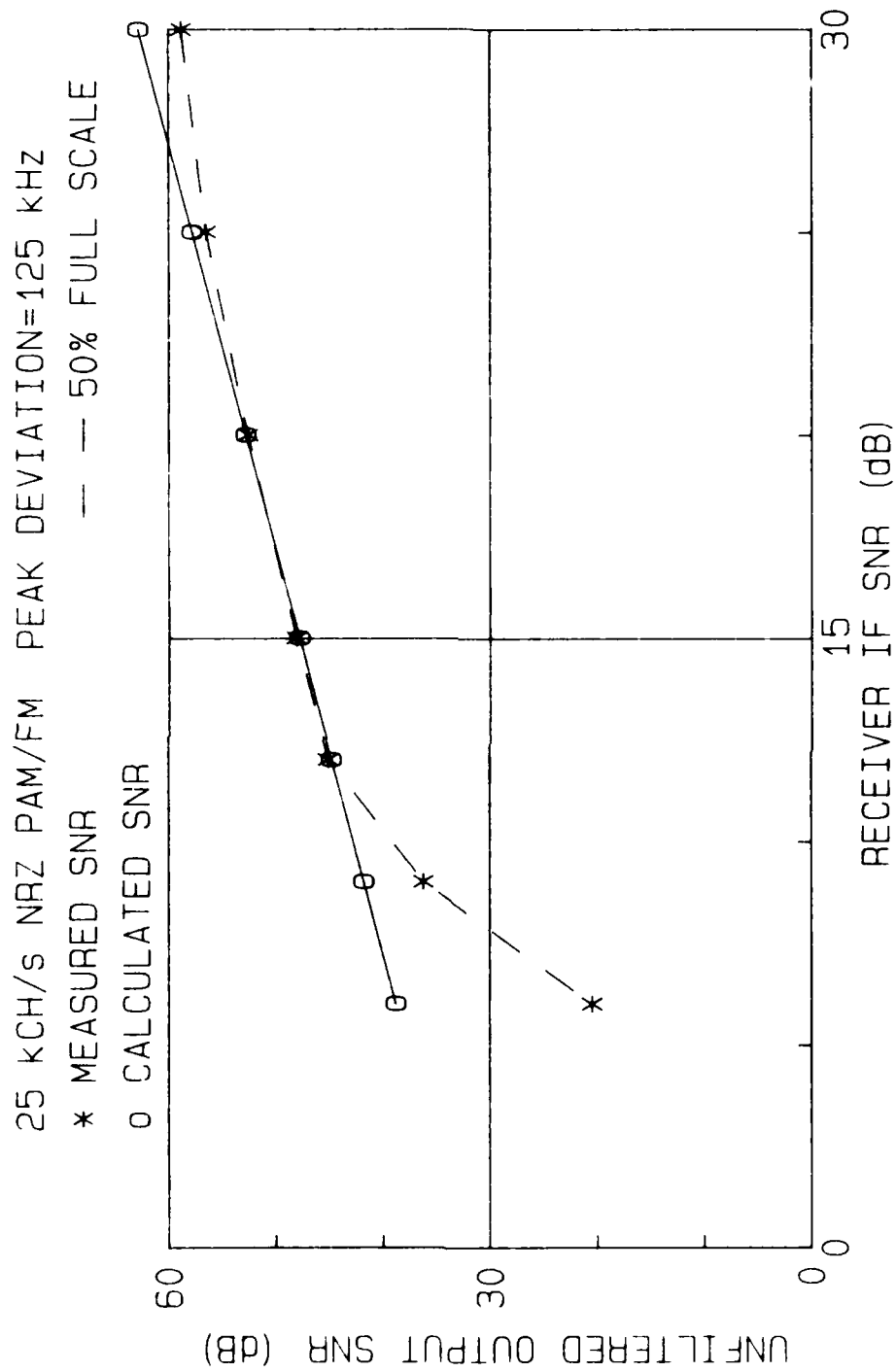


Figure 3.6-3. Measured and Calculated PAM Output SNR Versus IF SNR.

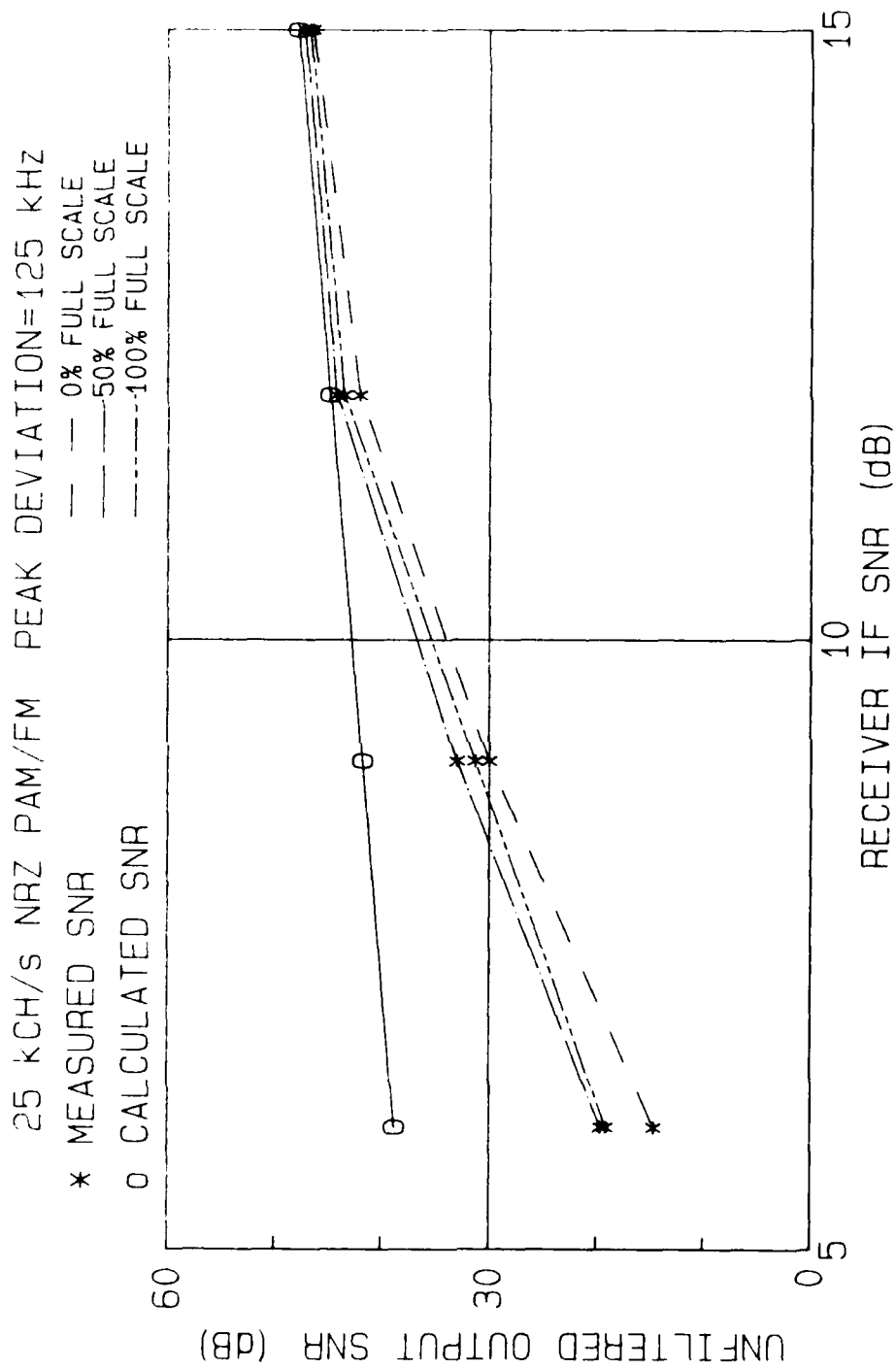


Figure 3.6-4. Measured and Calculated PAM SNR for 0, 50, and 100% Levels.

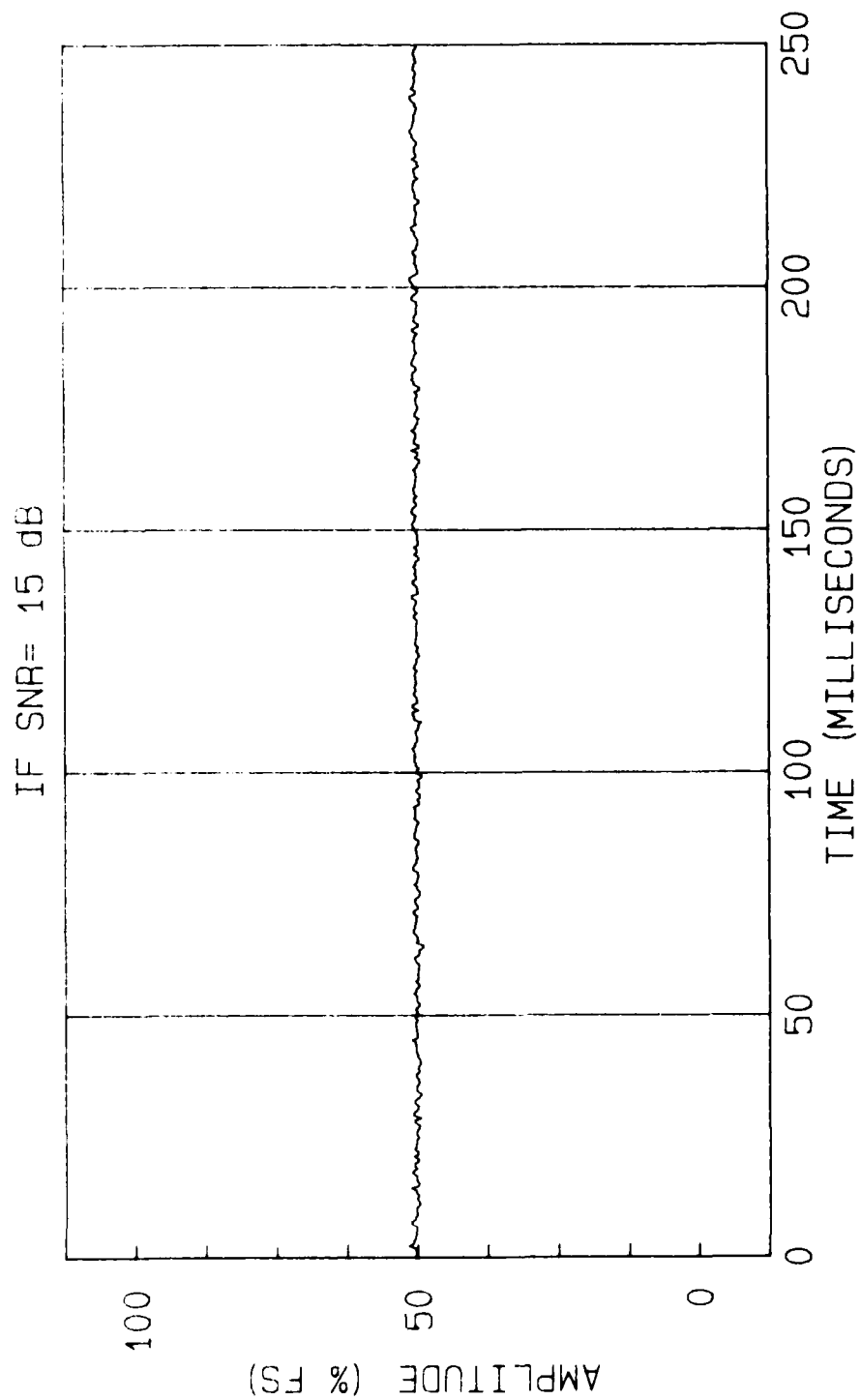


Figure 3.6-5. PAM DECOM Output for 15 dB IF SNR with 50% FS Modulation.

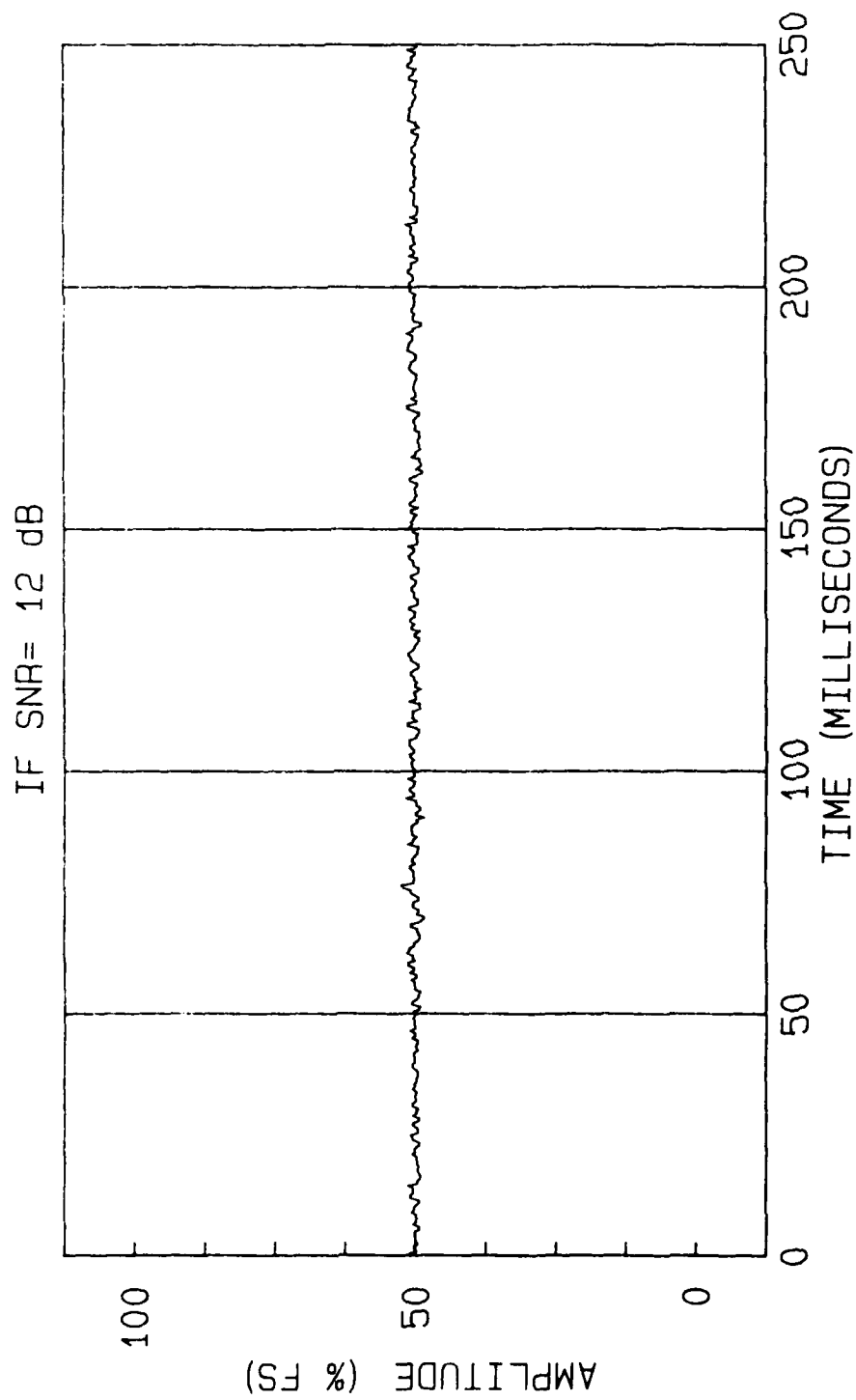


Figure 3.6-6. PAM DECOM Output for 12 dB IF SNR with 50% FS Modulation.

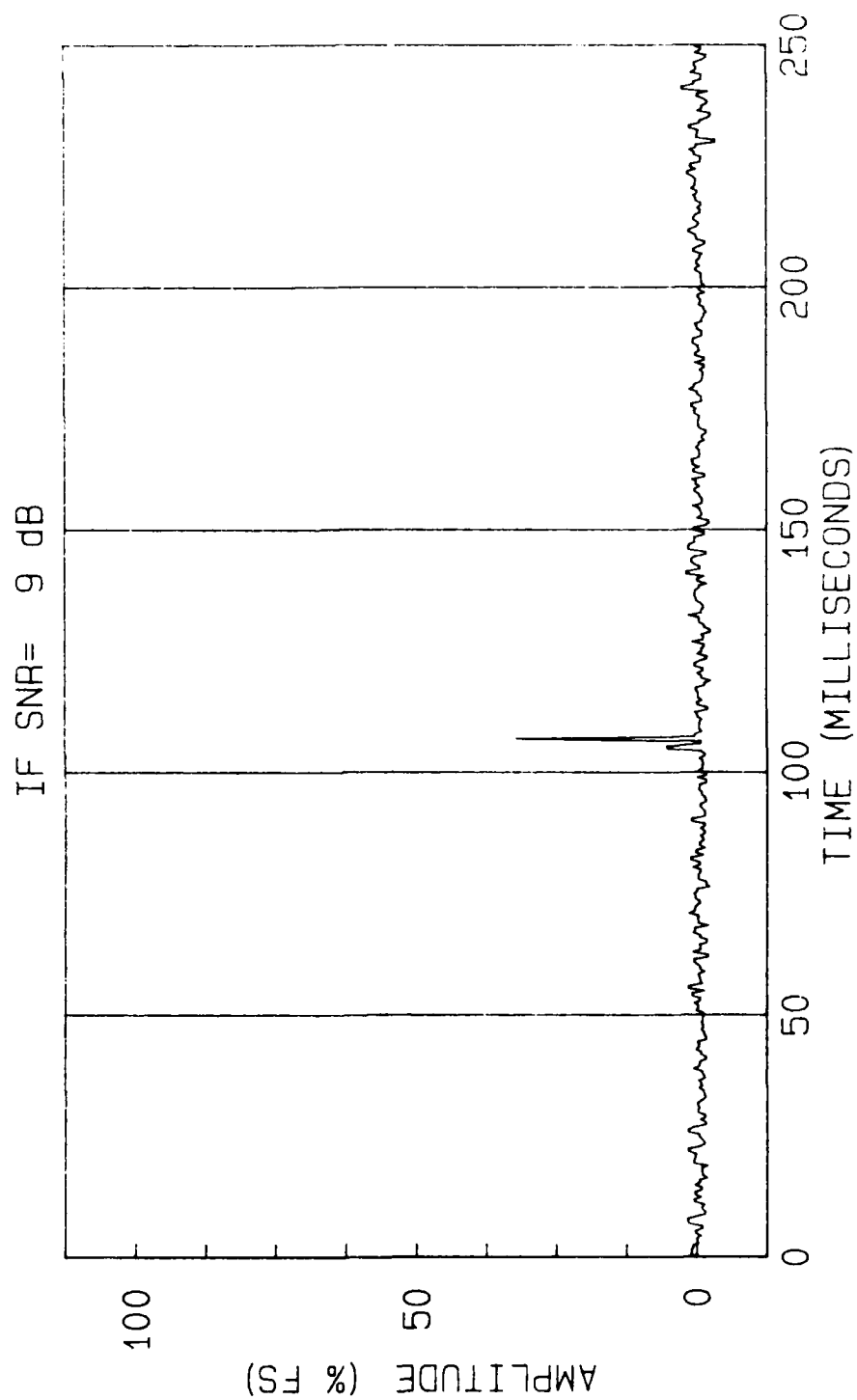


Figure 3.6-7. PAM DECOM Output for 9 dB IF SNR with 0% FS Modulation.



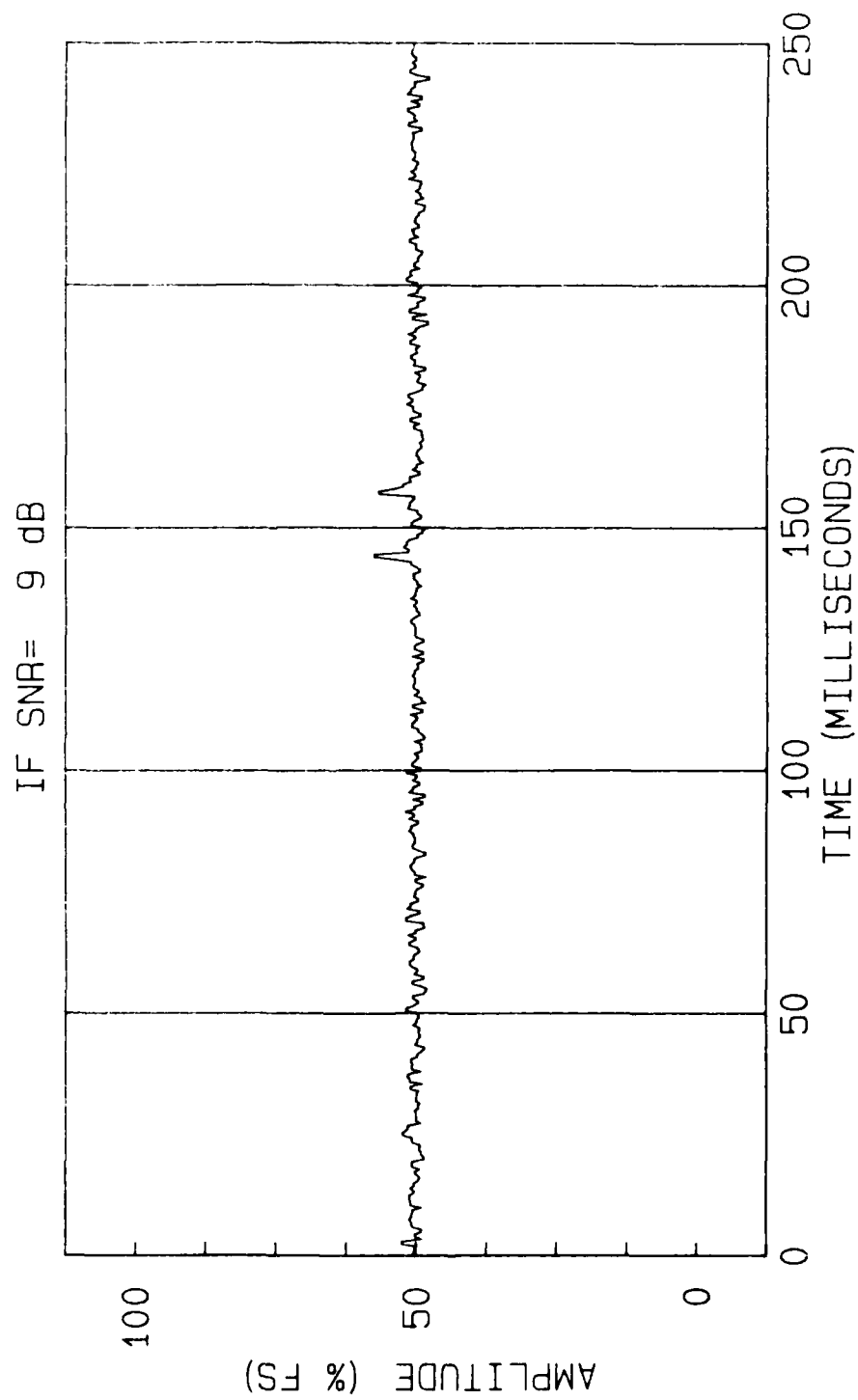


Figure 3.6-8. PAM DECOM Output for 9 dB IF SNR with 50% FS Modulation.

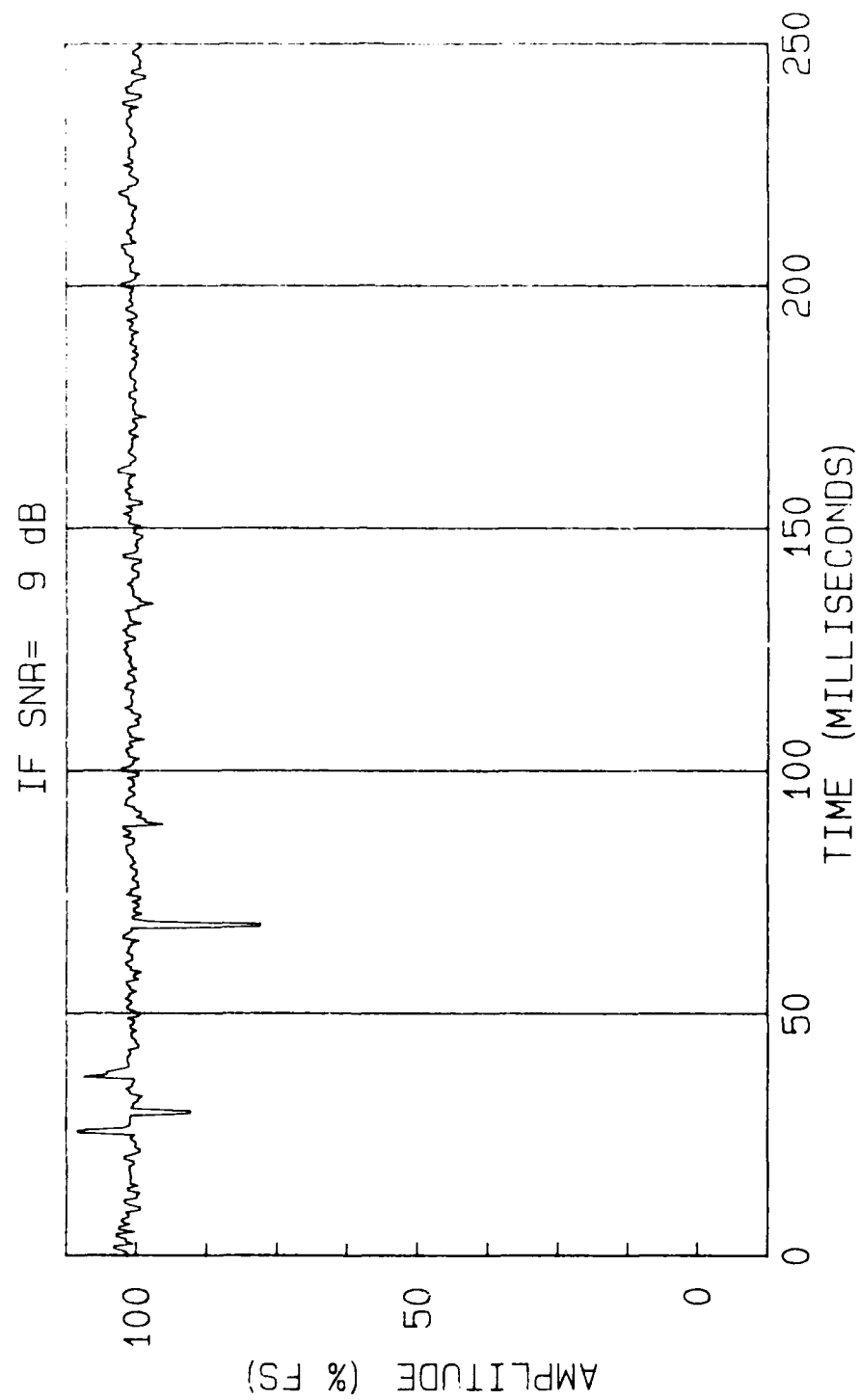


Figure 3.6-9. PAM DECOM Output for 9 dB IF SNR with 100% FS Modulation.

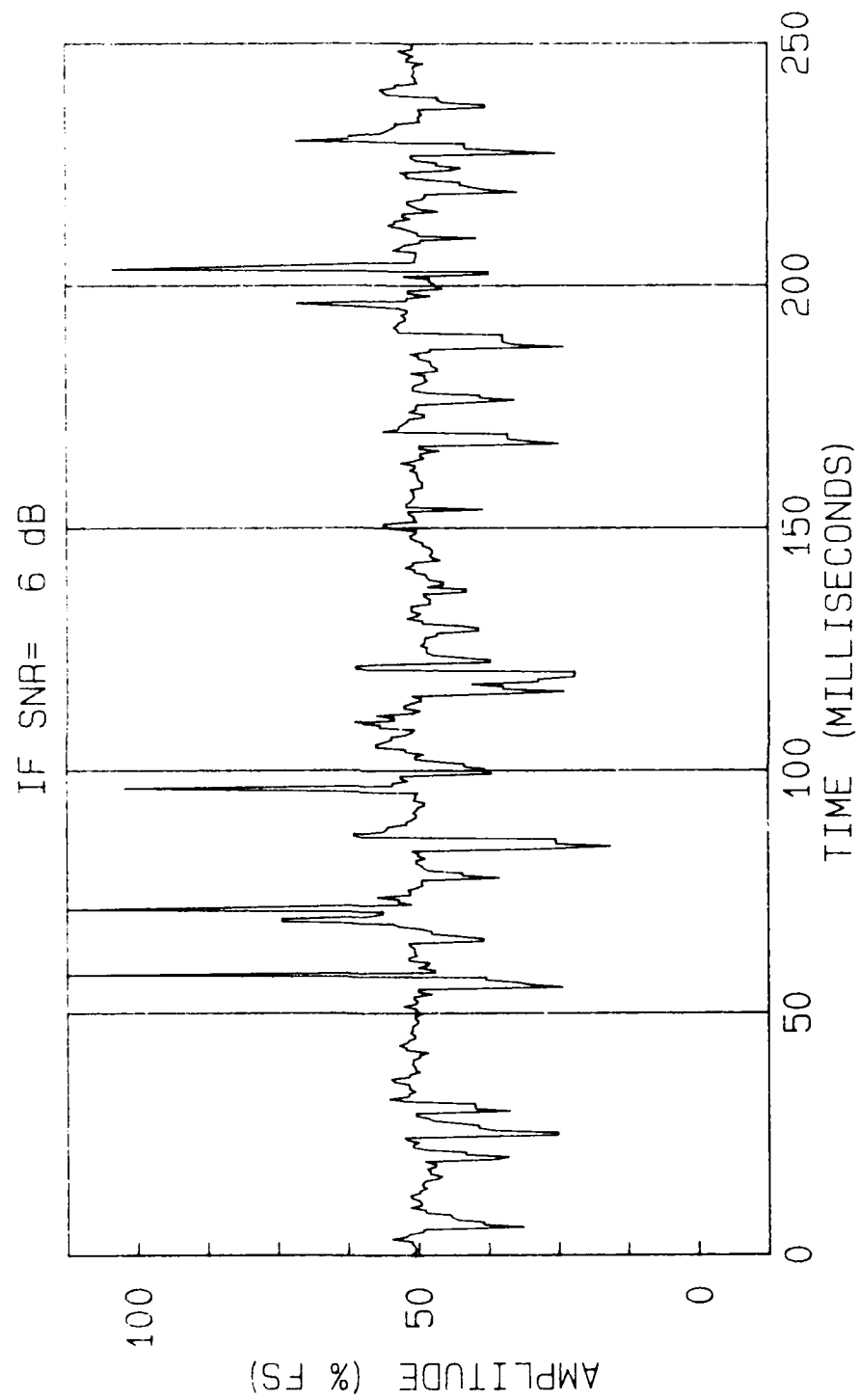


Figure 3.6-10. PAM DECOM Output for 6 dB IF SNR with 50% FS Modulation.

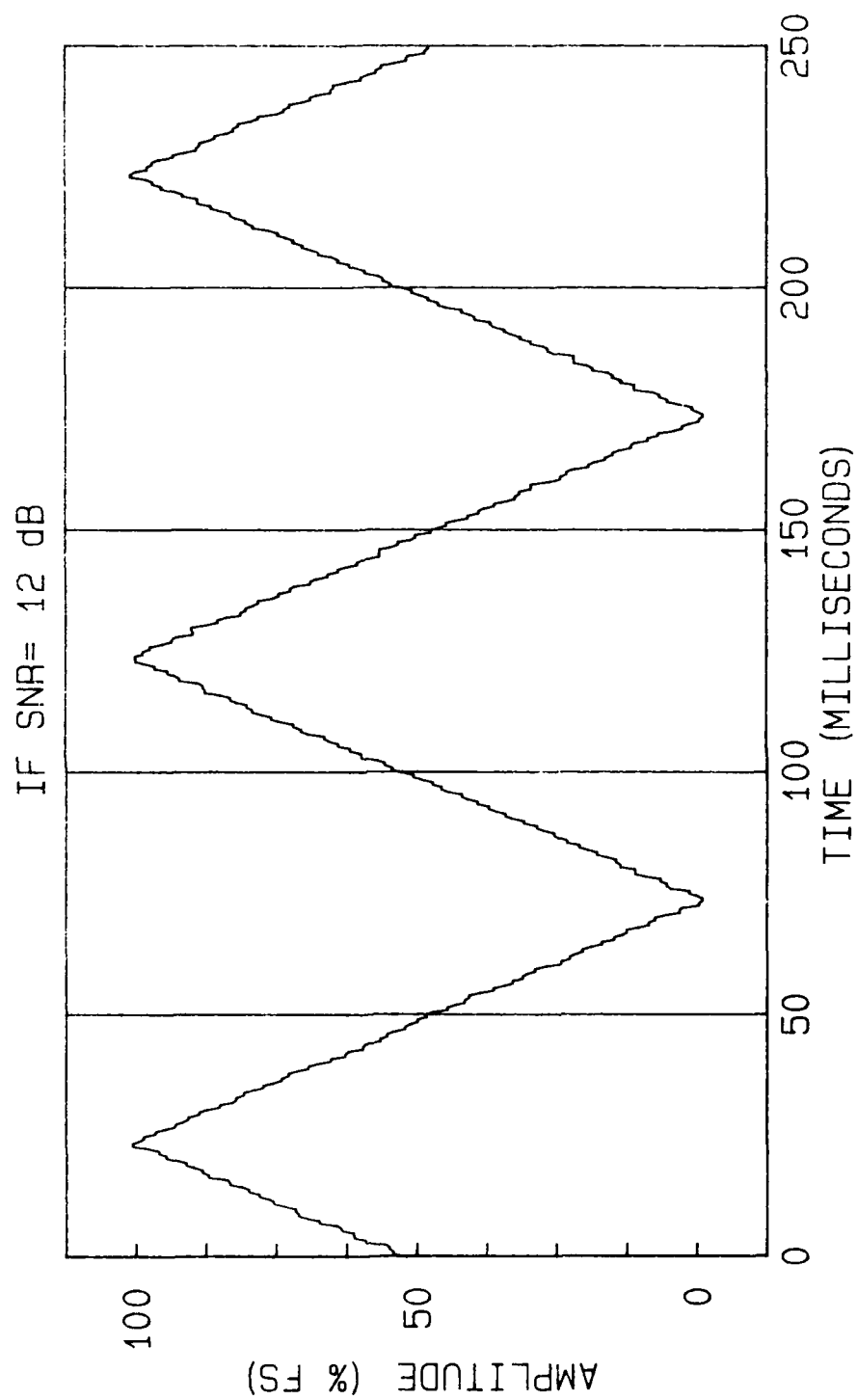


Figure 3.6-11. PAM DECOM Output for 12 dB IF SNR with Triangle Modulation.

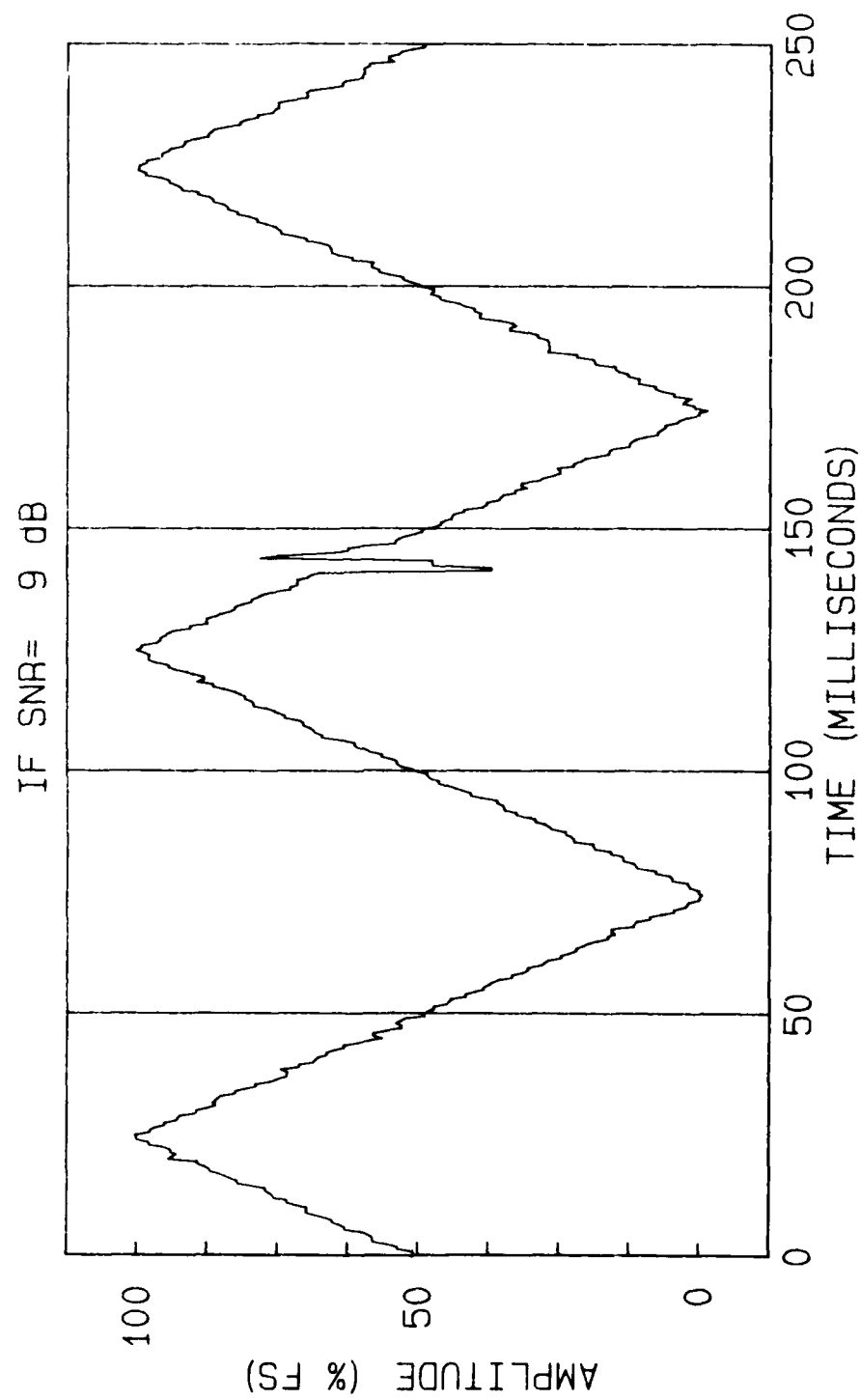


Figure 3.6-12. PAM DECOM Output for 9 dB IF SNR with Triangle Modulation.

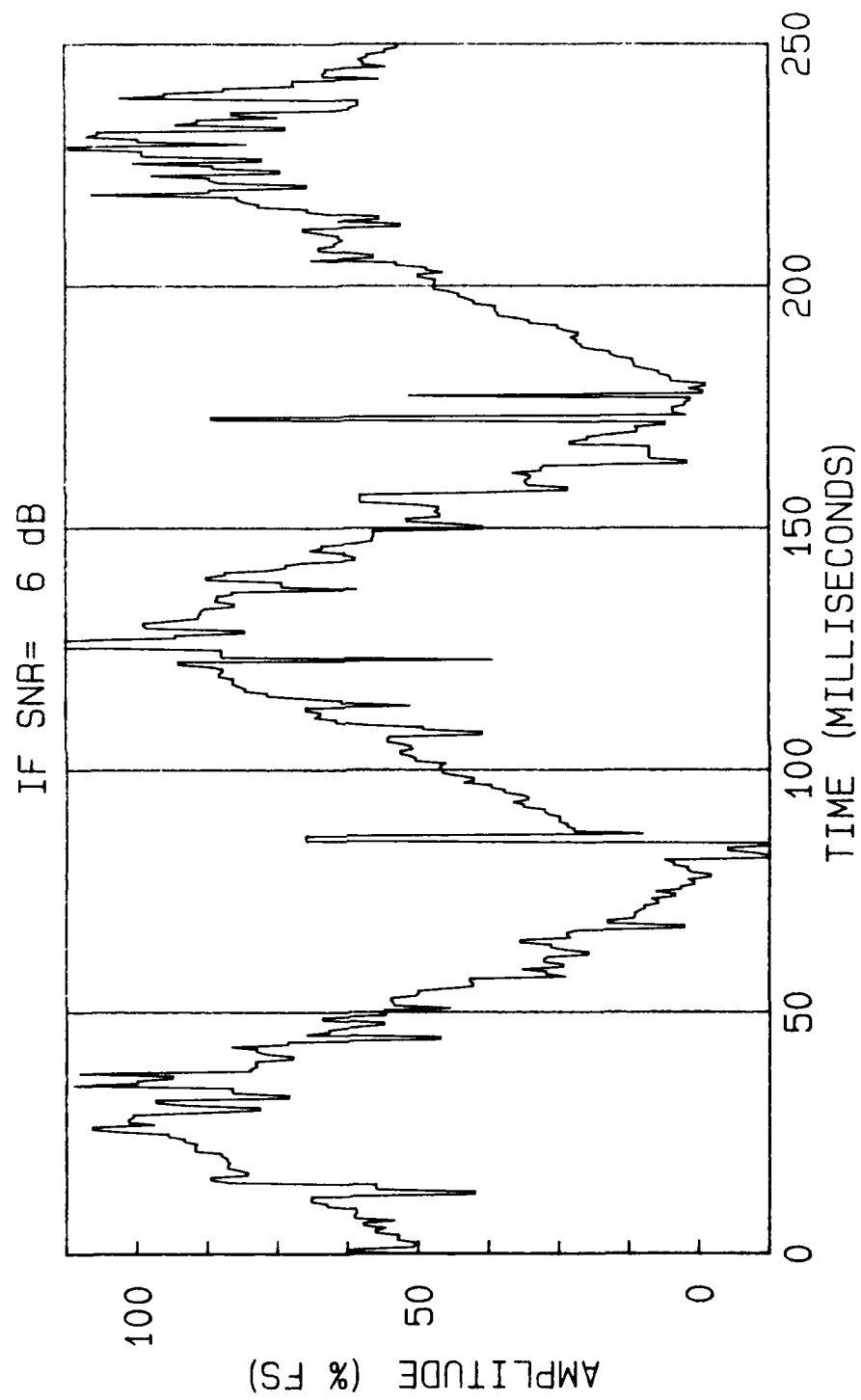


Figure 3.6-13. PAM DECOM Output for 6 dB IF SNR with Triangle Modulation.

### 3.6.6 NRZ PAM/FM Receiver IF Filter

The best receiver IF filter bandwidth (-3 dB) will usually be between 1.2 and 1.5 times the RF peak-to-peak deviation as long as the ratio of peak RF deviation to PAM channel rate is greater than 2. If the PAM signal is recorded in a predetection format, the best receiver filter bandwidth will probably be closer to twice the peak-to-peak RF deviation. This will allow the use of a filter on the recorder output of approximately the same bandwidth as the receiver filter. If the received signal is strong enough that the demodulator is always above FM threshold, the data quality will be slightly better with wide IF filters because they will tend to have better phase characteristics in the region the signal occupies. Therefore, the step response will be better and the crosstalk less. The disadvantage of wide IF filters is that they pass more noise and therefore FM threshold occurs sooner. The PAM data quality degrades rapidly below FM threshold so it is very desirable to remain above FM threshold. Narrow filters pass less noise and therefore the instantaneous signal amplitude is more likely to be greater than the instantaneous noise amplitude. However, narrow filters are more sensitive to receiver tuning errors and RF frequency drift. A filter with a -3 dB bandwidth equal to the peak-to-peak RF deviation would also attenuate the signal amplitude by 3 dB when the PAM signal is at either 0% or 100% of full scale. Therefore, the 0% and 100% signals would reach FM threshold 3 dB before the mid-scale signals. Since the 0% and 100% signals are used for calibration of the PAM decommutator, this could also degrade the accuracy of the mid-scale signals.

### 3.6.7 NRZ PAM/FM Receiver Video Filter

The receiver video filter should be a linear phase filter with bandwidth at least twice the PAM channel rate. This allows the decommutator to perform the filtering of the signal. The receiver video output must be DC coupled because the PAM signal usually contains a large DC component which varies in amplitude.

### 3.6.8 PAM Baseband Spectra

The baseband NRZ PAM power spectrum has an overall shape of:

$$[\sin^2 (\pi f / f_p)] / (\pi f / f_p)^2$$

where  $f_p$  is the PAM channel rate.

The exact spectrum depends on the amplitudes of the individual PAM channels. PAM signals are usually filtered by a 4- to 6-pole linear phase low-pass filter with a -3 dB point of approximately twice the PAM channel rate before they modulate a VCO or transmitter. A sample NRZ PAM baseband spectrum with a 4-pole filter is illustrated in figure 3.6-14. A linear phase filter is used to minimize the overshoot, crosstalk between adjacent channels, and the settling time.

25 KCH/S NRZ PAM  
PREMOD FILTER=50 KHZ 4-POLE BESSEL  
RESOLUTION BW=1 KHZ VIDEO BW=100 HZ

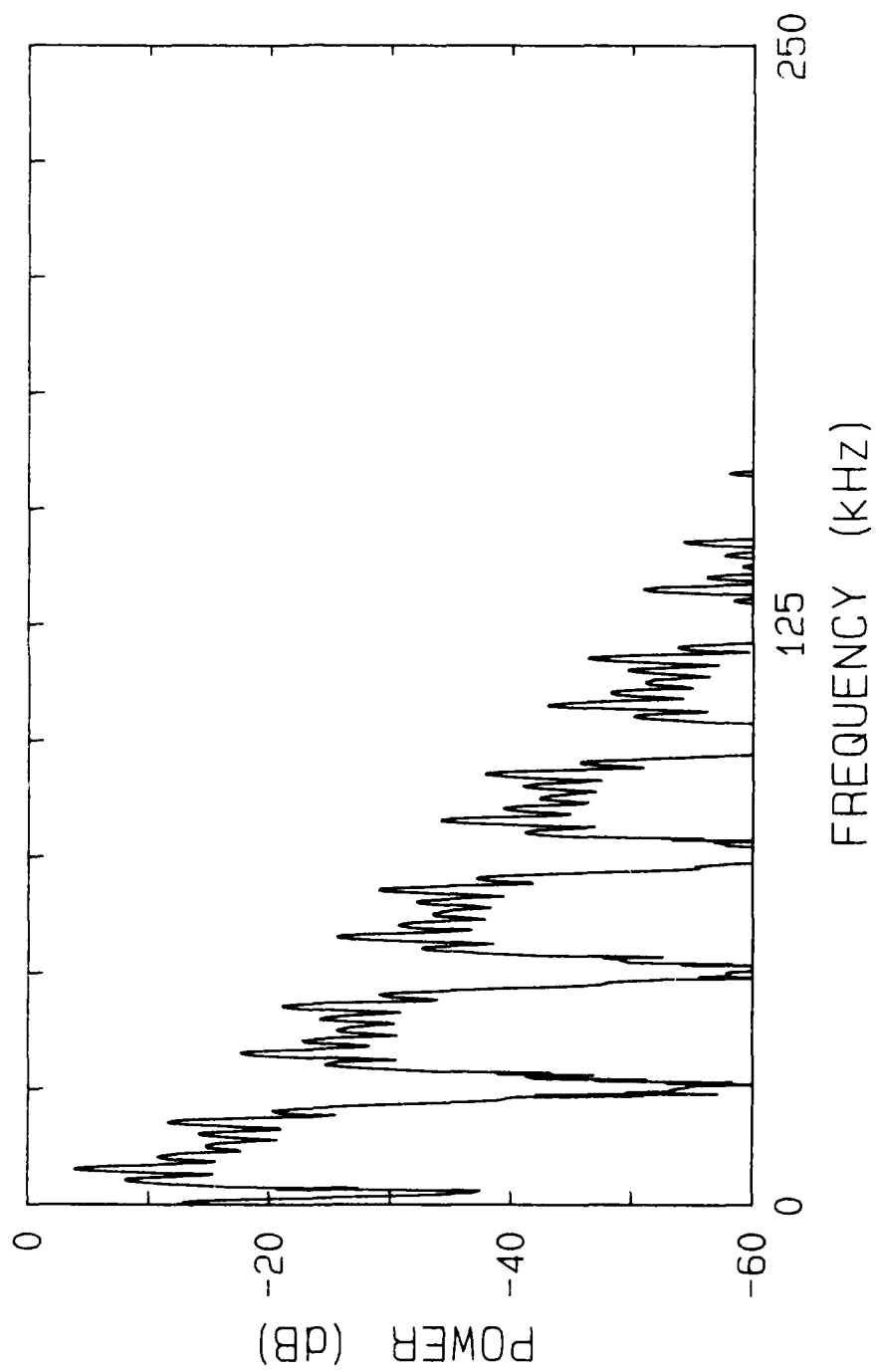


Figure 3.6-14. NRZ PAM Baseband Spectrum.



### 3.6.9 NRZ PAM/FM RF Spectra

The RF spectrum of an NRZ PAM/FM signal depends on the amplitude distribution of the PAM channels, the peak deviation, and the premodulation filter bandwidth. Typical NRZ PAM/FM spectra are illustrated in figures 3.6-15, 3.6-16, and 3.6-17 for 25 kCh/s PAM with a 50 kHz 5-pole linear phase premodulation filter and peak deviations of 50, 125, and 250 kHz. Figure 3.6-18 presents the spectra of the signal in figure 3.6-16 with the premodulation filter removed. Comparing these two figures we discover that the bandwidth that contains most of the energy is approximately 275 kHz in both figures but the -60 dBc bandwidth is much greater without a premodulation filter. Figure 3.6-19 shows the RF spectrum of a 50 kCh/s NRZ PAM/FM signal with a peak deviation of 125 kHz and a premodulation filter bandwidth of 100 kHz.

The bandwidth which contains most of the signal energy is approximately:

$$2(\text{peak deviation} + \text{PAM rate}/2).$$

The bandwidth beyond which all signals are 60 dB below the unmodulated carrier with a 4- to 6-pole linear phase premodulation filter with -3 dB bandwidth equal to twice the PAM rate is approximately:

$$2.5(\text{peak deviation} + 3 \text{ PAM rate}).$$

25 KCH/S NRZ PAM/FM  
PEAK DEVIATION=50 KHZ  
PREMOD FILTER=50 KHZ 5-POLE BESSEL  
RESOLUTION BW=3 KHZ VIDEO BW=100 HZ

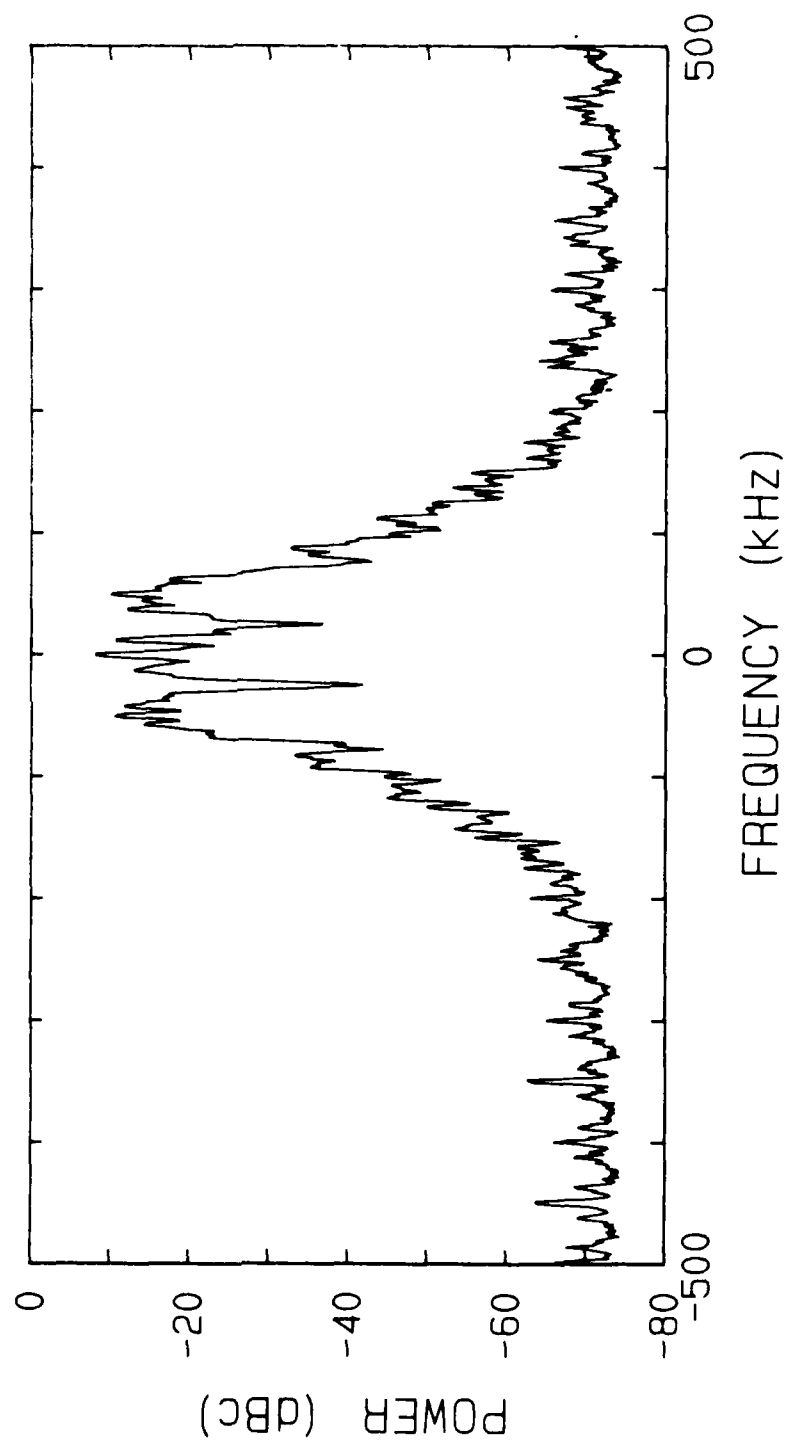


Figure 3.6-15. PAM/FM RF Spectrum with Peak Deviation=50 KHz.

25 KCH/S NRZ PAM/FM  
PEAK DEVIATION=125 KHZ  
PREMOD FILTER=50 KHZ 5-POLE BESSEL  
RESOLUTION BW=3 KHZ VIDEO BW=100 HZ

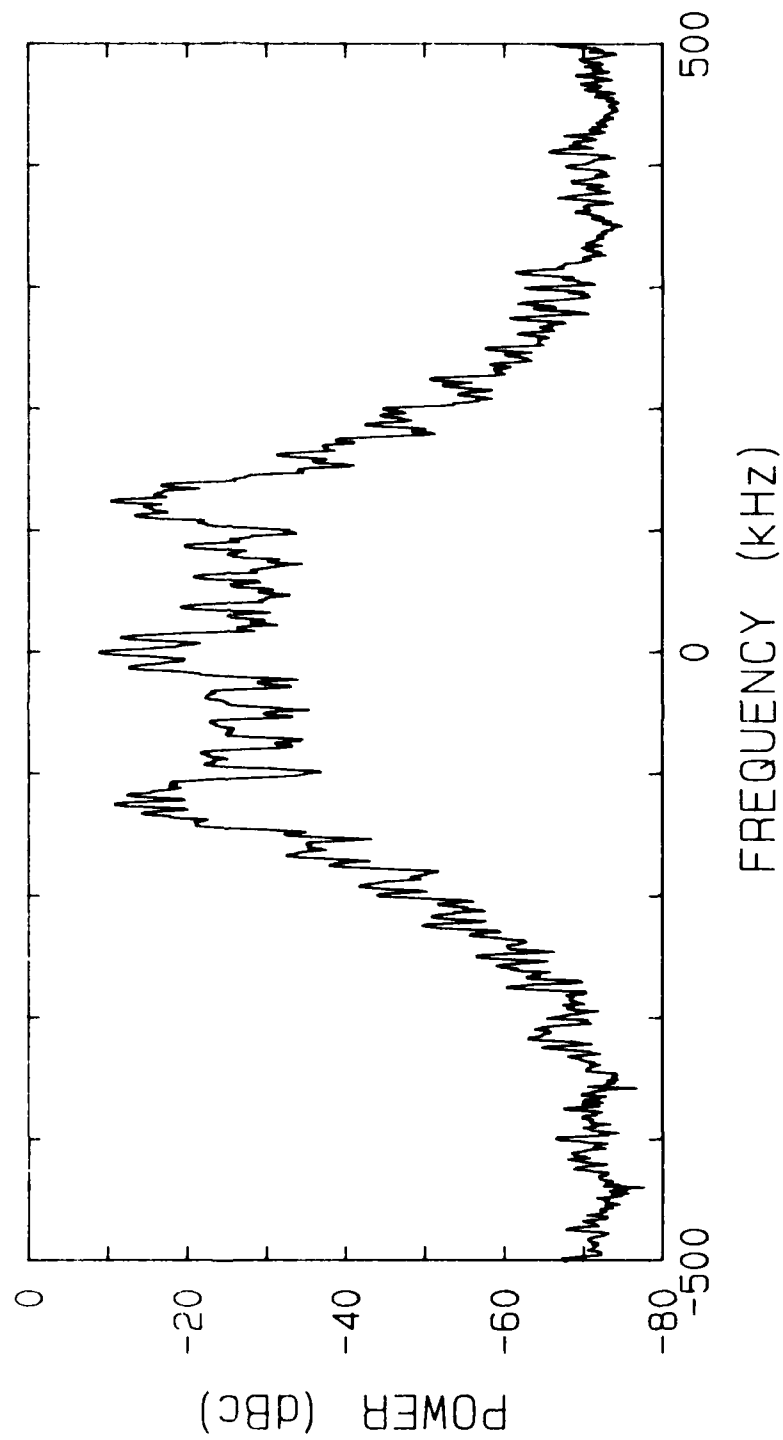


Figure 3.6-16. PAM/FM RF Spectrum with Peak Deviation=125 kHz.

25 KCH/S NRZ PAM/FM  
PEAK DEVIATION=250 KHZ  
PREMOD FILTER=50 KHZ 5-POLE BESSEL  
RESOLUTION BW=3 KHZ VIDEO BW=100 HZ

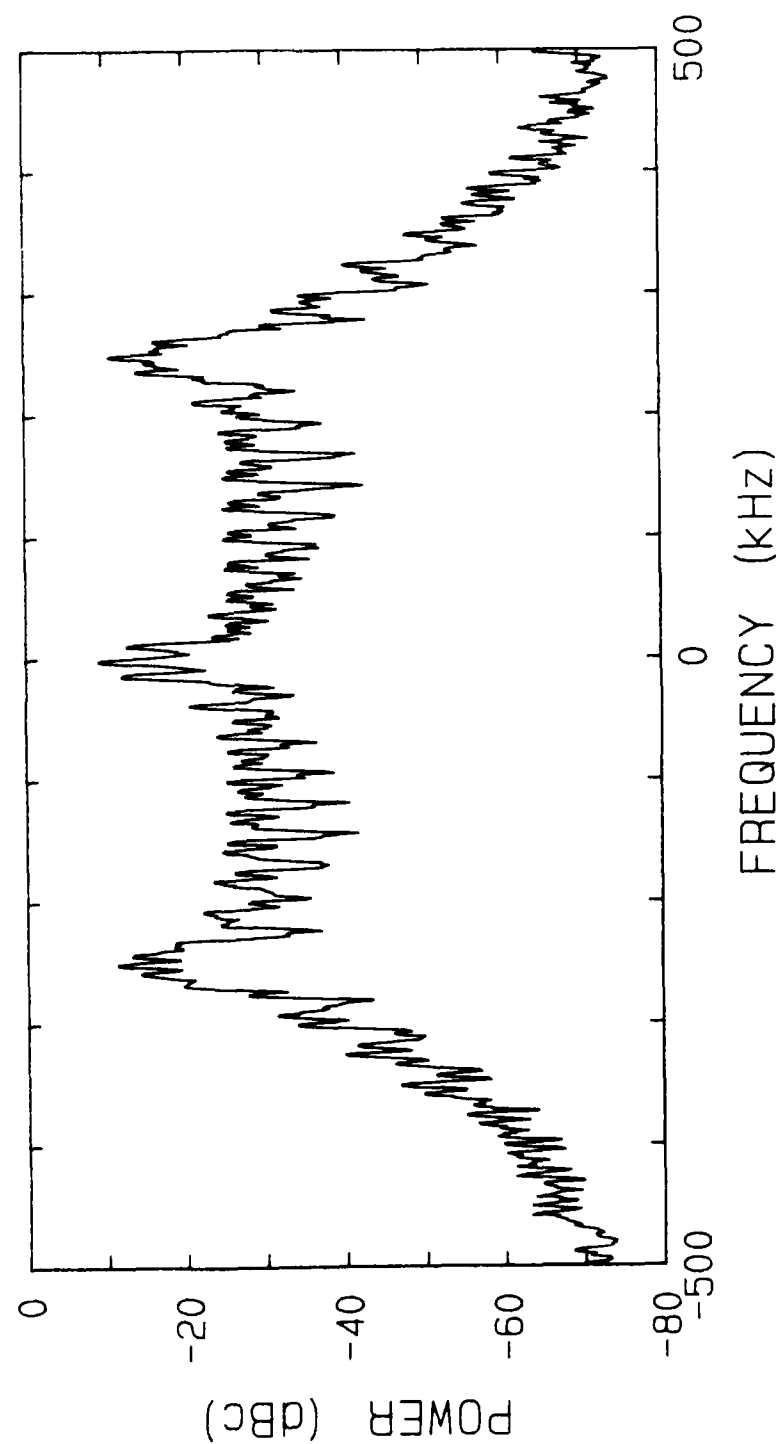


Figure 3.6-17. PAM/FM RF Spectrum with Peak Deviation=250 kHz.

25 KCH/S NRZ PAM/FM  
PEAK DEVIATION=125 KHZ  
PREMOD FILTER=NONE  
RESOLUTION BW=3 KHZ VIDEO BW=100 HZ

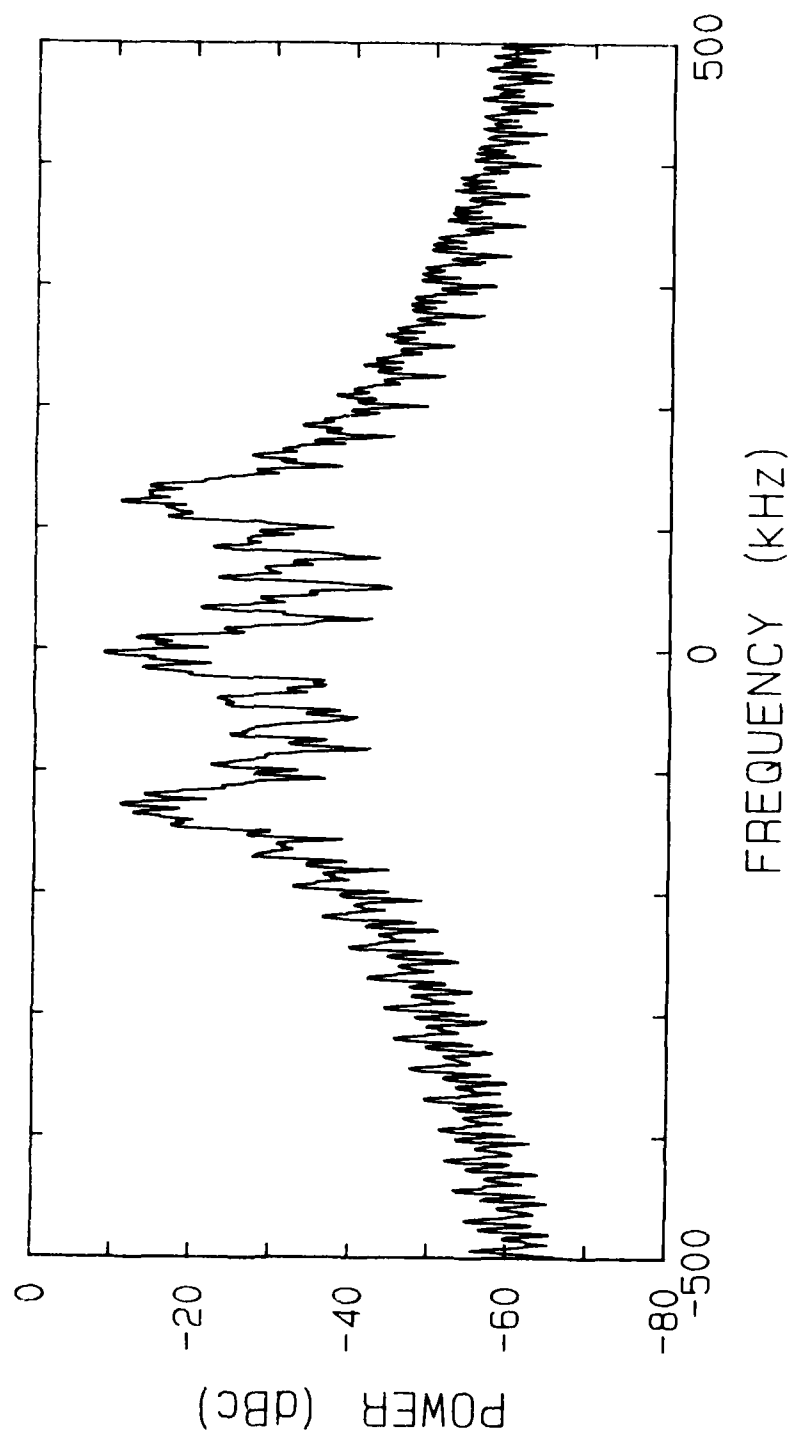


Figure 3.6-18. PAM/FM RF Spectrum with No Premodulation Filter.

50 KCH/S NRZ PAM/FM  
PEAK DEVIATION=125 KHZ  
PREMOD FILTER=100 KHZ 4-POLE BESSEL  
RESOLUTION BW=3 KHZ VIDEO BW=100 HZ

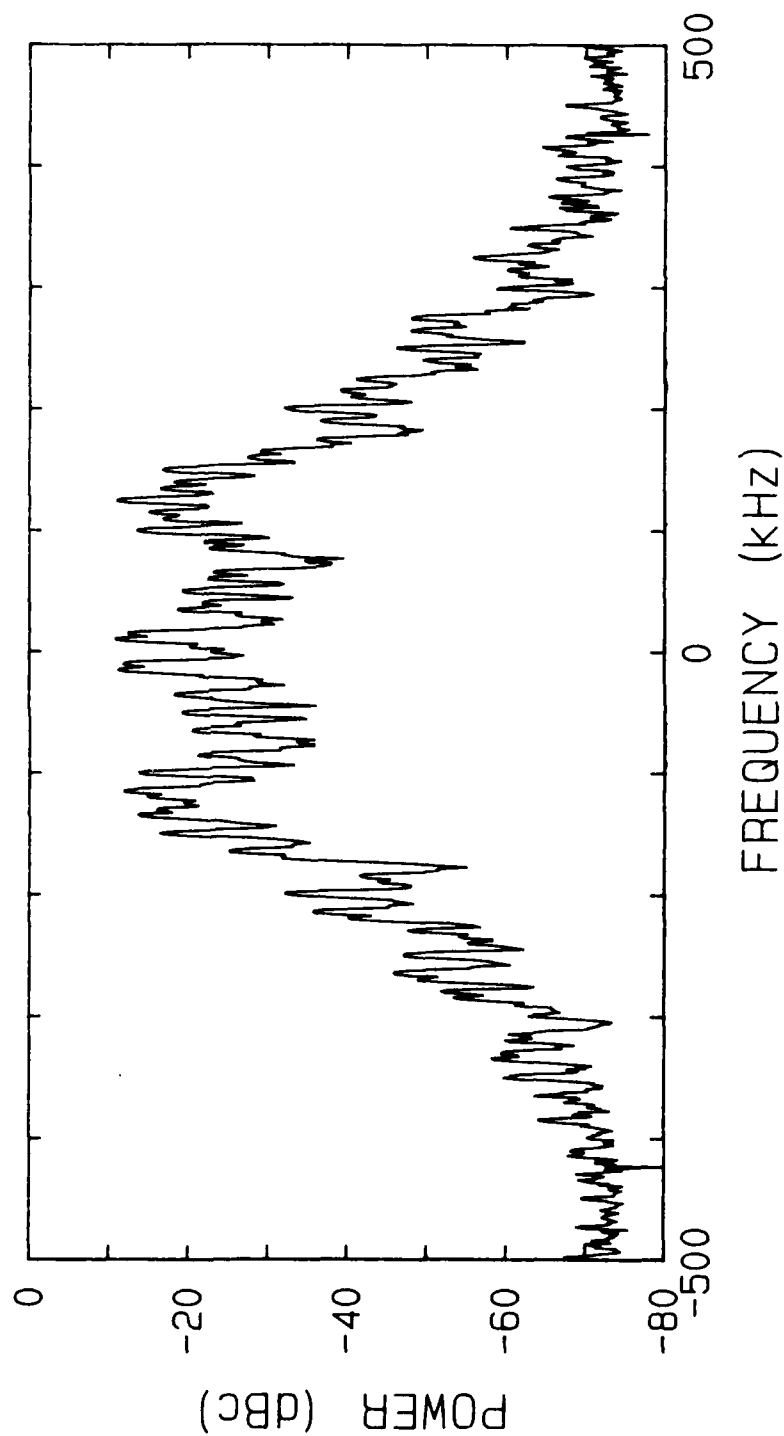


Figure 3.6-19. 50 KCH/s PAM/FM RF Spectrum.

### 3.7 FM/FM TELEMETRY

#### 3.7.1 Introduction

A typical FM/FM system block diagram is presented in figure 3.7-1. The transmitting system consists of several SCOs which are at different, compatible frequencies. A list of Inter-Range Instrumentation Group (IRIG) standard SCO frequencies is contained in the current issue of the Telemetry Standards IRIG 106-XX. The 1986 Telemetry Standards (IRIG 106-86) includes constant bandwidth (CBW) SCOs with center frequencies between 16 kHz and 1024 kHz and peak deviations from 2 kHz to 128 kHz and proportional bandwidth (PBW) SCOs with center frequencies between 400 Hz and 560 kHz with peak deviations of 7.5%, 15%, and 30% (the frequencies below 22 kHz are only used with 7.5% peak deviation). The SCO operates as a linear voltage-to-frequency converter. Therefore, the output frequency minus the SCO center frequency will be proportional to the input voltage. The center frequencies and deviation limits of the SCOs should be chosen to be compatible with the bandwidths of the input data signals, the available radio frequency (RF) spectral bandwidth, and the receiving equipment. The nominal IRIG deviation ratio is five. Deviation ratio is defined as the ratio of the maximum allowable subcarrier peak deviation to the discriminator low-pass cutoff frequency.

#### 3.7.2 FM/FM SNR

The SNR at the output of an FM demodulator will be discussed in this section. The signal and noise power at the output of an FM demodulator well above FM threshold can be described by the equations:

$$S_i = \frac{(K_d)^2 (\Delta f_{si})^2}{2}$$
$$N(f) = \frac{2 (K_d)^2 G(f) f^2}{A^2}$$

where:

- $S_i$  = Signal at FM demodulator output
- $N(f)$  = Noise spectrum at FM demodulator output
- $A^2/2$  = Signal power at FM demodulator input
- $G(f)$  = Noise power spectral density at FM demodulator input
- $K_d$  = Discriminator gain constant
- $\Delta f_{si}$  = Peak deviation of  $i^{\text{th}}$  subcarrier.

Note that the noise power spectral density is proportional to the square of the frequency.

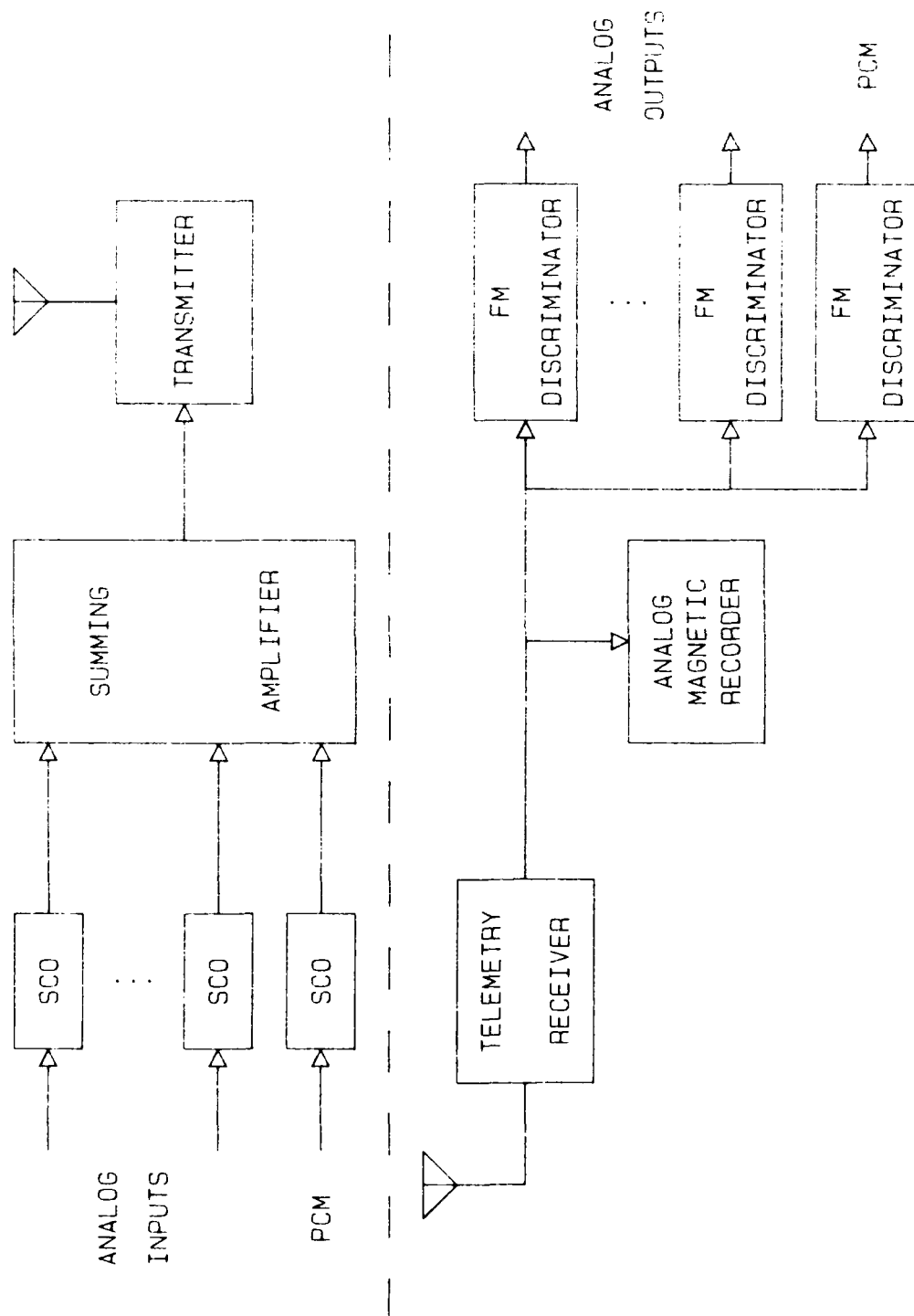


Figure 3.7-1. FM/FM System Block Diagram.



The following equations have been presented by several authors <sup>14,15,16,17</sup>.

The SNR (power ratio) at the output of an ideal low-pass filter can be shown to be:

$$(S/N)_{LPF} = \frac{3 (\Delta f_i)^2 B_{IF} (S/N)_{IF}}{2 (f_c)^3}$$

where:

$(S/N)_{IF}$  is the IF SNR

$B_{IF}$  is the IF bandwidth

$f_c$  is the low-pass filter bandwidth.

$\Delta f_i$  is the peak RF deviation of the  $i^{th}$  subcarrier.

The SNR at the output of an ideal bandpass filter can be approximated by:

$$(S/N)_{BPF} = \frac{(\Delta f_i)^2 B_{IF} (S/N)_{IF}}{2 (f_i)^2 B_i}$$

where:

$f_i$  is the center frequency of the subcarrier

$B_i$  is the bandwidth of the subcarrier discriminator bandpass filter.

These two equations can be used to calculate the approximate SNR of any FM signal.

The SNR (power ratio) at the output of a subcarrier discriminator can be calculated by substituting the SNR at the output of the bandpass filter for the  $SNR_{IF}$  and the subcarrier IF bandwidth for the receiver IF bandwidth in the lowpass filter case:

$$SNR_{dj} = \frac{3 (\Delta f_i)^2 (\Delta f_{si})^2 B_{IF} SNR_{IF}}{4 (f_i)^2 (f_c)^3}$$

<sup>14</sup>Nichols, M. H. and Rauch, L.L. Radio Telemetry, J. Wiley, 1956.

<sup>15</sup>Uglow, K. "Noise and Bandwidth in FM Radio Telemetry", *IRE Transactions*, pp 19-22, May 1957.

<sup>16</sup>Rosen, C. "System Transmission Parameters Design for Threshold Performance", in *Proceedings of the International Telemetry Conference*, Vol. XIX, pp 145-182, 1983.

<sup>17</sup>Rechter, R.J. "Summary and Discussion of Signal-to-Noise Ratio Improvement Formulae for FM and FM/FM Links", in *Proceedings of the International Telemetry Conference*, Vol. III, pp 221-255, 1967.

This SNR is the ratio of the power in a full scale sine wave to the noise power. To convert this to rms noise relative to full scale signal one would multiply the previous equation by 8 and take the square root.

This gives the following equation:

$$\text{SNR}_v = \frac{2.45 (\Delta f_i) (\Delta f_{si}) (B_{IF} \text{SNR}_{IF})^{1/2}}{f_i (f_c)^{3/2}}$$

This equation will be used in this report. It allows direct comparisons with PAM and PCM data quality. This equation appears to imply that the output SNR is a function of  $B_{IF}$ . However,  $\text{SNR}_{IF}$  is inversely proportional to the IF bandwidth. Therefore, the  $B_{IF}$  term cancels out.

The major assumptions that were made in deriving these expressions were:

1. The receiver noise power spectral density (PSD) was constant and the IF filter gain was constant over the bandwidth  $B_{IF}$  and zero everywhere else.
2. The noise PSD was constant in the discriminator bandpass.
3. The discriminator bandpass filter gain was constant over the bandwidth  $B_i$  and zero everywhere else.
4. The low-pass output filter gain was constant over the band from zero to  $f_c$  and zero everywhere else.
5. No intermodulation products were introduced in the system.
6. No interchannel interference was present.
7. The SNR was high enough that the noise did not capture the demodulator and cause pops.
8. No other noise sources were present (60 cycle, tape flutter, etc.).

The accuracy of these assumptions will now be discussed.

1. This affects signal and noise approximately the same and therefore should have no significant effect on SNR.
2. This assumption is quite good for narrow band channels but not very good for  $\pm 30\%$  channels. The noise at the output of an FM demodulator increases at 6 dB/octave. Therefore, the noise power/Hz at  $0.7 f_i$  is approximately 5.4 dB less than at  $1.3 f_i$ . However, this does not significantly affect performance above FM threshold. If the subcarrier discriminator reached FM threshold before the receiver discriminator this could cause the majority of noise pops to be towards higher frequency because the average noise frequency would be greater than the discriminator center frequency.

3. This assumption has little effect at high deviation ratios (greater than 2) above FM threshold. At a deviation ratio of 1, a modulating signal with a frequency equal to the low pass filter cutoff will be attenuated by 6 dB (3 dB due to BPF, 3 dB due to LPF) while the noise may only be attenuated by 1 dB (3-or 4-pole filters). The discriminator bandpass filter will attenuate a lower bandedge or upper bandedge signal by approximately 3 dB. Therefore, a signal at bandedge will reach FM threshold sooner and have more noise below FM threshold than a signal at bandcenter. This is illustrated in figure 3.7-2.

4. This assumption is fairly good for 7-pole Butterworth filters with the -3 dB point at the listed cutoff. Some discriminators use 3-pole Butterworth filters with the -0.5 dB point at the listed cutoff. This causes approximately 6.5 dB more noise power at high deviation ratios (3 or greater). Bessel filters typically pass 3-4 dB more noise than the theoretical brickwall filter. The effects of low-pass filter type and number of poles are shown in figures 3.7-3 through 3.7-7. Reference 4 also includes plots of these errors.

3. and 4. The cumulative filter error varies from 6-7 dB optimistic for a signal at the low-pass cutoff frequency and any Bessel low-pass filter at a high deviation ratio to 1 dB pessimistic for a deviation ratio of 1 and a frequency at less than 1/2 of the low-pass cutoff frequency.

5. This assumption is fairly good for IF SNRs below 20 dB. At low IF SNRs the thermal noise tends to swamp the intermodulation distortion. The amount of intermodulation distortion depends on the linearity of the modulator and demodulator and the phase linearity of the receiver IF filter.

6. This assumption is valid for high deviation ratios (3 or greater) and IF SNRs below 20 dB. For a deviation ratio of 1 and a 40 dB IF SNR the interchannel interference can be at least 10 dB larger than the noise.

7. Receiver noise pops should be insignificant for SCO frequencies above 10 kHz with receiver IF SNRs greater than 12 dB. Noise pops are insignificant for all SCO frequencies for receiver IF SNRs greater than 18 dB. The actual onset of FM threshold varies somewhat for different receiver designs. Ignoring noise pops at a 12 dB IF SNR can lead to an optimistic estimate of SNR for low frequency channels. The data in figure 3.7-8 show the measured receiver output noise power at a frequency of 5 kHz for peak deviations of 50, 100, 150, and 200 kHz (500 kHz IF bandwidth) and IF SNRs from 8 to 15 dB. This data shows that the measured and calculated noise at a 12 dB IF SNR agreed well when the peak deviation was 50 kHz but the measured noise power increased by approximately 1.5 dB when the peak deviation was increased to 200 kHz. The excess noise due to pops at a 9 dB IF SNR was 4 dB for 50 kHz peak deviation, 8 dB for 100 kHz peak deviation, and 19 dB for 200 kHz peak deviation. The same measurements were also made at a frequency of 100 kHz. The excess noise due to pops with a 9 dB IF SNR and 200 kHz peak deviation was only 1 dB.

The data in figures 3.7-9 through 3.7-14 show both measured and calculated discriminator output SNRs for various test conditions and assumptions. The units of the vertical axes are dB with respect to full scale (dBFS). This is defined as 20 times the logarithm (base ten) of the ratio of the discriminator bandedge-to-bandedge voltage swing to the rms noise voltage, eg, 20 mV rms noise

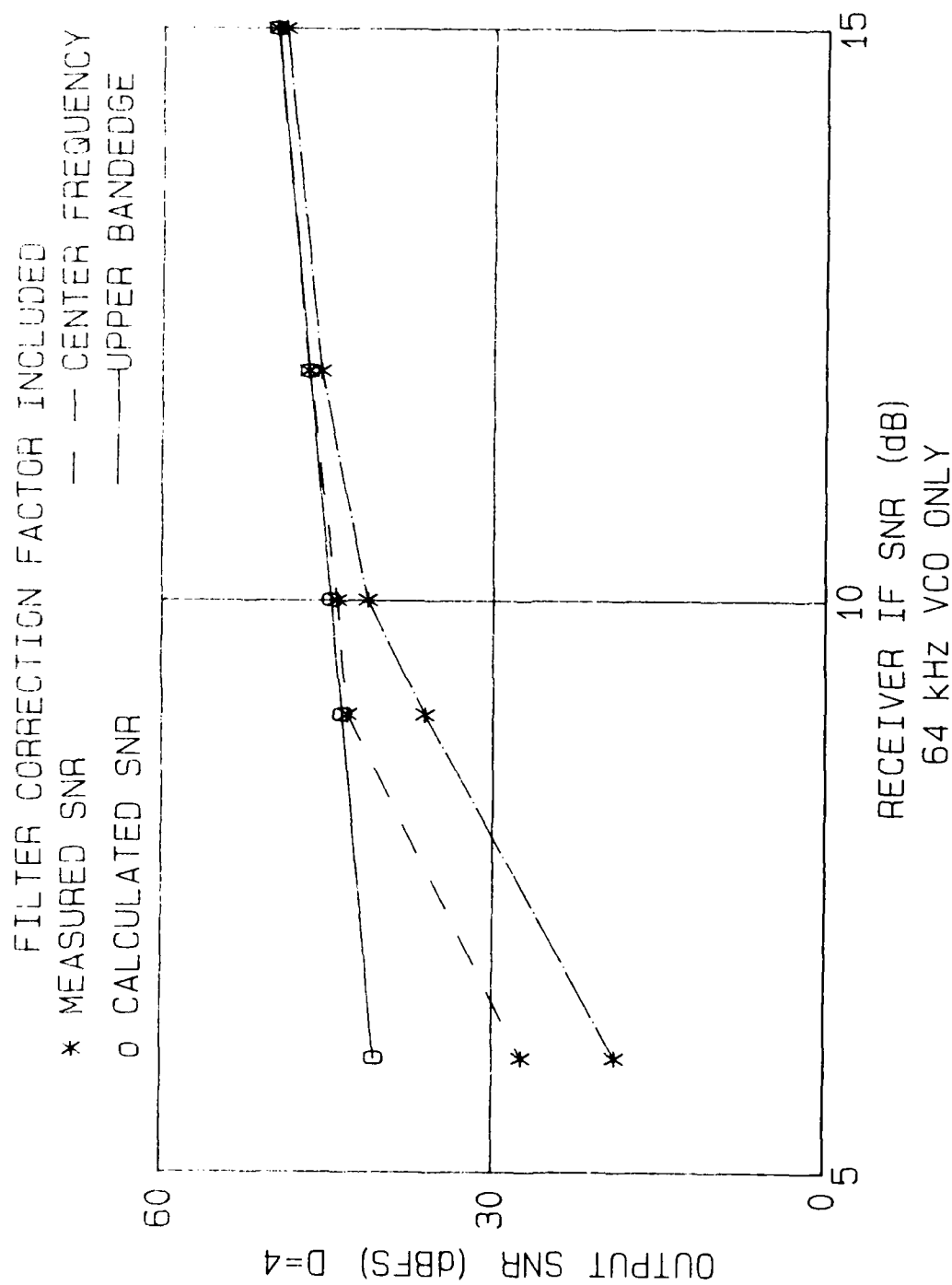


Figure 3.7-2. FM/FM SNR for Center Frequency and Upper Bandedge Signals.

FM NOISE X BESSEL LPF 3-POLE  
 NOISE POWER CORRECTION= 4.15 dB

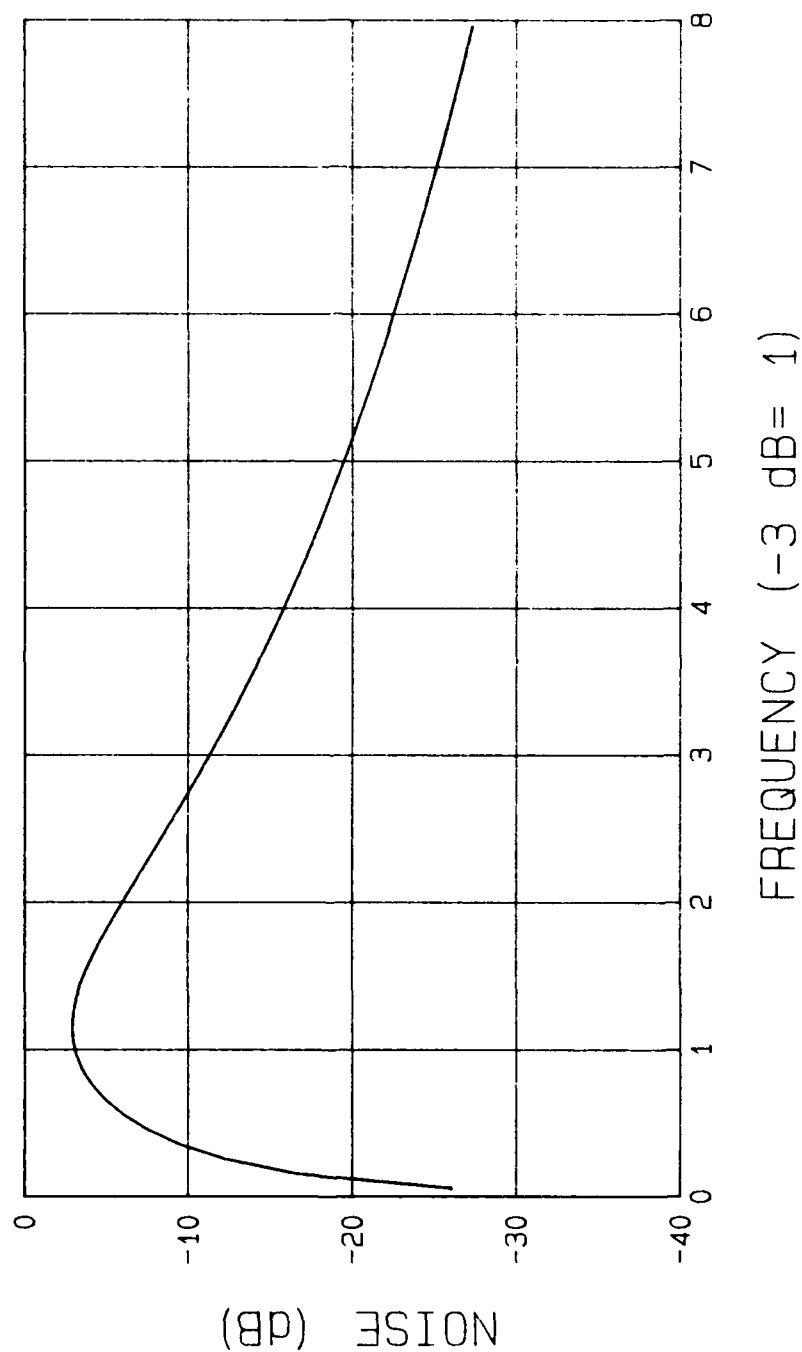


Figure 3.7-3. FM Noise with 3-pole Bessel LPF.

FM NOISE X BESSEL LPF 7-POLE  
 NOISE POWER CORRECTION= 3.05 dB

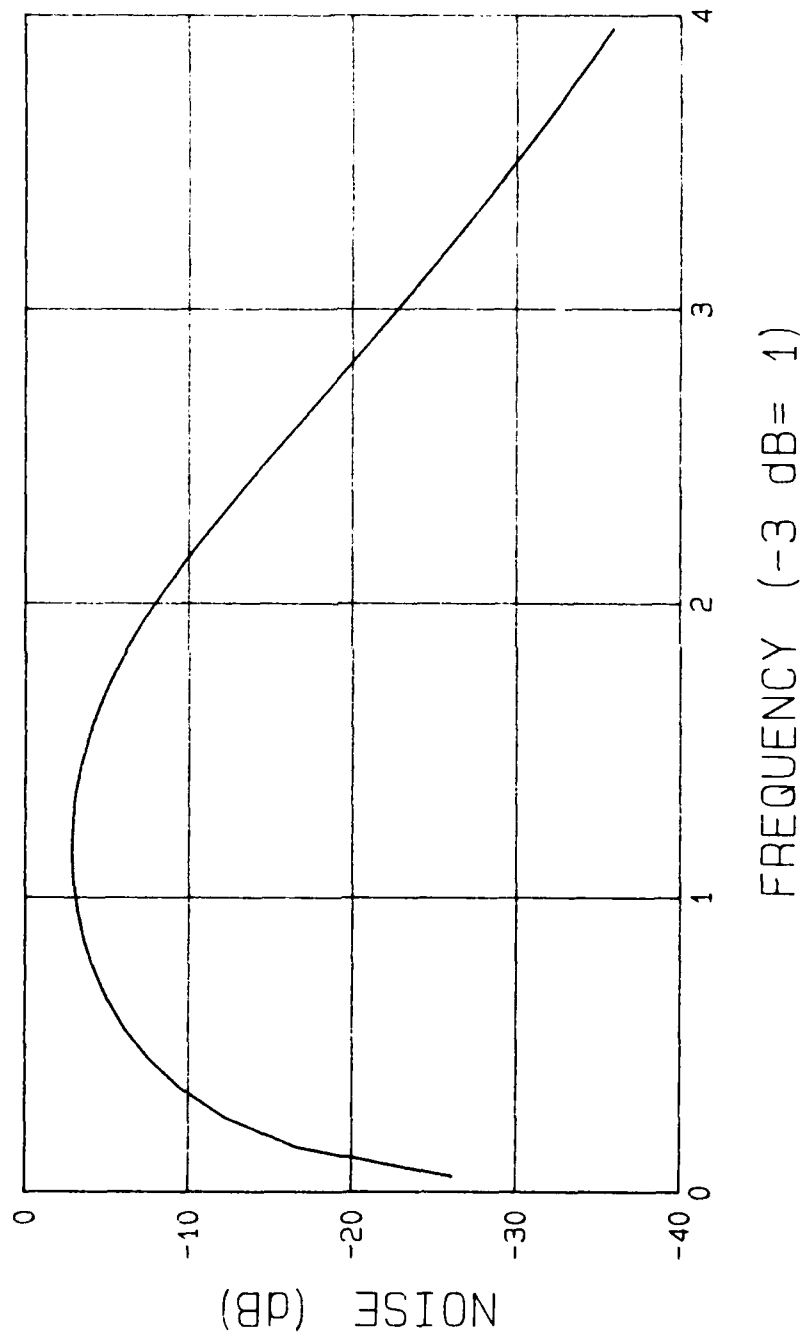


Figure 3.7-4. FM Noise with 7-pole Bessel LPF.

FM NOISE X BUTTERWORTH LPF 3-POLE  
 NOISE POWER CORRECTION= 6.52 dB

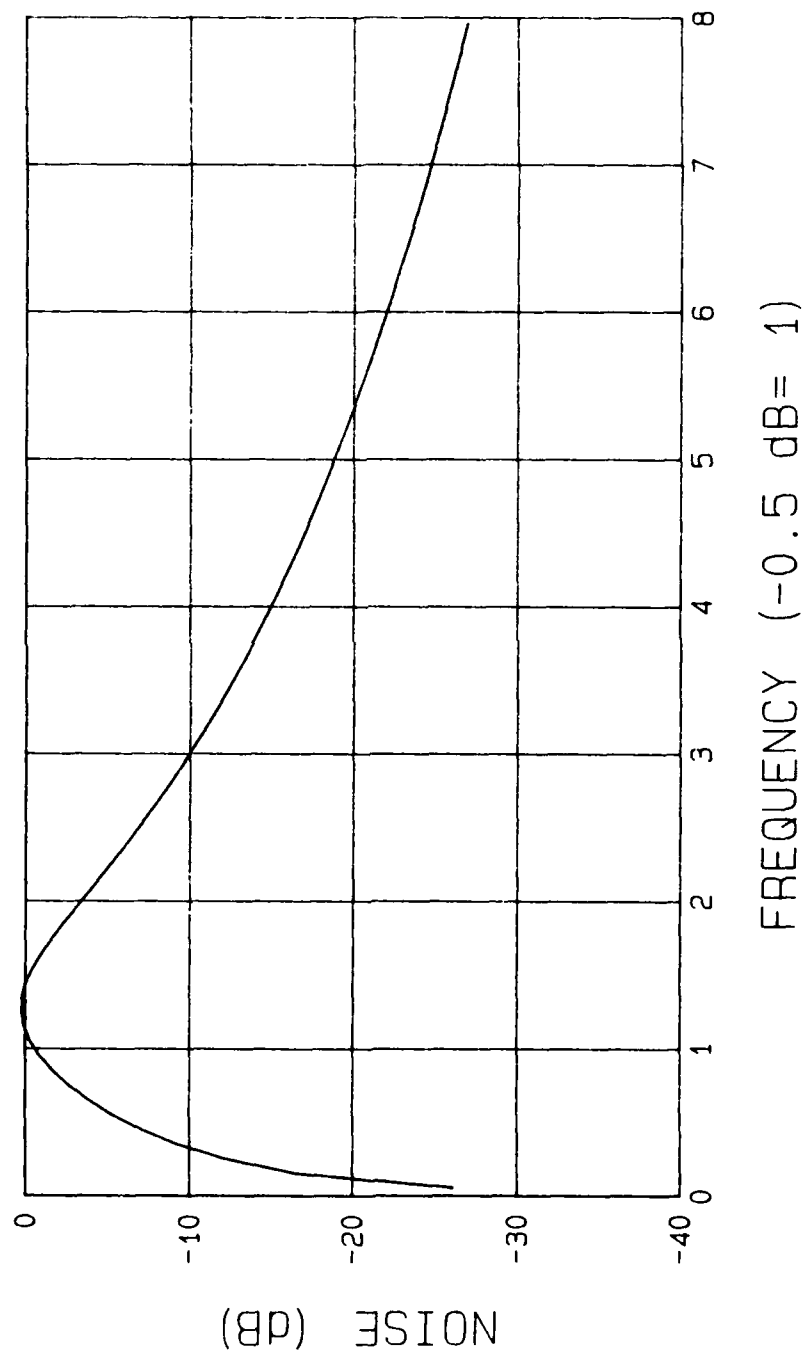


Figure 3.7-5. FM Noise with 3-pole Butterworth LPF (-0.5 dB).

FM NOISE X BUTTERWORTH LPF 7-POLE  
 NOISE POWER CORRECTION= 2.30 dB

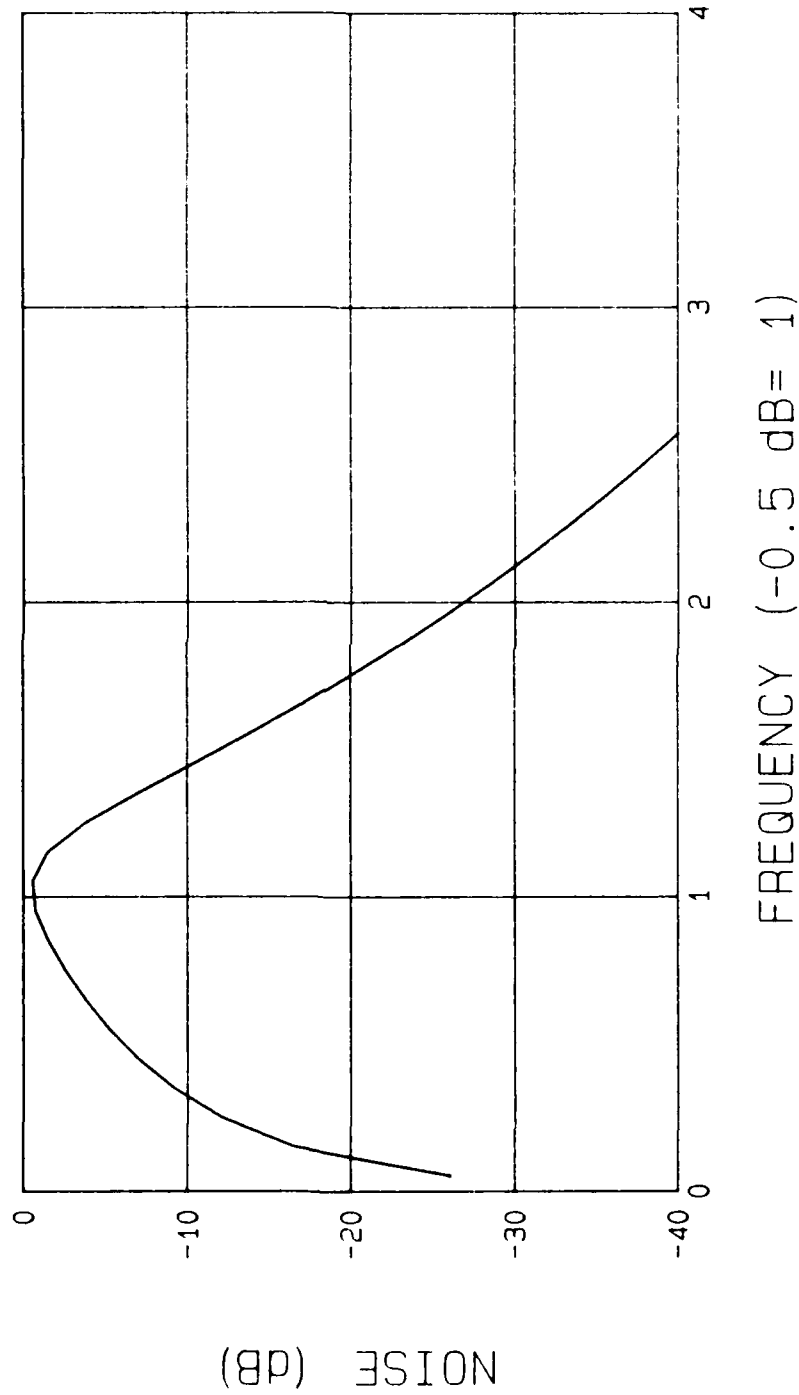


Figure 3.7-6. FM Noise with 7-pole Butterworth LPF.



FM NOISE X BUTTERWORTH LPF 7-POLE  
 NOISE POWER CORRECTION= .34 dB

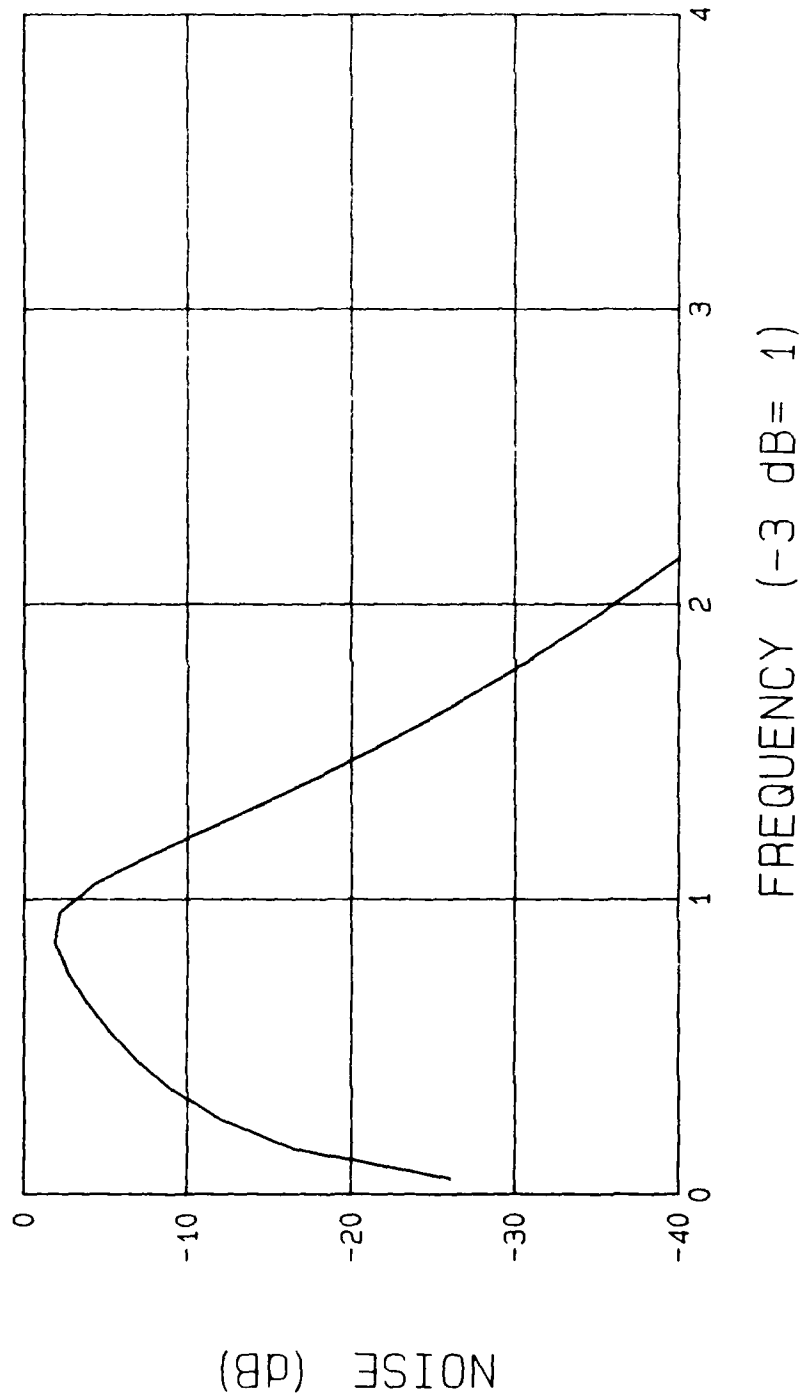


Figure 3.7-7. FM Noise with 7-pole Butterworth LPF (-3 dB).

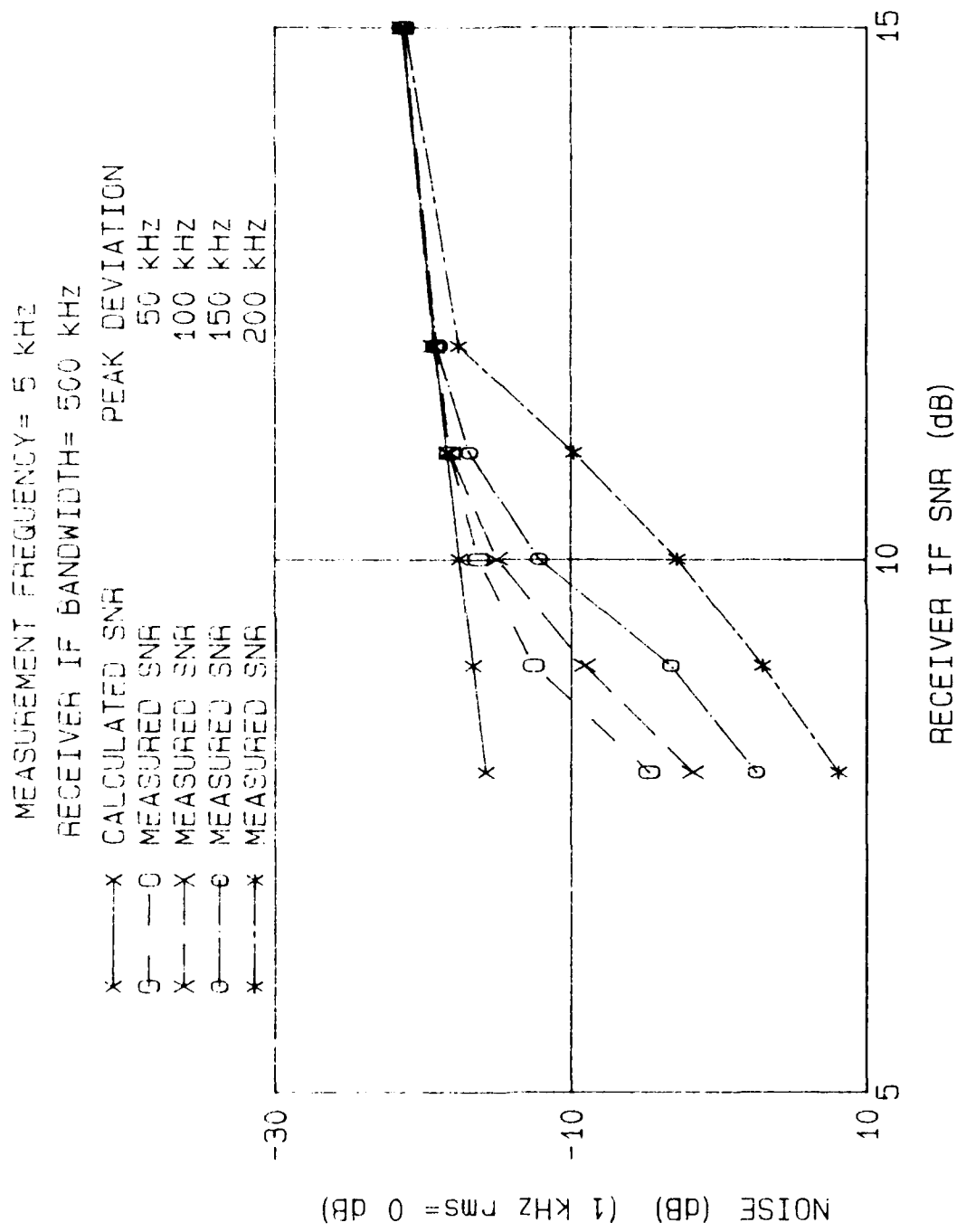


Figure 3.7-8. FM Noise for Several Peak Deviations.

PBW 1.7 TO 93 KHZ 9 dB/OCTAVE TAPER

BRICKWALL FILTERS ASSUMED

\* MEASURED SNR  
 O CALCULATED SNR  
 --- 93 KHZ  
 --- 5.4 KHZ

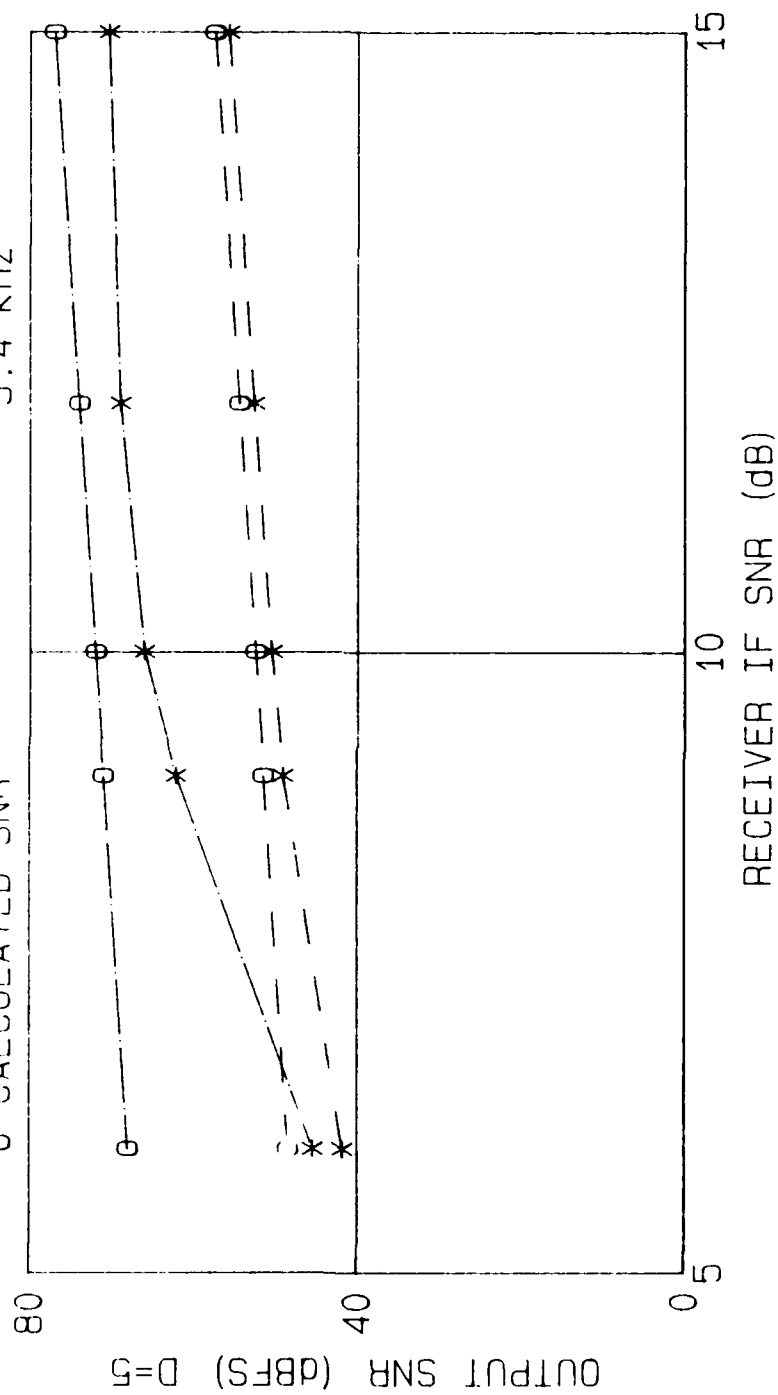


Figure 3.7-9. PBW Measured and Calculated SNRs with Brickwall Filters.

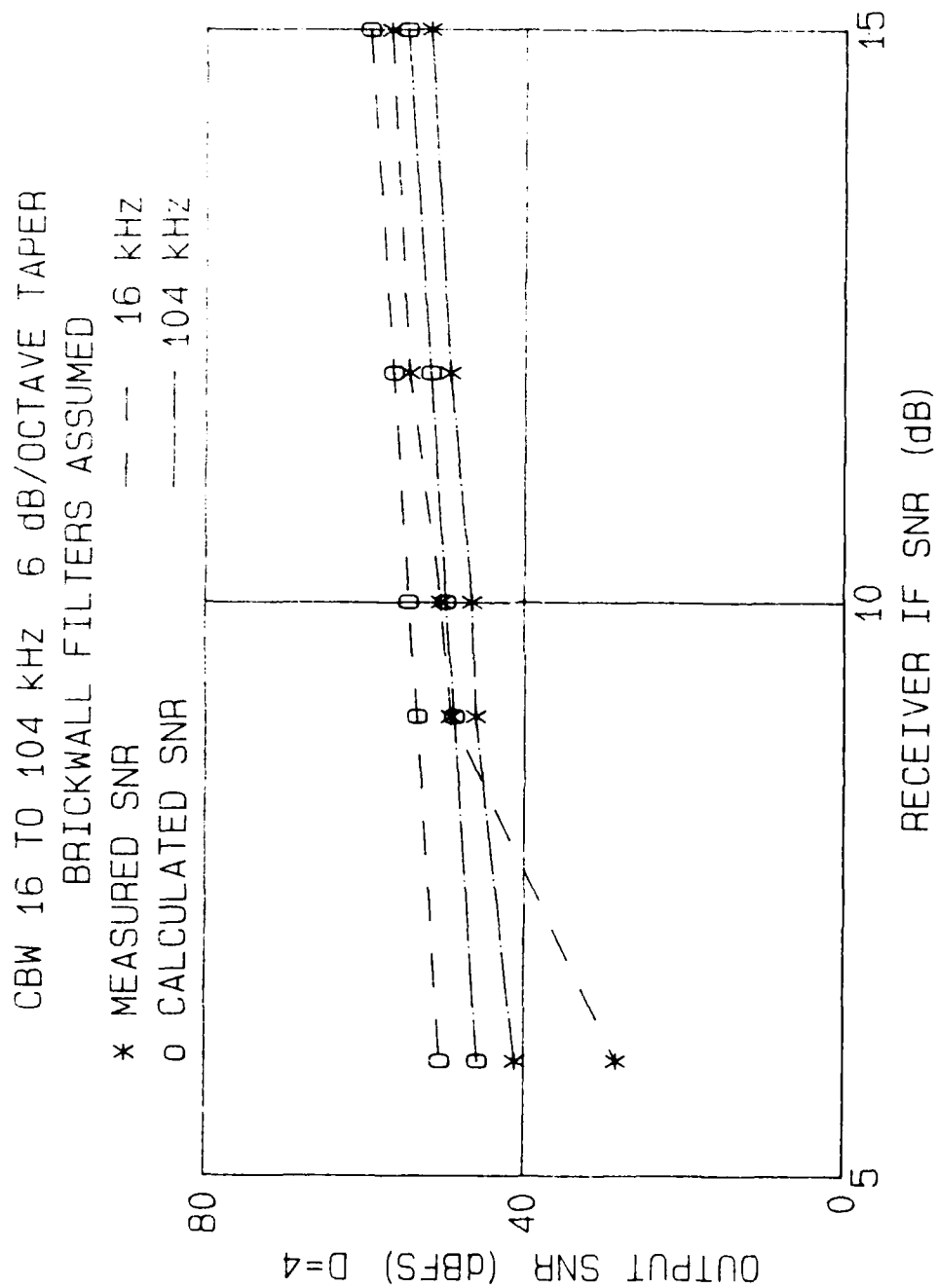


Figure 3.7-10. CBW Measured and Calculated SNRs with Brickwall Filters.

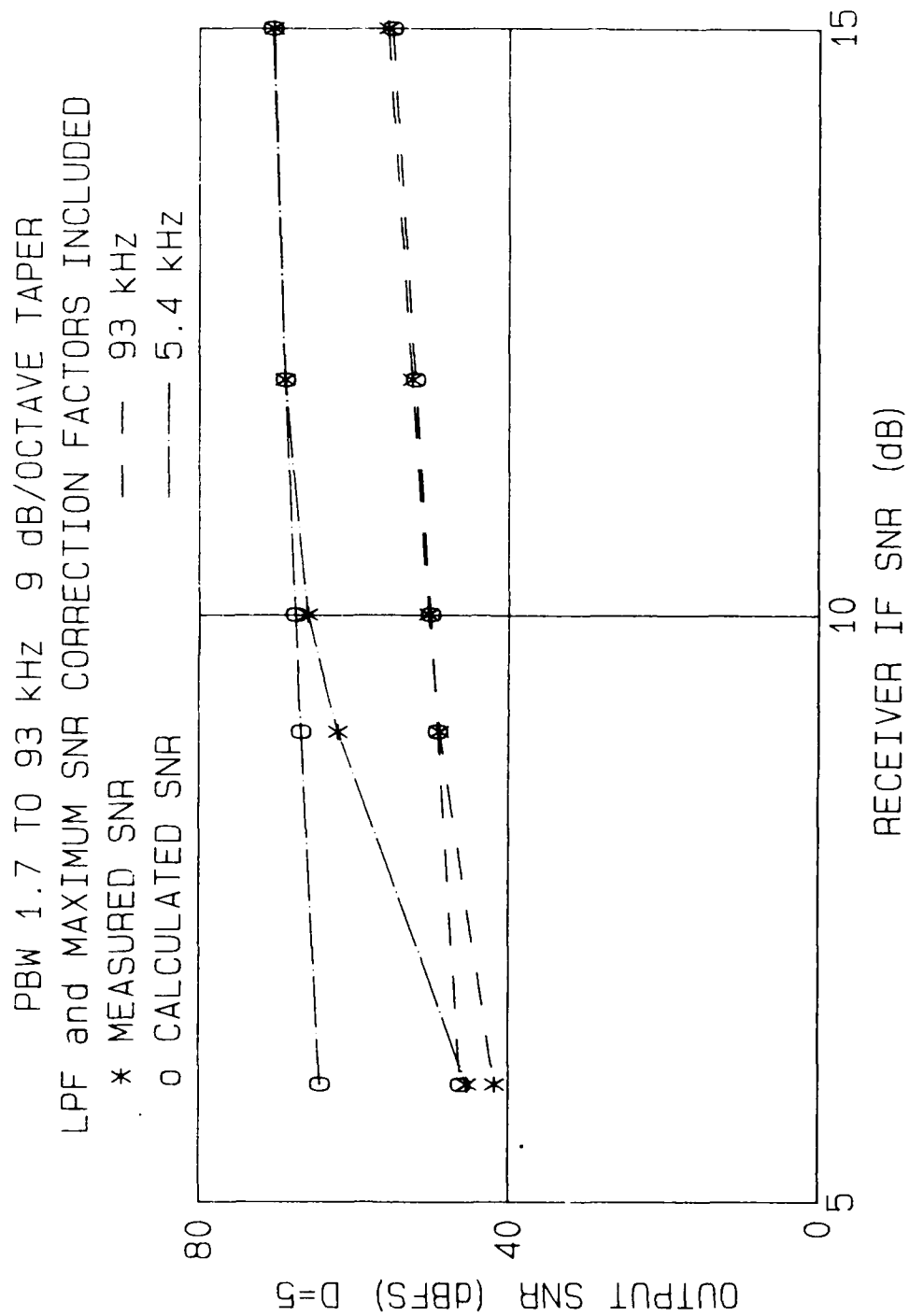


Figure 3.7-11. PBW Measured and Calculated SNRs with Correction Factors.

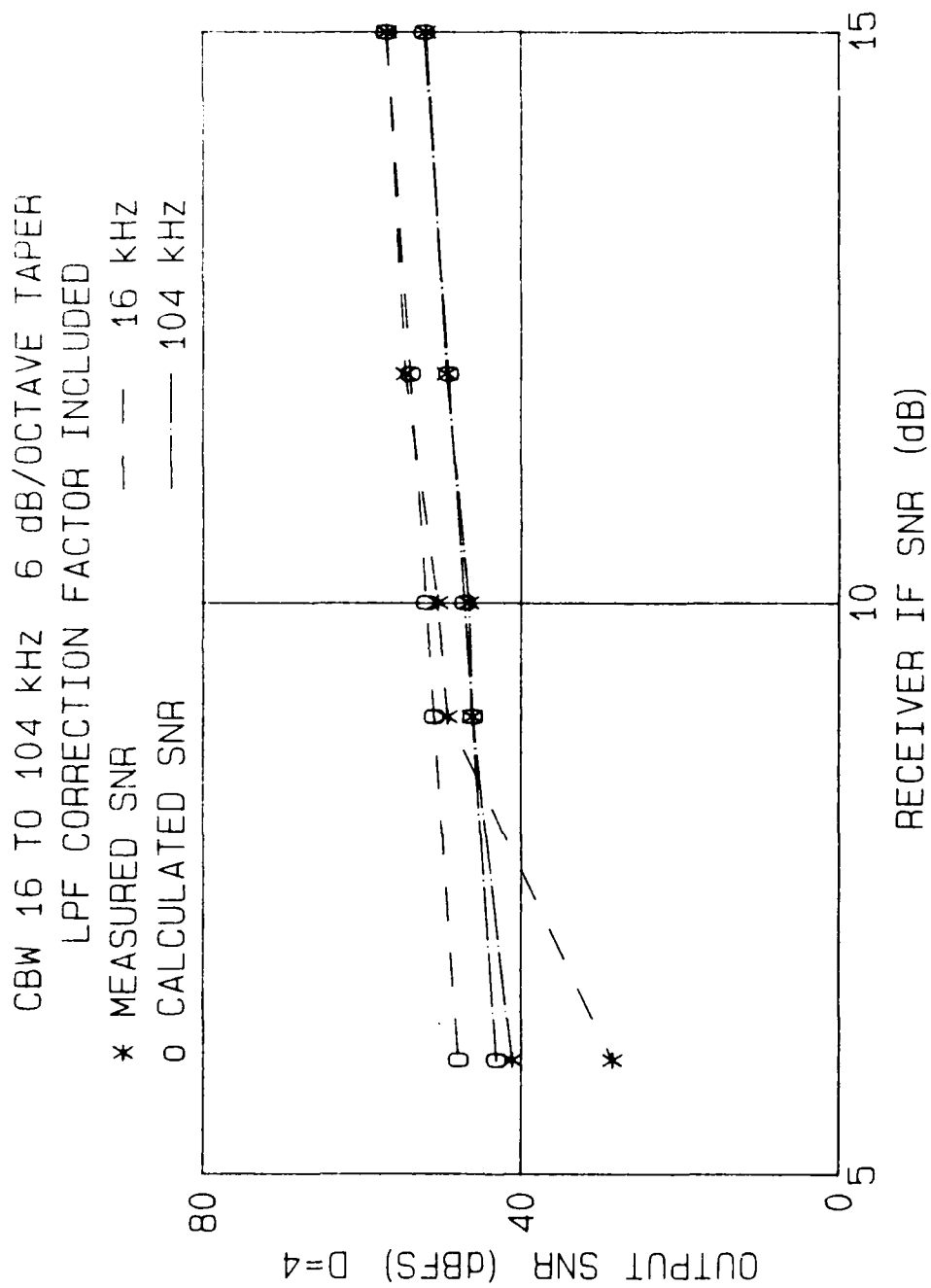


Figure 3.7-12. CBW Measured and Calculated SNRs with LPF Correction Factors.

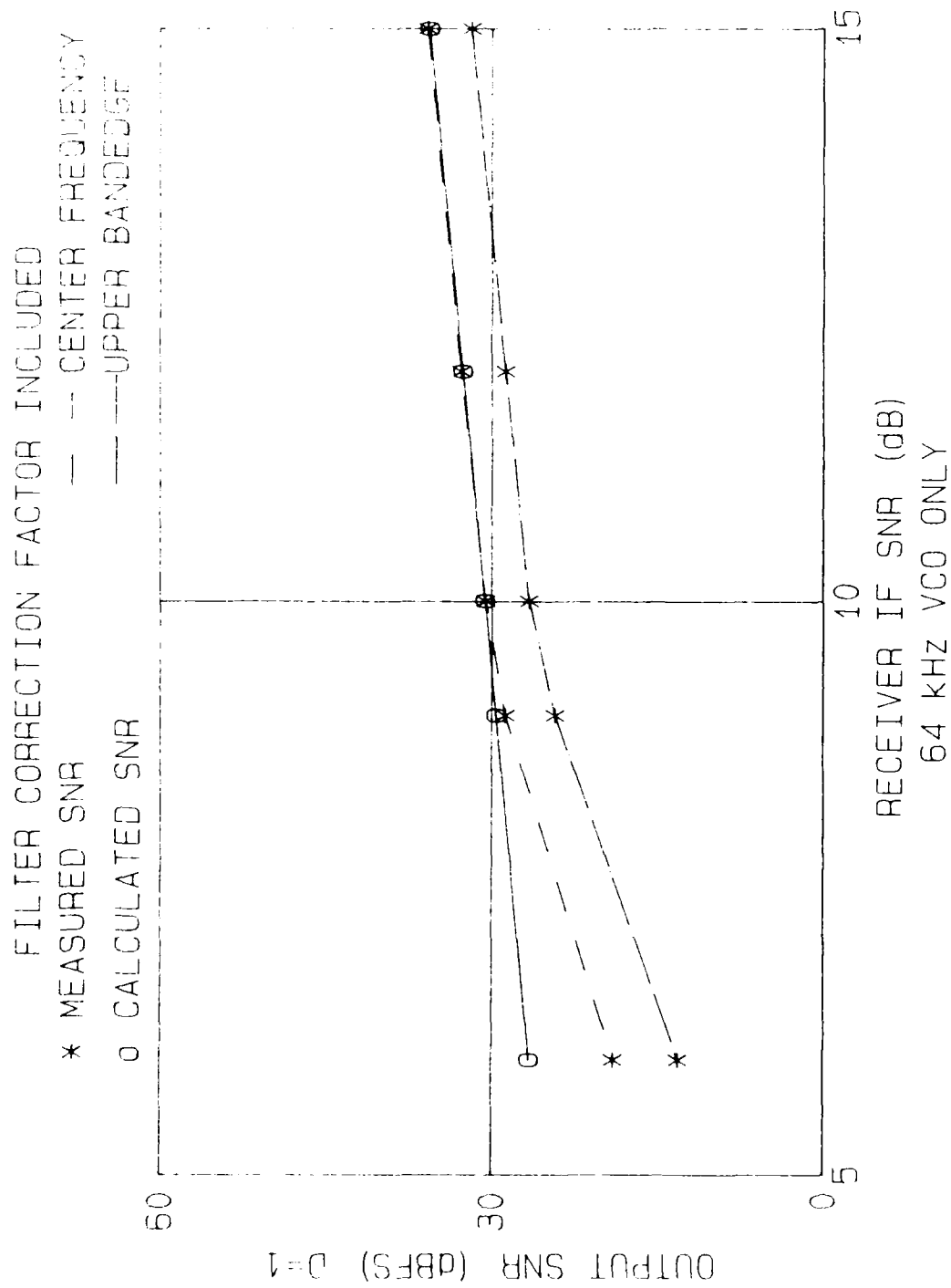


Figure 3.7-13. Measured and Calculated SNRs with Correction Factors ( $D=1$ ).

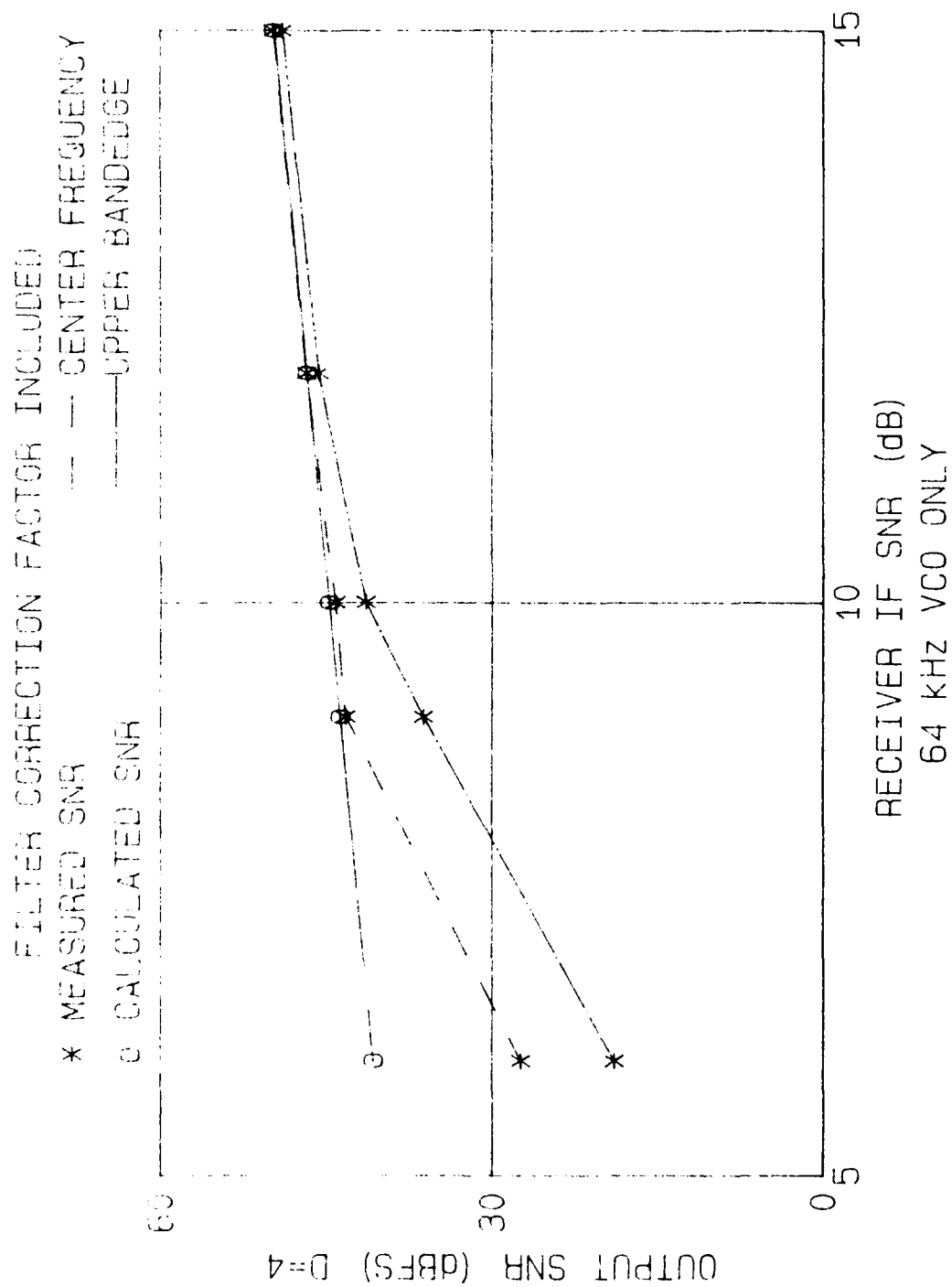


Figure 3.7-14. Measured and Calculated SNRs with Correction Factors (D=4) .



with 20 V peak-to-peak signal gives 60 dBFS. The modulation inputs to the SCOs were DC levels for these tests. The data in figures 3.7-9 and 3.7-10 show that use of the ideal assumptions predicts SNRs that are 2 to 6 dB too large for IF SNRs between 10 and 15 dB. The data in figures 3.7-11 and 3.7-12 include corrections for all the significant error effects except noise pops. The predicted and measured SNRs agree very well at IF SNRs of 12 and 15 dB. The low frequency channels have a 1 to 2 dB error at a 10 dB IF SNR due to the effects of noise pops. The errors are much larger at lower IF SNRs. This data also shows that the receiver noise pops affect the lower frequency channels much more than the higher channels. The data in figures 3.7-13 and 3.7-14 show that the SNR of a signal at upper bandedge is 4 dB lower than a signal at bandcenter for a deviation ratio of one and 1 dB lower for a deviation ratio of four at a 12 dB IF SNR. The large degradation at a deviation ratio of one is caused by the fact that the signal at bandedge is attenuated relative to the noise near bandcenter. Overall, the data in figures 3.7-9 through 3.7-14 suggest that use of a 6 dB correction factor ( $\Gamma$ ) would provide a conservative estimate of discriminator output SNR for most conditions.

### 3.7.3 Transmitter Deviation

An FM/FM system should be designed so that the subcarrier discriminator bandpass SNRs are greater than the receiver IF SNR. If this is not the case the subcarrier discriminator will reach FM threshold before the receiver demodulator. The discriminator output noise will then be much worse than predicted by the equations in this report at a 12 dB IF SNR. A good rule of thumb is to always have:

$$\frac{(\Delta f_i)^2 B_{IF}}{2 f_i^2 B_i} > 2$$

or

$$\Delta f_i > 2 f_i (B_i/B_{IF})^{1/2}$$

Therefore, the peak deviation of a 5.4 kHz PBW SCO which will be received with a 500 kHz IF bandwidth should be at least 0.435 kHz.

Another good rule of thumb is to have the rms deviation of each SCO be at least 10% of the total rms deviation. This minimizes the probability that system non-linearities will introduce enough spurious signals to significantly degrade data quality. For example, a PBW multiplex of 7.5% channels from 1.7 to 93 kHz with a theoretical 9 dB/octave taper would have 52 dB more amplitude in the 93 kHz SCO than the 1.7 kHz SCO. This would overstress the dynamic range of the telemetry transmit, receive, and record system. Increasing the rms deviation of the lowest 8 channels to 10% of the original total rms deviation would increase the total rms deviation by less than 4%.

The first estimate transmitter deviation can be calculated if one knows the required minimum data quality for each channel. Let us assume that the telemetry analysts would like to have the peak-to-peak noise ( $\pm 2$  sigma) due to the telemetry RF link at a 12 dB IF SNR be no greater 2% of the channel bandedge-to-bandedge voltage.

This is achieved when the rms value of the noise is less than 0.5% of full scale (SNR = 46 dBFS). Using this value in our corrected SNR equation (filter correction factor ( $\Gamma$ ) = 6 dB) results in:

$$\text{SNR} = 10 \log \left\{ \frac{6 (\Delta f_i)^2 (\Delta f_{si})^2 B_{IF}}{(f_i)^2 (f_c)^3} \right\} + \text{SNR}_{IF} - \Gamma$$

$$46 = 10 \log \left\{ \frac{6 (\Delta f_i)^2 (\Delta f_{si})^2 B_{IF}}{(f_i)^2 (f_c)^3} \right\} + 12 - 6$$

$$\Delta f_i = \frac{40.8 f_i (f_c)^{3/2}}{\Delta f_{si} (B_{IF})^{1/2}}$$

Let us further assume that we need a PBW multiplex of  $\pm 7.5\%$  channels with center frequencies from 1.7 to 93 kHz, deviation ratios of 5, and a 500 kHz receiver IF bandwidth. The peak deviation of the 93 kHz SCO should be:

$$\Delta f_{93} = \frac{40.8 (93) (1.395)^{3/2}}{6.975 500^{1/2}} \text{ kHz peak}$$

$$\Delta f_{93} = 40.1 \text{ kHz peak or } 28.3 \text{ kHz rms.}$$

The rms deviation of the total signal will be approximately 1.3 times the rms deviation of the highest frequency subcarrier or 36.8 kHz. Another reasonable rule-of-thumb is that the rms deviation should be approximately one-sixth of the receiver IF bandwidth. This means the total rms deviation for a 500 kHz IF bandwidth should be approximately 83 kHz. If we double the values calculated using the equation we would get a total rms deviation of approximately 75 kHz. This means that each of the lower frequency SCOs should have an rms deviation of approximately 7.5 kHz or a peak deviation of 10.6 kHz. This is approximately one-eighth of the deviation of the 93 kHz channel (now 80.2 kHz peak). Since the deviation of fixed percentage PBW SCOs changes by a factor of 8 when the center frequency changes by 4, we only have to calculate the deviations for the channels with center frequencies above 23 kHz. Our equation is now:

$$\Delta f_i = \frac{2 (40.8) (f_i) (f_c)^{3/2}}{\Delta f_{si} (B_{IF})^{1/2}}$$

$$\Delta f_{70} = \frac{2 (40.8) (70) (1.05)^{3/2}}{5.25 (500)^{1/2}}$$

$$\Delta f_{70} = 52.4 \text{ kHz peak}$$

Similarly we get:

$$\begin{aligned}\Delta f_{52.5} &= 34 \text{ kHz peak} \\ \Delta f_{40} &= 22.6 \text{ kHz peak} \\ \Delta f_{30} &= 14.7 \text{ kHz peak} \\ \Delta f_{22} &= 10.6 \text{ kHz peak} \\ \Delta f_{14.5} &= 10.6 \text{ kHz peak} \\ &\vdots \\ &\vdots \\ \Delta f_{1.7} &= 10.6 \text{ kHz peak.}\end{aligned}$$

The overall rms transmitter deviation is approximately 77.3 kHz. We have designed an FM/FM system which will provide data quality that exceeds our requirements by a minimum of 6 dB. However, we have assumed no error due to tape recorder effects such as tape speed or flutter.

Let us now assume that we need to add a 165 kHz  $\pm$  15% SCO to the multiplex to transmit a 40 kilobit per second (kb/s) signal for a special test. We need to guarantee that the subcarrier discriminator will reach FM threshold later than the receiver demodulator. Therefore, the minimum peak deviation is:

$$\begin{aligned}\Delta f_{165} &= 2 (165) \{(165)(.3)/500\}^{1/2} \\ \Delta f_{165} &= 104 \text{ kHz peak or } 73.4 \text{ kHz rms.}\end{aligned}$$

If we now reduce the peak deviation of the other SCOs to the minimum values calculated earlier (with a minimum of 12 kHz peak) we get deviations of:

$$\begin{aligned}\Delta f_{165} &= 104 \text{ kHz peak} \\ \Delta f_{93} &= 40.2 \text{ kHz peak} \\ \Delta f_{70} &= 26.2 \text{ kHz peak} \\ \Delta f_{52.5} &= 17 \text{ kHz peak} \\ \Delta f_{40} &= 12 \text{ kHz peak} \\ \Delta f_{30} &= 12 \text{ kHz peak} \\ &\vdots \\ &\vdots \\ \Delta f_{1.7} &= 12 \text{ kHz peak}\end{aligned}$$

This gives a total rms deviation of 86.6 kHz.

This is slightly more than one-sixth of the receiver IF bandwidth. This is tolerable because most of the signal energy is in the 165 kHz SCO. The maximum desirable peak deviation if only one SCO is present is approximately 0.4 times the receiver IF bandwidth. The maximum desirable SCO frequency is also approximately 0.4 times the receiver IF bandwidth.

### 3.7.4 Receiver IF Bandwidth

The "best" receiver IF bandwidth is a function of the maximum SCO frequency, the transmitter deviation, and the link analysis. The main disadvantages of a wide receiver IF bandwidth are:

1. FM threshold is reached sooner.
2. If the signal is being predetection recorded, the tape speed may have to be increased because the predetection carrier frequency should be at least one-half of the IF bandwidth.

The main disadvantages of a narrow IF bandwidth are:

1. The receiver RF tuning becomes very critical.
2. The video output distortion increases.
3. The receiver may reach FM threshold sooner at the maximum deviation excursions.

Some general rules-of-thumb for receiver IF bandwidth are:

1. The IF bandwidth should be at least 2.5 times the highest SCO frequency.
2. The IF bandwidth should be at least 6 times the transmitter rms deviation.
3. The IF bandwidth should be narrow enough so that the probability of being above FM threshold is sufficiently high.

The discriminator output SNR is independent of the IF bandwidth when the signal is above FM threshold (no noise pops) and the distortion is much smaller than the video noise. Receiver IF bandwidths are usually only available in discrete steps with a step size between 50 and 100 percent. It is usually desirable to choose the narrowest IF bandwidth that meets 1 and 2 above.

### 3.7.5 Effect of Adjacent Channel or Co-channel Interference on FM/FM Discriminator Output

This section will describe a method that can be used to calculate the amplitude at the discriminator output due to an interfering sine wave whose amplitude is less than the desired signal. Assume that the discriminator input can be described by:

$$A \sin (2\pi f_1 t) + B \sin (2\pi f_2 t + \phi)$$

where  $A \sin (2\pi f_1 t)$  is the desired signal.

The frequency of the spurious signal at the discriminator output will be  $|f_1 - f_2|$ . The amplitude at the discriminator output will be:

$$\frac{B K_d |f_1 - f_2| G_{IF}(f_2) G_{LPF}(|f_1 - f_2|)}{A G_{IF}(f_1)}$$

where:

$K_d$  = Discriminator gain constant (V/Hz)

$G_{IF}(f)$  = Discriminator bandpass filter voltage gain at frequency  $f$

$G_{LPF}(f)$  = Discriminator output lowpass filter voltage gain at frequency  $f$ .

As an example, let us calculate the interference between two adjacent CBW "A" channels when the lower channel is at UBE and the higher channel is at LBE. We will assume a 48 kHz discriminator with input signals at 50 and 54 kHz. The frequency of the interfering signal will therefore be 4 kHz. The measured values of gain and voltage were:

$$\begin{aligned} B/A &= 0.984 \\ K_d &= 2.5 \text{ V/kHz} \\ G_{IF}(54) &= 0.160 \\ G_{IF}(50) &= 0.816 \\ G_{LPF}(4) &= 0.186. \end{aligned}$$

Therefore, the calculated output amplitude at 4 kHz is:

$$\text{Amplitude} = 0.984 (2.5) (4) (0.16) (0.186) / (2 (0.816))$$

$$\text{Amplitude} = 0.254 \text{ V rms.}$$

The measured amplitude at a frequency of 4 kHz was 0.249 V rms. These values agree very well.

As a second example let us assume we have a 48 kHz desired signal with an interfering signal at 48.4 kHz whose amplitude is one-tenth of the desired signal. The frequency of the spurious component will be 400 Hz ( $|48 - 48.4|$  kHz). The calculated amplitude is:

$$0.1 (2.5) (0.4) (1.0) (0.993) / (2 (0.999)) = 0.0703 \text{ V rms.}$$

The measured amplitude under these conditions at 400 Hz was 0.0694 V rms.

If either the desired or the undesired signal is modulated, the instantaneous spurious output can be calculated as shown above using the instantaneous amplitude and frequency of both signals. This method also works when there is more than one undesired signal. The measurements were made using a pulse averaging discriminator. Other types of discriminators may have a loop filter gain that must also be included.

### 3.7.6 Record Level for Tape Recorder

Figures 3.7-15 and 3.7-16 show the effects of recording a non-preemphasized CBW multiplex at normal record level (0 dBN) and at one-half of normal record level (-6 dBN). Normal record level is the rms input voltage of a sine wave at one-tenth upper bandedge which produces 1 percent third harmonic distortion. Figure 3.7-15 shows that the distortion terms are only 30 dB below the signals with a 0 dBN input. Figure 3.7-16 shows that the largest distortion terms are approximately 38 dB below the signals with a -6 dBN input. The noise is smaller than the distortion in both cases. Therefore, the best record level for an FM/FM multiplex will frequently be less than 0 dBN.

### 3.7.7 Effect of Tape Recorder Flutter and Speed Error on FM/FM Data Quality

FM/FM data accuracy is directly related to the difference in instantaneous tape speed at the time of recording and at the time of playback. The error can also be increased by any tape speed errors during tape copying (dubbing). Typical specifications for laboratory recorders give absolute tape speed accuracy of  $\pm 0.1\%$  in tachometer mode and  $\pm 0.01\%$  in tape servo mode. The typical flutter in tachometer mode at 30 ips is 0.2% peak-to-peak (2 sigma value) or 0.05% rms. Recorders in severe environments can have errors of ten times these values. If we reproduce data from a tape copy and make worst case assumptions (laboratory recorder) we can have a tape speed error of 0.4% (all operations in tachometer mode) and a flutter error of 0.1% rms. The effect that this will have on data quality varies with the percentage deviation of the subcarrier channel. The smallest percentage deviation channel is the 176A channel which has a specified maximum peak-to-peak deviation of 4 kHz which is 2.27% of the center frequency. A speed error of 0.4% translates to an error of 17.6% of full scale. An rms flutter value of 0.1% translates to rms noise of 4.4% of full scale. The narrowest PBW channels have maximum deviation limits of  $\pm 7.5\%$ . This translates to a speed error of 1.3% of full scale and a flutter error of 0.33% of full scale. These errors can be greatly reduced by the use of a properly damped tape playback servo system, tape speed compensation, and/or digital time base correction.

### 3.7.8 Preemphasis

Preemphasis is the process of increasing the amplitude (deviation) of the higher frequency and wider bandwidth SCOs to keep the SNRs at the discriminator bandpass outputs nearly the same for all channels with the same data quality requirements. The SNR (voltage ratio) at the output of the bandpass filter is directly proportional to the SCO peak deviation, and inversely proportional to the SCO center frequency and the square root of the discriminator bandpass bandwidth. Therefore, the SCO peak deviation should be proportional to the product of the SCO center frequency and the square root of the discriminator bandpass bandwidth. The equation for calculating SCO peak deviation provides the proper preemphasis for each SCO. Figures 3.7-17 through 3.7-21 show typical baseband spectra for CBW and PBW multiplexes with and without preemphasis. Figure 3.7-20 illustrates the problem of using a straight 9 dB/octave preemphasis for a PBW multiplex. The low frequency signals disappear. Figure 3.7-21 shows the same signal with a minimum rms deviation of 10% of the total rms deviation.

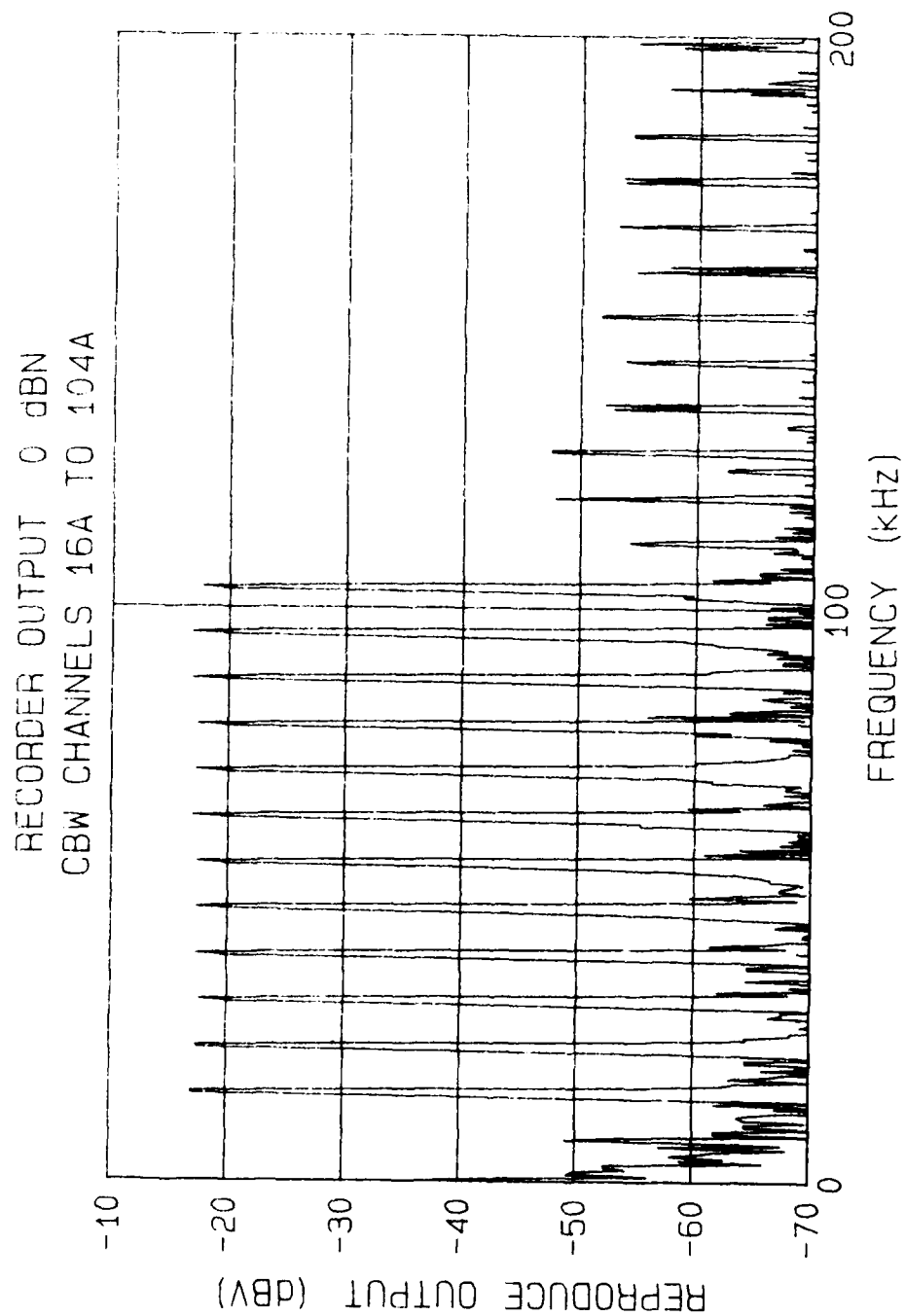


Figure 3.7-15. Tape Recorder Output with Normal Record Level CBW Input.

RECORDER OUTPUT -6 dBN  
CBW CHANNELS 16A TO 104A

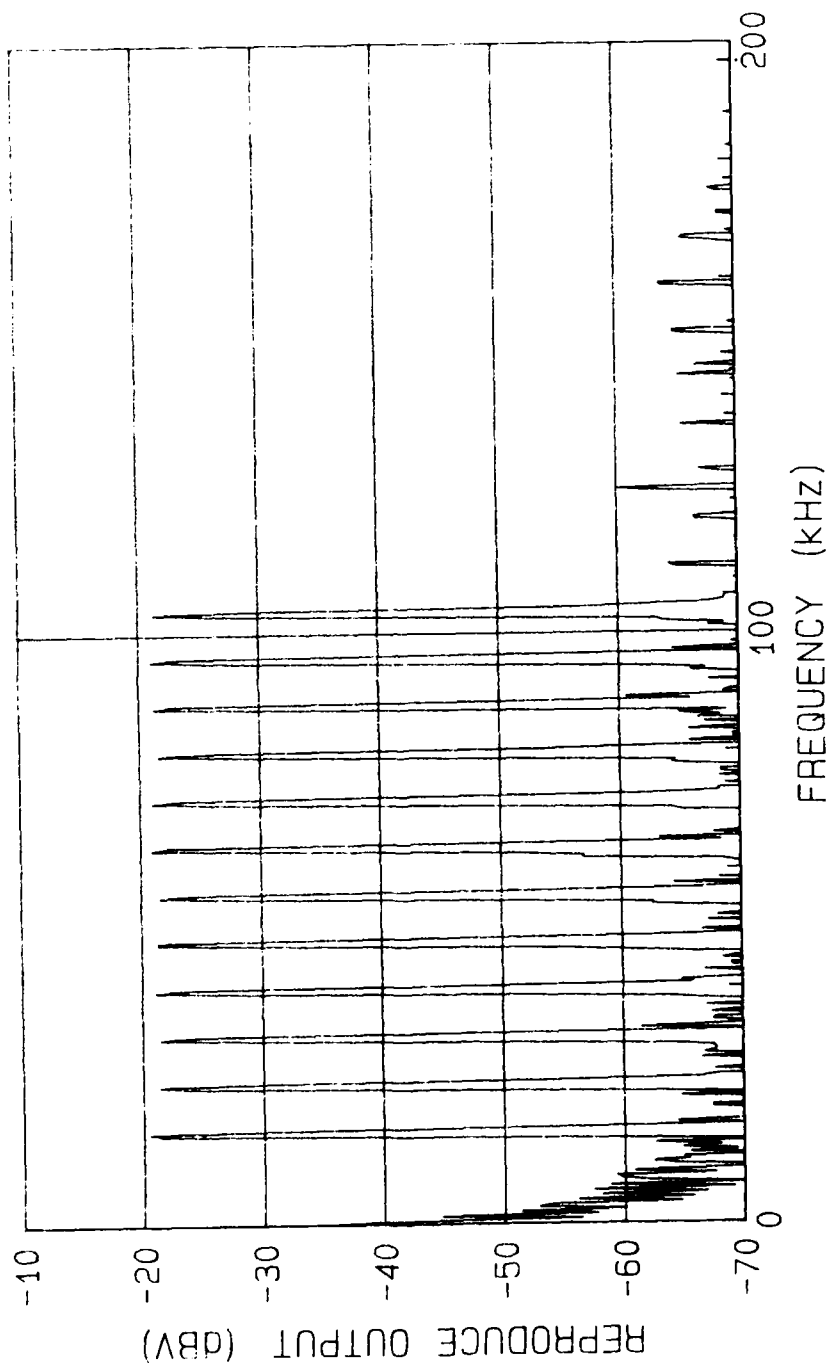


Figure 3.7-16. Tape Recorder Output with (Normal Record Level) / 2 CBW Input.



# CBW SPECTRUM WITH NO PREEMPHASIS

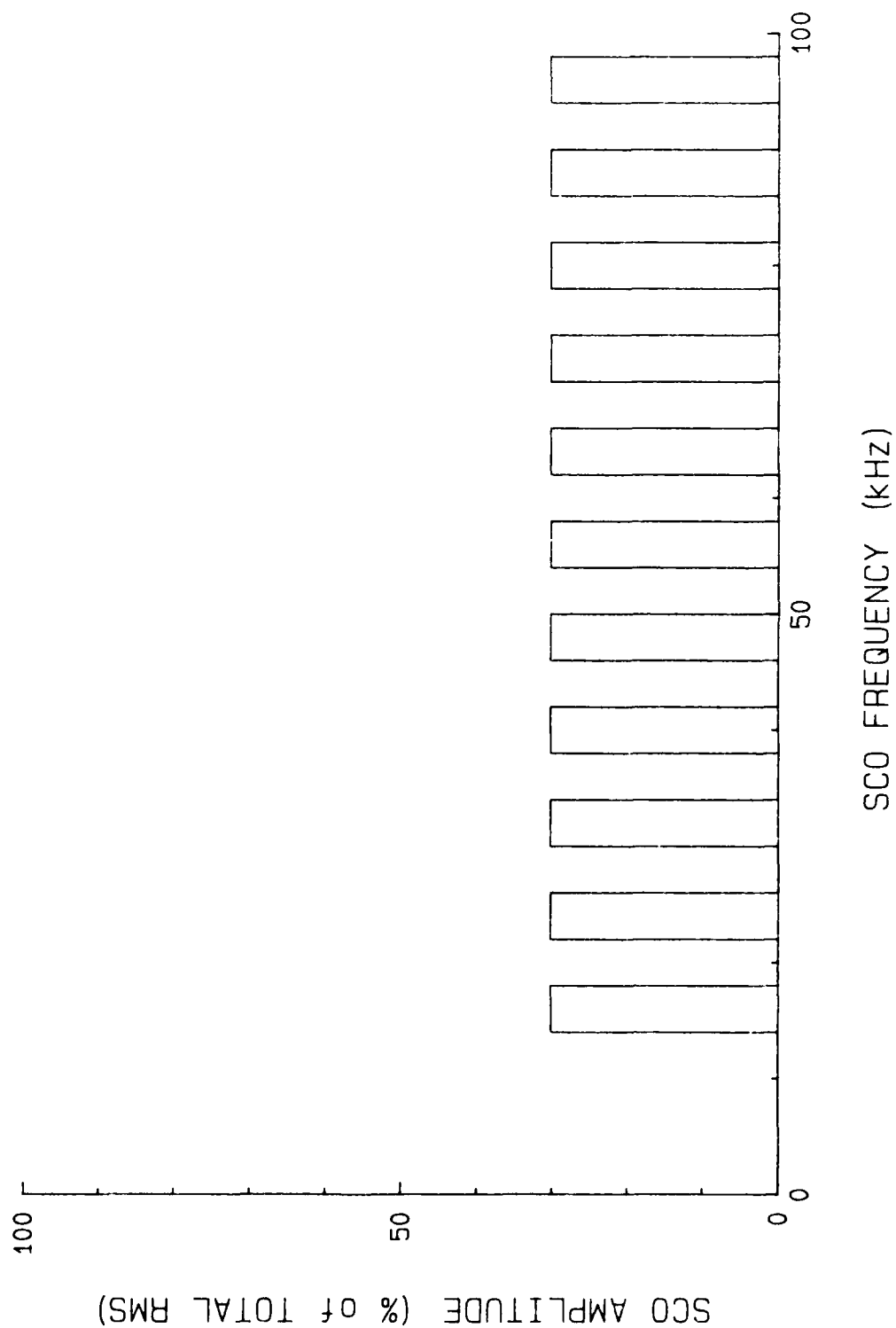


Figure 3.7-17. CBW Spectrum with No Preemphasis.

# CBW SPECTRUM WITH 6 dB/OCTAVE PREEMPHASIS

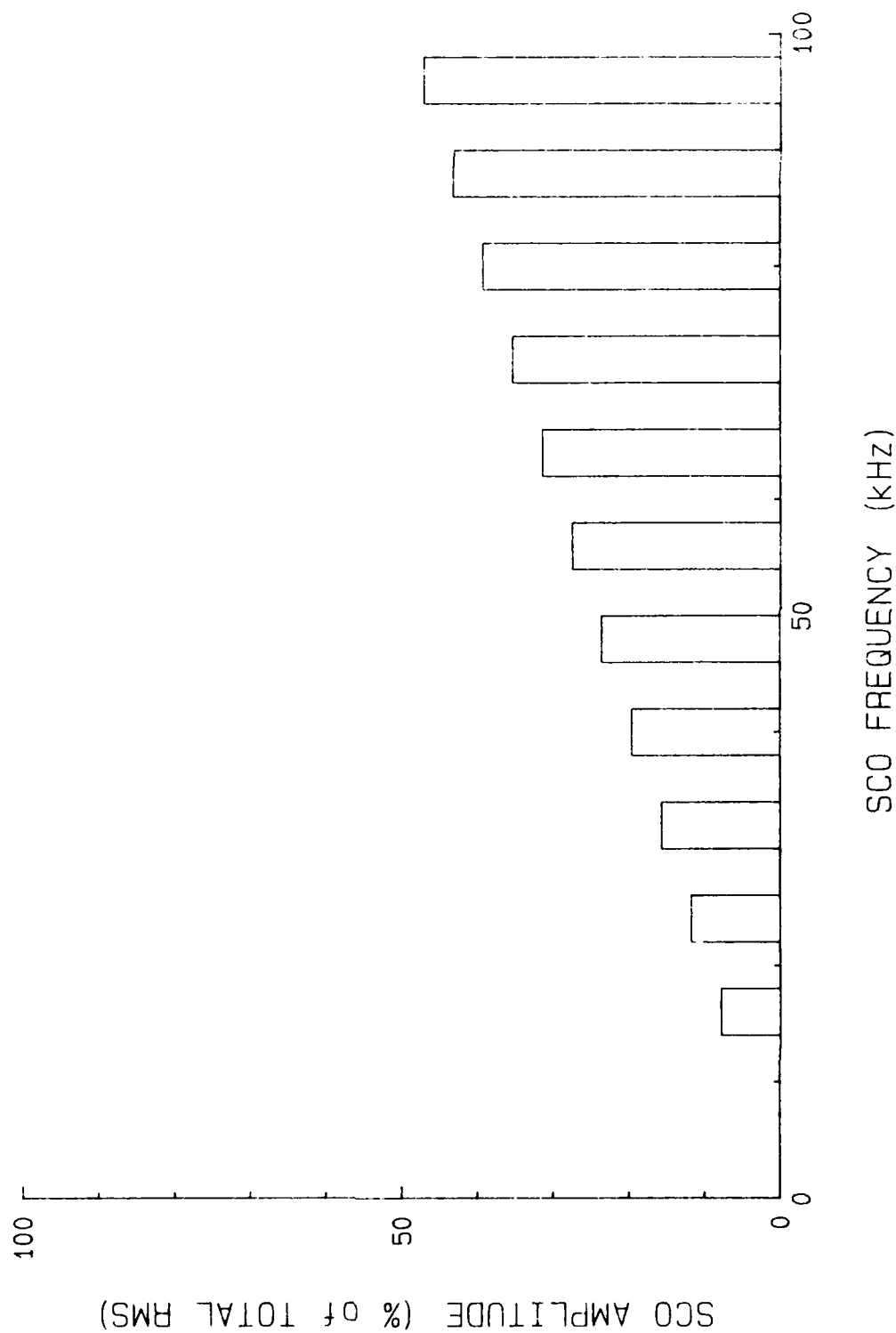


Figure 3.7-18. CBW Spectrum with 6 dB/Octave Preemphasis.

# PBW SPECTRUM WITH NO PREEMPHASIS

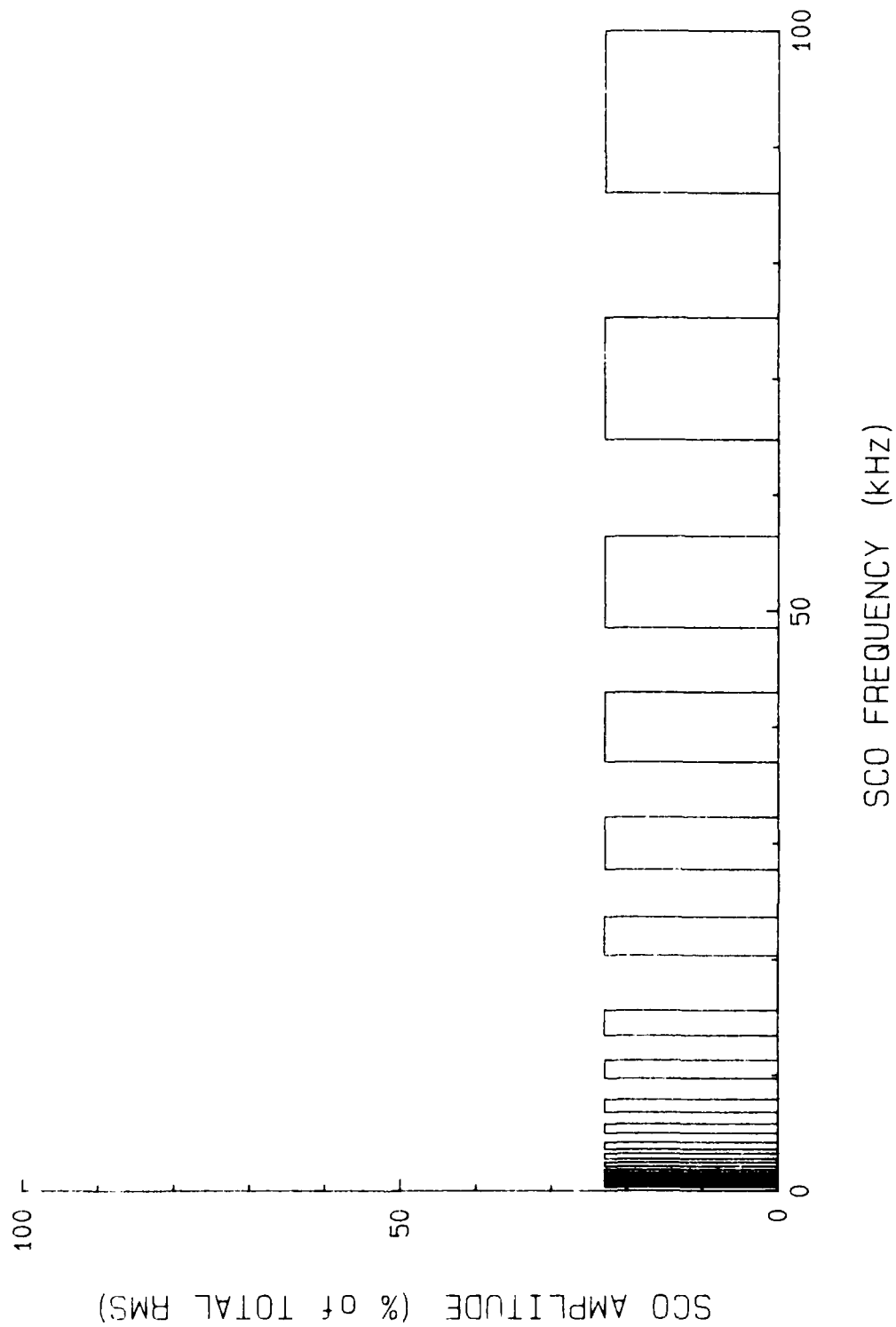


Figure 3.7-19. PBW Spectrum with No Preemphasis

# PBW SPECTRUM WITH 9 dB/OCTAVE PREEMPHASIS

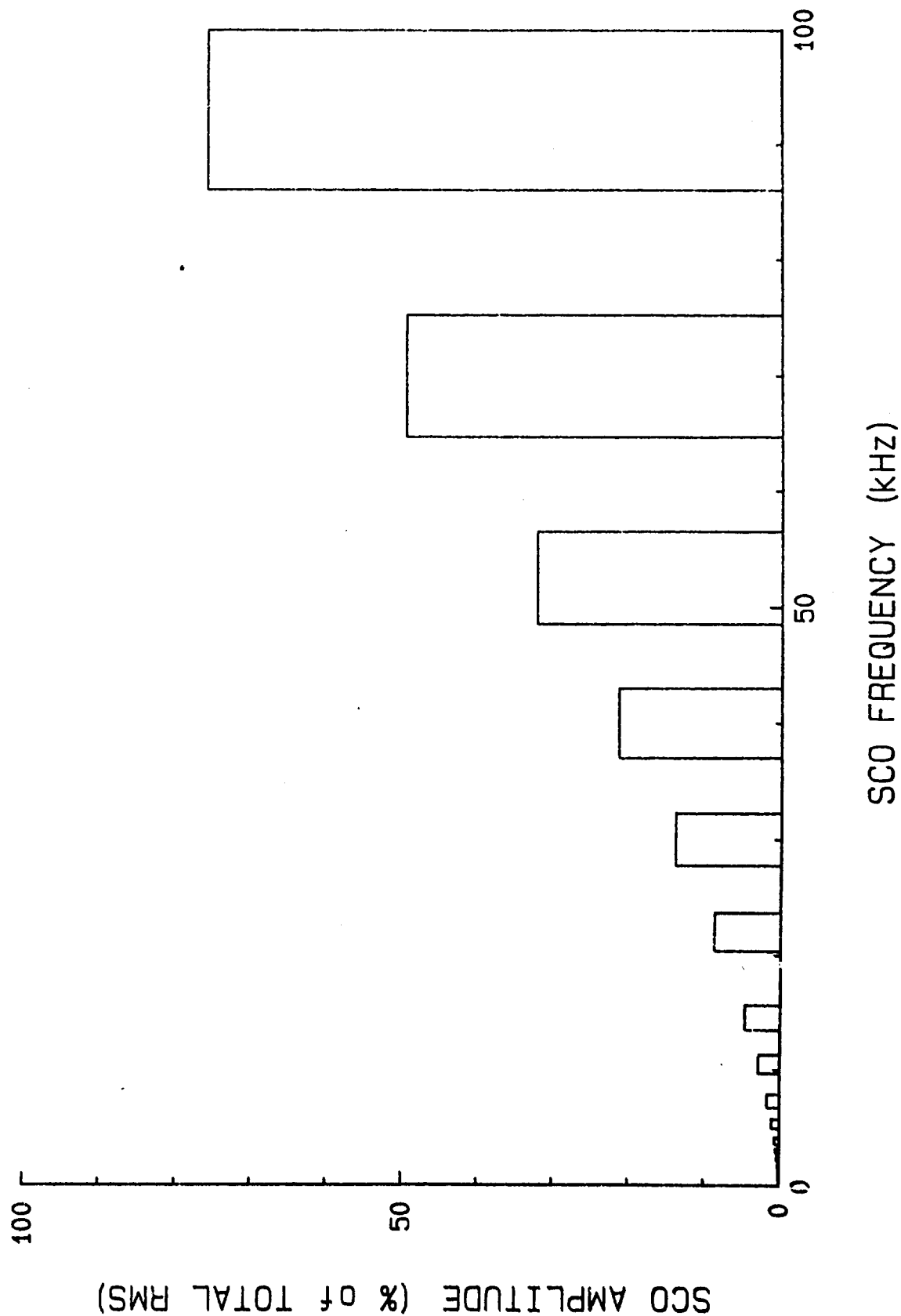


Figure 3.7-20. PBW Spectrum with 9 dB/Octave Preemphasis.

PBW SPECTRUM WITH 9 dB/OCTAVE PREEMPHASIS  
10% MINIMUM DEVIATION

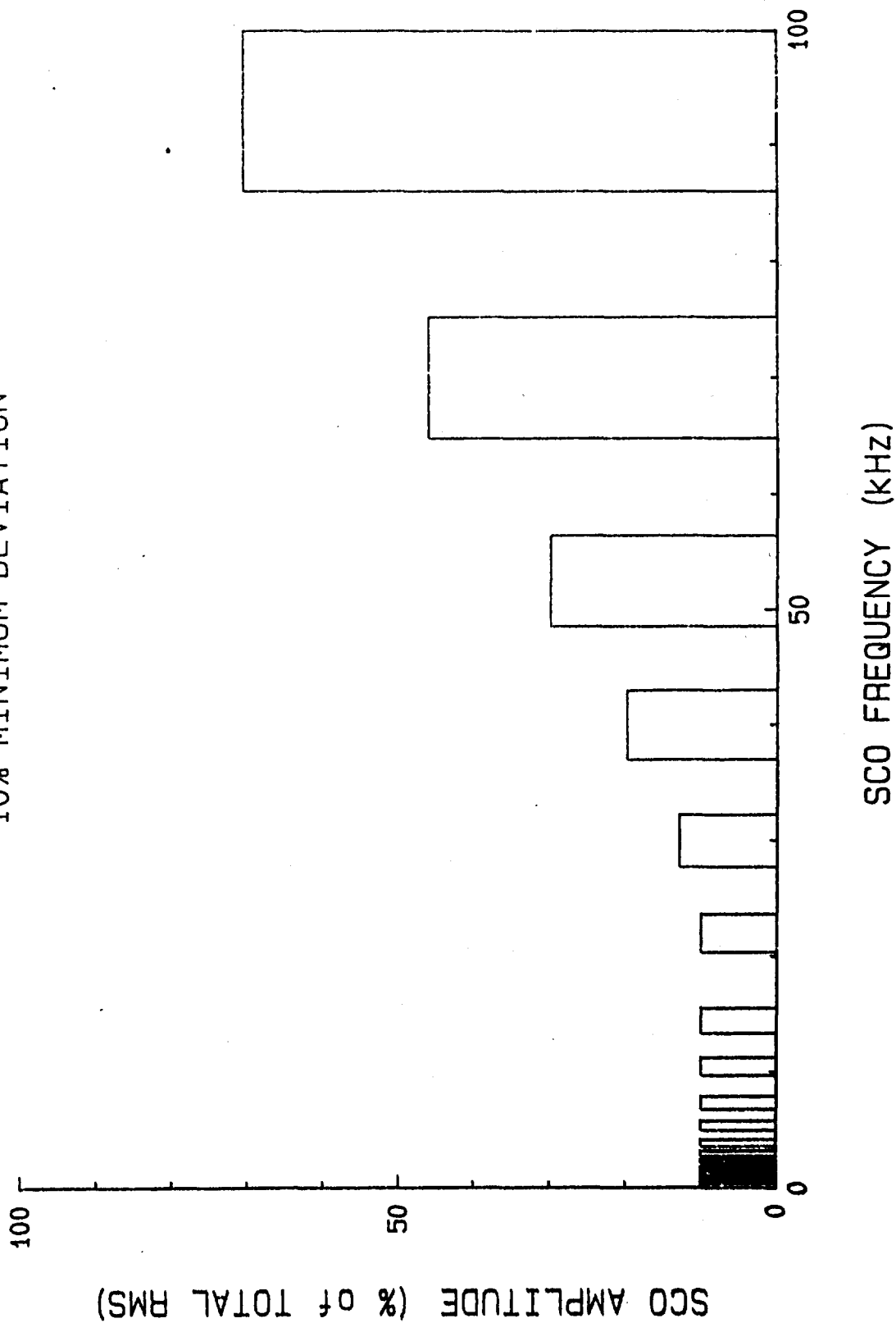


Figure 3.7-21. PBW Spectrum with 9 dB/Octave Preemphasis and 10% Minimum Amplitude.

### 3.7.9 FM Spectrum With Single Sine Wave Modulation

We can represent a sine wave carrier which is frequency modulated by a single sine wave by<sup>18</sup>:

$$f(t) = \cos(\omega_c t + \beta \sin \omega_m t)$$

$$f(t) = \cos(\omega_c t) \cos(\beta \sin \omega_m t) - \sin(\omega_c t) \sin(\beta \sin \omega_m t)$$

$$\begin{aligned} f(t) = J_0(\beta) \cos(\omega_c t) &- J_1(\beta) [\cos(\omega_c - \omega_m)t - \cos(\omega_c + \omega_m)t] \\ &+ J_2(\beta) [\cos(\omega_c - 2\omega_m)t + \cos(\omega_c + 2\omega_m)t] \\ &- J_3(\beta) [\cos(\omega_c - 3\omega_m)t - \cos(\omega_c + 3\omega_m)t] \\ &+ \dots \end{aligned}$$

where:

$\omega_c$  = Frequency of carrier in radians/sec.

$\omega_m$  = Frequency of modulating signal in radians/sec.

$\beta$  = Peak deviation/frequency of modulating signal

$J_i(\beta)$  =  $i^{\text{th}}$  order Bessel function of the first kind.

The amplitude of the remnant carrier is  $J_0(\beta)$ , the amplitudes of the sideband pairs spaced  $\pm\omega_m$  away from the carrier are  $J_1(\beta)$ , etc. The unmodulated carrier amplitude is assumed to be 1. Table 3.7-1 lists the amplitude (in dBc) of  $J_i(x)$  for  $i = 0, 1, 2, 3, 4, 5$ , and 6 and for  $x = 0.1$  to 5.0 in steps of 0.1. The value of -18.79 dBc for  $J_2(1.0)$  means that the theoretical amplitude of the components at  $\omega_c \pm 2\omega_m$  will be 0.1149 times the unmodulated carrier amplitude for  $\beta = MI = 1.0$ . This is illustrated in figure 3.7-22.

If we modulate a carrier with a single sine wave, we can use the relative amplitudes of the carrier components to determine the peak deviation. This is commonly done using either the first null of the carrier or the first null of the first sideband. If we look at table 3.7-1, we find that  $J_0$  has a minimum at approximately 2.4 and  $J_1$  has a minimum at approximately 3.8. The actual values of MI for the first two carrier nulls are approximately 2.40482 and 5.52008 while the first null of  $J_1$  occurs at approximately 3.83171. If the modulation amplitude is set to a very low value and the amplitude increased slowly until the first carrier null occurs, (monitor modulated carrier on spectrum analyzer), we find the amplitude which produces a peak deviation of approximately 2.405 times the modulating frequency. At this MI the amplitude of the second sideband should be at least 1 dB lower than the amplitude of the first sideband and the amplitudes of the higher order sidebands should decrease rapidly. This is illustrated in figure 3.7-23. We can also use the relative amplitudes of the sidebands to calculate the effective peak deviation in situations where we may not be able to vary parameters to achieve a null. The equations in table 3.7-2 allow one to calculate the approximate modulation index for  $0.1 < MI < 1.6$  from the difference in amplitude between  $J_0$  and  $J_1$ .

<sup>18</sup>Panter, P. F. *Modulation, Noise, and Spectral Analysis*. McGraw-Hill, New York, pp. 236-270, 1965.

Table 3.7-1. FM Sideband Power Versus MI.

MI	FM SIDEBAND POWER (dBc)						
	J0	J1	J2	J3	J4	J5	J6
.10	-.02	-26.03	-58.07	-93.63	-131.69	-171.69	-213.27
.20	-.09	-20.04	-46.05	-75.58	-107.62	-141.60	-177.16
.30	-.20	-16.58	-39.04	-65.05	-93.56	-124.01	-156.04
.40	-.35	-14.15	-34.10	-57.59	-83.59	-111.54	-141.07
.50	-.55	-12.31	-30.28	-51.82	-75.88	-101.88	-129.47
.60	-.80	-10.85	-27.20	-47.13	-69.59	-94.00	-120.00
.70	-1.10	-9.66	-24.61	-43.19	-64.29	-87.35	-112.01
.80	-1.45	-8.66	-22.40	-39.79	-59.72	-81.61	-105.10
.90	-1.86	-7.83	-20.48	-36.81	-55.70	-76.56	-99.01
1.00	-2.32	-7.13	-18.79	-34.17	-52.12	-72.05	-93.58
1.10	-2.86	-6.54	-17.29	-31.80	-48.90	-67.99	-88.68
1.20	-3.46	-6.05	-15.95	-29.66	-45.98	-64.29	-84.22
1.30	-4.15	-5.65	-14.75	-27.72	-43.31	-60.91	-80.12
1.40	-4.93	-5.32	-13.67	-25.93	-40.85	-57.79	-76.35
1.50	-5.82	-5.07	-12.69	-24.30	-38.59	-54.90	-72.84
1.60	-6.83	-4.88	-11.80	-22.79	-36.48	-52.21	-69.57
1.70	-8.00	-4.76	-11.00	-21.40	-34.52	-49.70	-66.52
1.80	-9.37	-4.71	-10.28	-20.10	-32.69	-47.34	-63.65
1.90	-11.00	-4.71	-9.63	-18.91	-30.98	-45.13	-60.95
2.00	-13.00	-4.78	-9.05	-17.79	-29.37	-43.05	-58.40
2.10	-15.57	-4.91	-8.53	-16.76	-27.86	-41.08	-55.99
2.20	-19.14	-5.10	-8.07	-15.79	-26.44	-39.22	-53.70
2.30	-25.11	-5.35	-7.66	-14.90	-25.10	-37.46	-51.52
2.40	-52.01	-5.68	-7.31	-14.06	-23.83	-35.79	-49.46
2.50	-26.31	-6.07	-7.01	-13.29	-22.64	-34.20	-47.48
2.60	-20.28	-6.54	-6.76	-12.57	-21.51	-32.69	-45.60
2.70	-16.93	-7.10	-6.57	-11.90	-20.45	-31.25	-43.81
2.80	-14.65	-7.75	-6.42	-11.29	-19.44	-29.88	-42.09
2.90	-12.98	-8.51	-6.32	-10.72	-18.49	-28.57	-40.44
3.00	-11.70	-9.39	-6.27	-10.20	-17.59	-27.32	-38.87
3.10	-10.69	-10.43	-6.26	-9.72	-16.74	-26.14	-37.36
3.20	-9.89	-11.66	-6.31	-9.29	-15.93	-25.00	-35.91
3.30	-9.26	-13.13	-6.41	-8.90	-15.18	-23.91	-34.51
3.40	-8.77	-14.93	-6.56	-8.56	-14.46	-22.88	-33.18
3.50	-8.40	-17.24	-6.77	-8.25	-13.79	-21.89	-31.89
3.60	-8.14	-20.40	-7.04	-7.99	-13.16	-20.95	-30.66
3.70	-7.99	-25.38	-7.36	-7.76	-12.57	-20.04	-29.47
3.80	-7.90	-37.84	-7.76	-7.58	-12.02	-19.18	-28.33
3.90	-7.92	-31.29	-8.23	-7.43	-11.50	-18.36	-27.24
4.00	-8.02	-23.60	-8.77	-7.33	-11.02	-17.58	-26.18
4.10	-8.21	-19.72	-9.41	-7.26	-10.58	-16.84	-25.17
4.20	-8.48	-17.16	-10.16	-7.24	-10.17	-16.13	-24.19
4.30	-8.85	-15.29	-11.02	-7.26	-9.80	-15.46	-23.25
4.40	-9.31	-13.86	-12.04	-7.33	-9.46	-14.82	-22.35
4.50	-9.88	-12.73	-13.24	-7.44	-9.16	-14.21	-21.49
4.60	-10.57	-11.82	-14.68	-7.60	-8.89	-13.64	-20.65
4.70	-11.39	-11.09	-16.45	-7.80	-8.65	-13.10	-19.86
4.80	-12.38	-10.50	-18.71	-8.06	-8.45	-12.59	-19.09
4.90	-13.57	-10.04	-21.80	-8.38	-8.28	-12.11	-18.36
5.00	-15.01	-9.69	-26.64	-8.76	-8.15	-11.66	-17.65

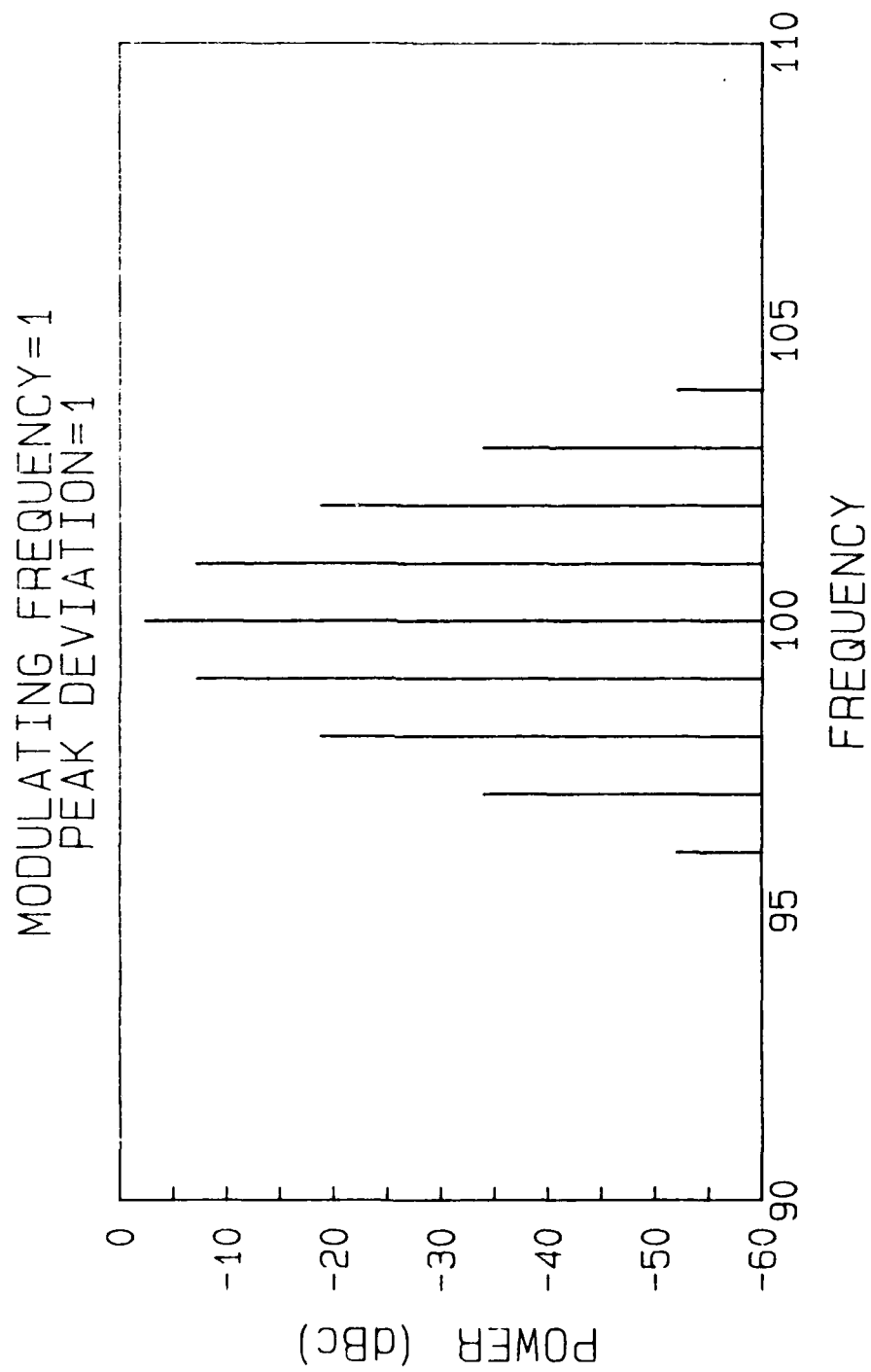


Figure 3.7-22. FM Spectrum with Single Sine Wave Modulation and  $MI=1$ .



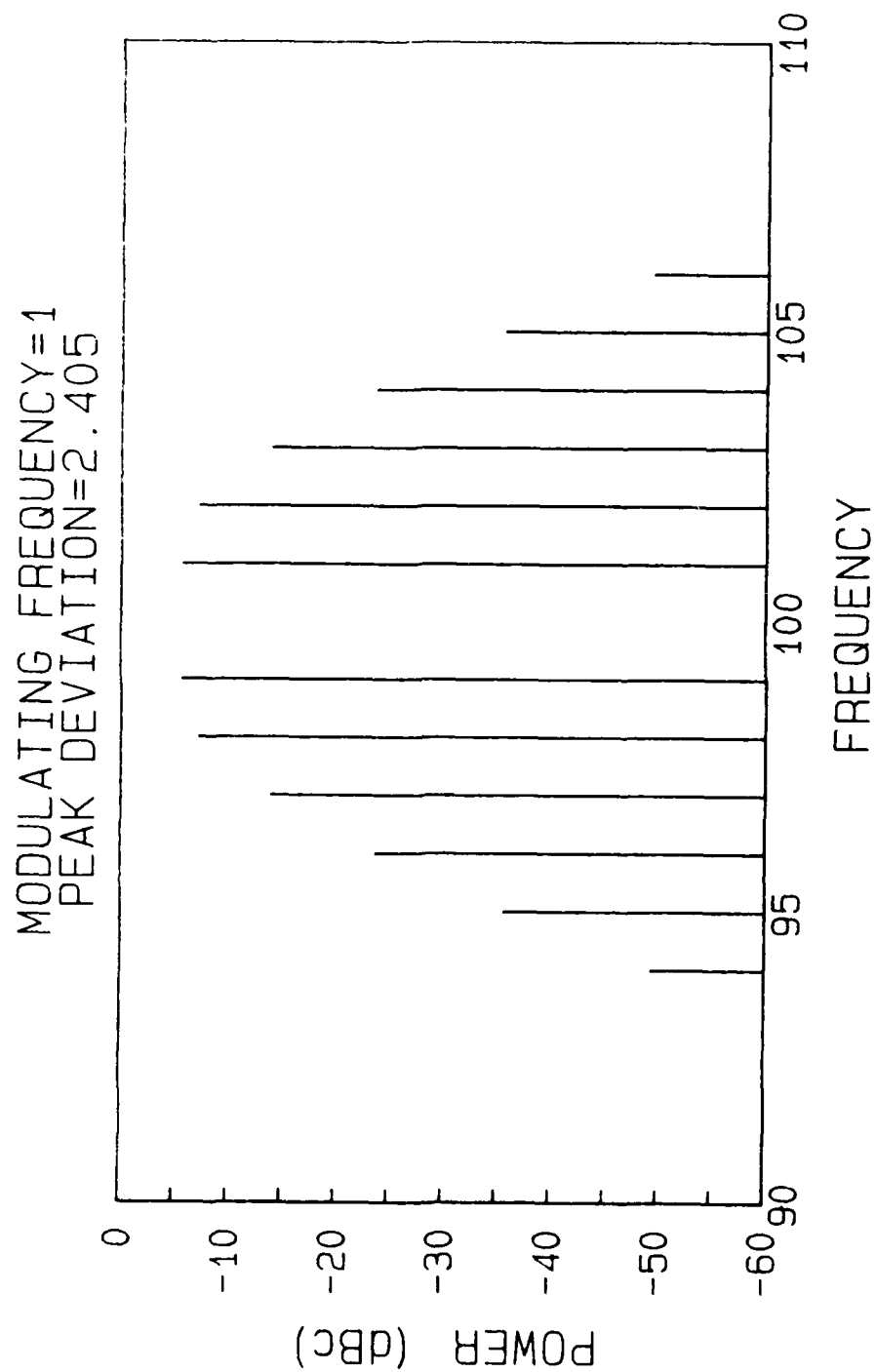


Figure 3.7-23. FM Spectrum with Single Sine Wave Modulation and  $MI=2.405$ .

Table 3.7-2. Coefficients of equation for using  $J_0/J_1$  (dB) to calculate MI for  $MI < 1.6$ .

Min $J_0/J_1$	Max $J_0/J_1$	$a_0$	$a_1$	$a_2$	Max error
16.5	26	1.1237	-0.06922	0.001150	0.0017
10	16.5	1.4582	-0.10886	0.002532	0.0007
6	12.7	1.4992	-0.11530	0.002601	0.0004
2.5	7	1.4540	-0.10191	0.001545	0.0009
3.5	6	1.4560	-0.10233	0.001546	0.0002
-2	2.5	1.4345	-0.08780	-0.001232	0.0010

$$MI = a_0 + a_1x + a_2x^2$$

where:

$$x = J_0/J_1 \text{ (dB) or } J_0 \text{ (dB)} - J_1 \text{ (dB)}$$

MI = peak deviation/modulating frequency

Many modern spectrum analyzers allow the measurement of the difference in amplitude between two components simply and accurately. The equations in table 3.7-2 are useful when the higher order components ( $J_2$ ,  $J_3$ , etc.) are at least 5 dB lower in amplitude than the smaller of  $J_0$  and  $J_1$ . This occurs when the modulation index is less than approximately 1.6. The equations were developed by fitting a least squares curve of the form  $MI = a_0 + a_1x + a_2x^2$  to the ideal values for MI,  $J_0(MI)$ , and  $J_1(MI)$ . The accuracy of these equations is better than 0.5% for  $J_0/J_1 < 20$  dB. As an example, assume that  $J_0$  is 6 dB larger than  $J_1$  and all other components are at least 10 dB lower than  $J_1$ . The fifth set of coefficients has the lowest maximum error of the sets that include 6 dB for  $J_0/J_1$ . Using this equation we get:

$$MI = 1.456 + (-0.10233)(6) + .001546 (6)^2$$

$$MI = 0.8977.$$

If the sine wave modulation frequency is 100 kHz then the peak deviation is 89.77 kHz. The modulation frequency is the difference in frequency between any two adjacent spectral components. If we look up 0.9 on the Bessel table in table 3.7-1 we get  $J_0 = -1.86$  dB and  $J_1 = -7.83$  dB.

### 3.7.10 RF Spectrum of an FM/FM Multiplex

An RF carrier that is frequency modulated by the sum of N sine waves can be represented by:

$$f_c(t) = \cos [\omega_c t + \beta_1 \sin (\omega_1 t + \phi_1) + \beta_2 \sin (\omega_2 t + \phi_2) + \dots + \beta_n \sin (\omega_n t + \phi_n)].$$

It can be shown that the amplitude at frequency:

$$\omega_c \pm a_1 \omega_1 \pm a_2 \omega_2 \pm \dots \pm a_n \omega_n$$

is equal to:  $J_{a1}(\beta_1) J_{a2}(\beta_2) \dots J_{an}(\beta_n)$

or in dB:  $J_{a1}(\beta_1) + J_{a2}(\beta_2) + \dots + J_{an}(\beta_n).$

This will be illustrated with a few simple examples. First, assume that we have a carrier frequency of 100 modulated by sine waves at frequencies of 1 and 1.4 both with a modulation index of 1. The power at the carrier frequency will be  $J_0(1) + J_0(1)$  or  $-2.32 + (-2.32) = -4.64$  dBc. The power at 99 and 101 will be  $J_1(1) + J_0(1)$  or  $-7.13 + (-2.32) = -9.45$  dBc. The power at 98.6 and 101.4 will be  $J_0(1) + J_1(1)$  or  $-2.32 + (-7.13) = -9.45$  dBc. The power at 96.6, 99.4, 100.6, and 103.4 will be  $J_2(1) + J_1(1) = -18.79 + (-7.13) = -25.92$ . This modulated signal spectrum is illustrated in figure 3.7-24. The data in figure 3.7-24 show that the 99% power bandwidth is 5.6 (4 times higher modulating frequency) and the -60 dBc bandwidth is 13.2 (8 times higher modulating frequency + 2 times lower modulating frequency). Figure 3.7-25 shows the effect of increasing the modulation index of the lower frequency to 2.4. The carrier amplitude has been decreased to  $J_0(2.4) + J_1(1) = -52.01 + (-2.32) = -54.33$  dBc. If any of the individual modulation indices produces a carrier null, the carrier will be nulled independent of the other modulation indexes. This may be very difficult to detect with many modulating signals because some of the sum and difference combinations will produce components at frequencies very close to the carrier frequency.

Reference 18 also derives an equation for calculating the RF spectrum for square wave modulation. The magnitude of the  $n^{\text{th}}$  sideband is:

$$\frac{2\beta \sin [(\beta - n)\pi/2]}{\pi (\beta^2 - n^2)}.$$

Therefore, the first carrier null for square wave modulation will occur at a modulation index ( $\beta$ ) of 2 ( $\sin (\pi) = 0$ ).

The -60 dBc bandwidth for this signal was 16.4 (8 times the lower frequency + 6 times the higher frequency). Figures 3.7-26 and 3.7-27 illustrate the spectra of a carrier modulated by three sine waves. Figure 3.7-26 shows that most of the power is in the carrier component for three sine waves each with a modulation index of 0.6. The spectrum in figure 3.7-27 is similar to figure 3.7-25 but with many more spectral components. The -60 dBc bandwidth is 13.42 for figure 3.7-26 and 18.42 for figure 3.7-27. In general, with several SCOs the -60 dBc bandwidth will almost always be less than eight times the highest frequency SCO if the modulation indices are less than one and less than six times the rms deviation if the modulation indices are greater than one.

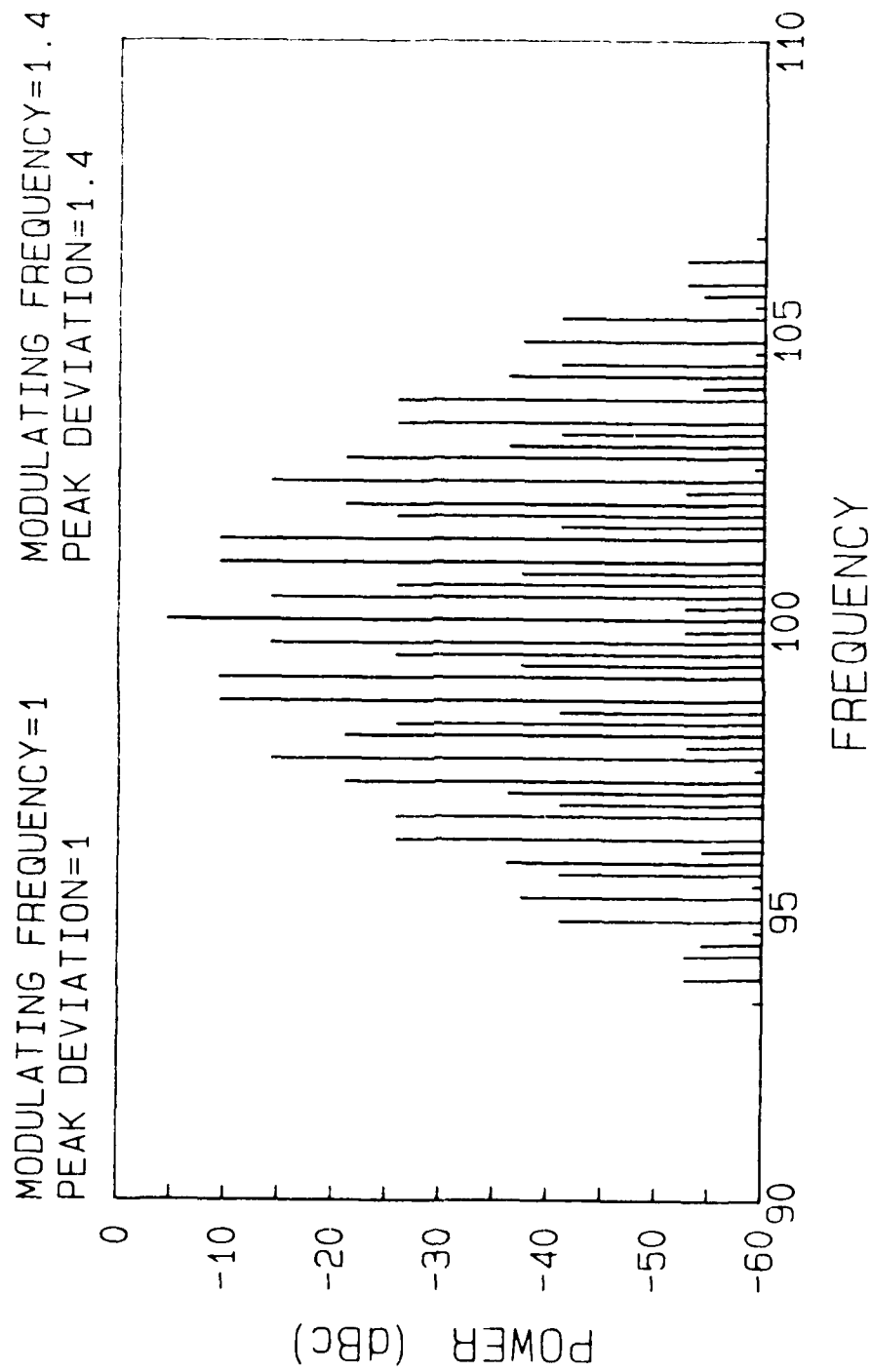


Figure 3.7-24. FM Spectrum with Two Sine Wave Modulation and  $MI=1$ .

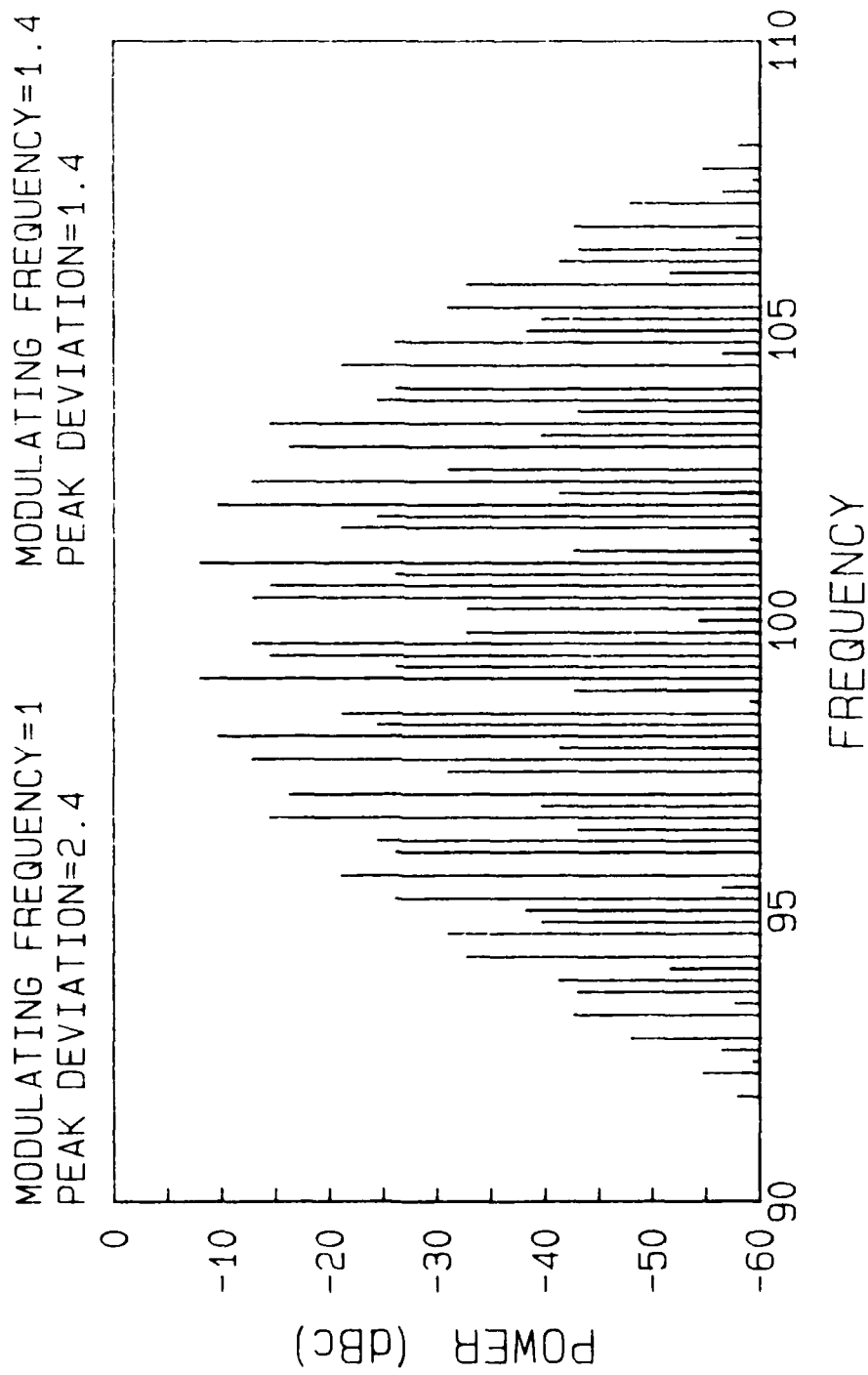


Figure 3.7-25. FM Spectrum with Two Sine Wave Modulation and MI=1 and MI=2.4.

MODULATION FREQUENCY=1    PEAK DEVIATION=0.6  
MODULATION FREQUENCY=1.4    PEAK DEVIATION=0.84  
MODULATION FREQUENCY=1.77    PEAK DEVIATION=1.06

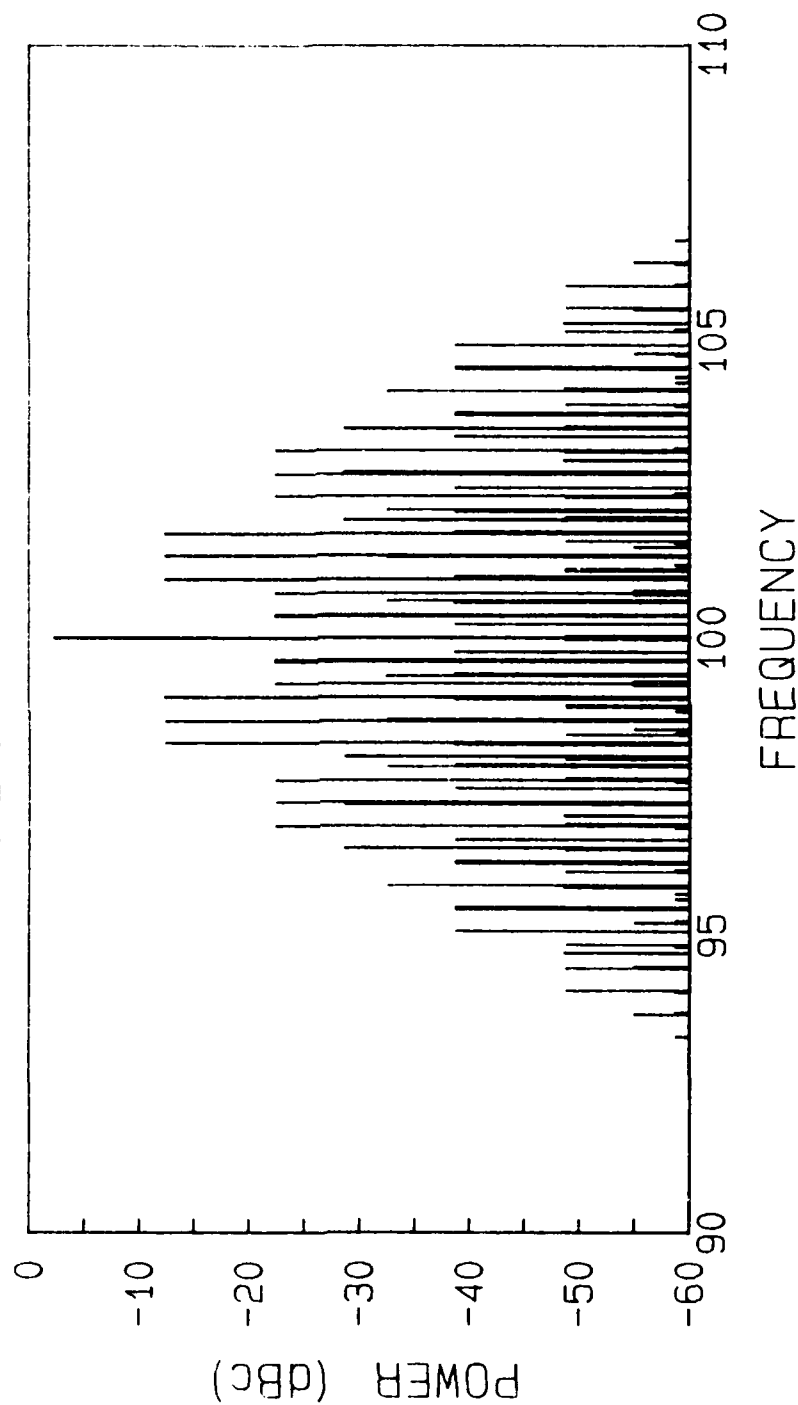


Figure 3.7-26. FM Spectrum with Three Sine Wave Modulation and MI=0.6.

MODULATION FREQUENCY=1 PEAK DEVIATION=2.4  
MODULATION FREQUENCY=1.4 PEAK DEVIATION=1.4  
MODULATION FREQUENCY=1.77 PEAK DEVIATION=1.77

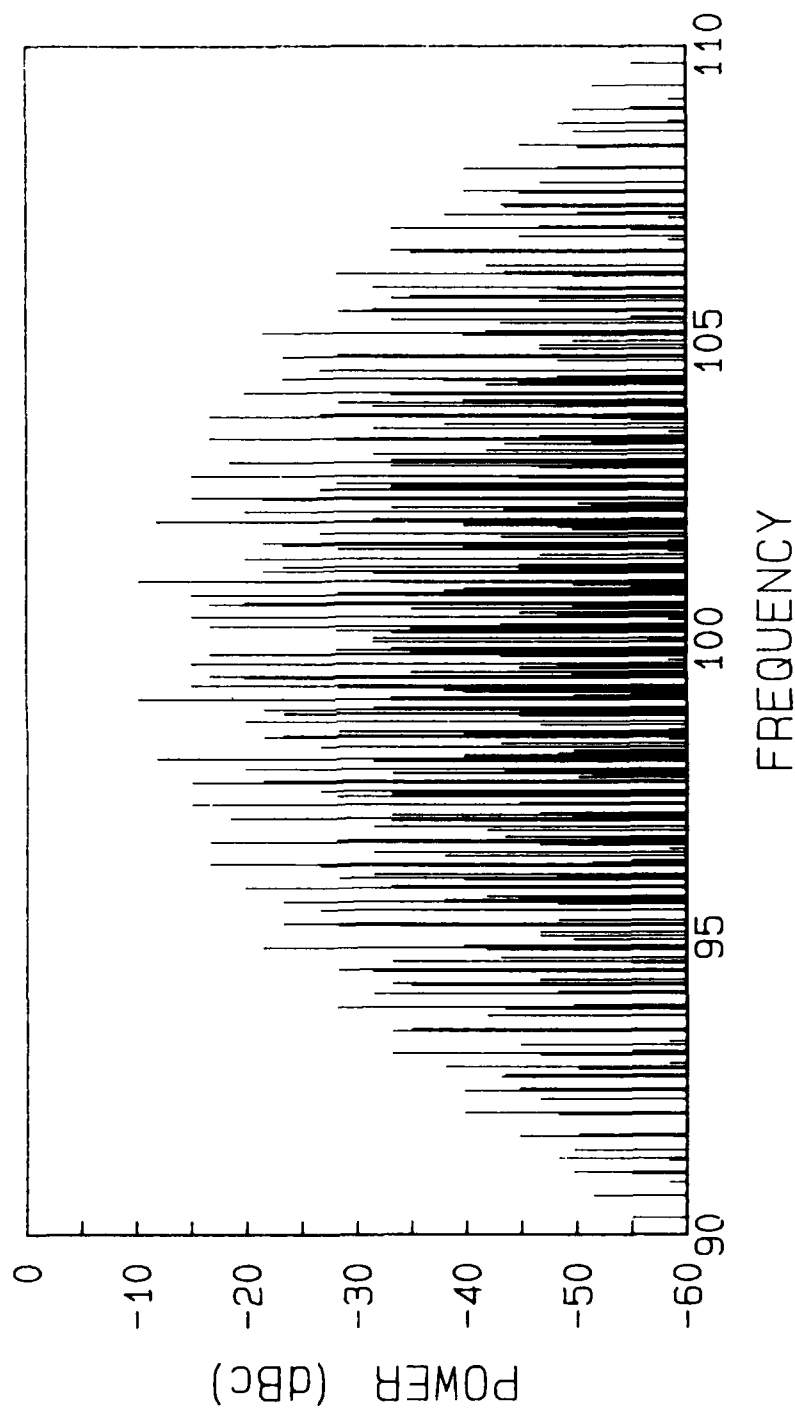


Figure 3.7-27. FM Spectrum with Three Sine Wave Modulation and  $MI=1$  and  $MI=2.4$ .

### 3.7.11 Noise Power Ratio

Noise loading tests have been used for many years to test various communications systems. This section will describe noise loading testing as related to an FM/FM telemetry link. One output of a noise loading test is the noise power ratio (NPR). NPR is the decibel ratio of the noise level at the output of the system under test at the measurement frequency with the baseband fully loaded to the level with all of the baseband noise loaded except for a narrow band around the measurement frequency.

A noise power ratio test uses a noise signal to simulate an FM/FM multiplex. Either white noise (constant power spectral density) or spectrally shaped noise can be used. The noise power ratio is measured as follows:

1. Measure the noise power in a narrow bandwidth (bandpass filter).
2. Insert a notch filter in the noise source which is somewhat wider than the bandpass filter in 1. Adjust the noise level to keep the source rms noise level constant. Measure the noise power at the output of the bandpass filter. The ratio of these two noise powers is the NPR.
3. Decrease the source noise amplitude to zero. Measure the noise power at the output of the bandpass filter. The ratio of the noise measured in 1 to the noise measured in 3 is called the noise power ratio floor NPRF or NPRO.

The use of NPR to predict FM/FM subcarrier SNR is described in references 19 and 20. These publications presented experimental NPR values and subcarrier discriminator SNRs and also derived equations to predict the subcarrier discriminator output SNR from the NPR. The agreement between theory and experiment was quite good. The basic equation used to estimate discriminator output SNR (power ratio) from NPR (when NPR = NPRF) was:

$$(S/N)_{LPF} = \{ 48 \Gamma (\Delta f)^3 (NPR - 1) \} / (f_c)^3.$$

<sup>19</sup>Law, E. L., E. T. Kimball, and M. H. Nichols, "Relationship of Noise Power Ratio to FM/FM Data Quality", in *Proceedings of the International Telemetry Conference, Vol. XII*, pp 234-250, 1976.

<sup>20</sup>Pacific Missile Test Center, *Relationship of Noise Power Ratio to Subcarrier Discriminator Signal-to-Noise Ratio*, by E. L. Law, E. T. Kimball, and M. H. Nichols, Point Mugu, CA, 1 Aug 1975, PMTC TP-75-21.



The expected noise power ratio due to FM demodulator noise (NPRF) can be calculated from the FM noise equations. Assume that a white noise modulation signal with a bandwidth  $B_n$  and rms deviation  $\Delta f_r$  is used. Therefore, the noise power in bandwidth  $b$  is  $(\Delta f_r)^2 b/B_n$ . Substituting this into the bandpass filter SNR equation we get:

$$\text{NPRF} = \frac{B_{IF} \text{SNR}_{IF} (\Delta f_r)^2 b/B_n}{f_o^2 b}$$

or

$$\text{NPRF} = \frac{B_{IF} \text{SNR}_{IF} (\Delta f_r)^2}{f_o^2 B_n}$$

where:

$\text{SNR}_{IF}$  = IF SNR (power ratio)

$\Delta f_r$  = RF rms deviation due to noise source

$f_o$  = noise measurement frequency

$$\text{NPRF (dB)} = \text{SNR}_{IF} \text{ (dB)} + 10 \log \left\{ \frac{B_{IF} (\Delta f_r)^2}{B_n f_o^2} \right\}.$$

If noise with a 6 dB/octave taper with a 3 dB point of  $f_c$  is used the noise spectrum is proportional to  $1 + (f/f_c)^2$ . The NPRF for this case can be shown to be:

$$\text{NPRF} = (K \text{SNR}_{IF} B_{IF}) / f_o^2$$

or

$$\text{NPRF (dB)} = \text{SNR}_{IF} \text{ (dB)} + 10 \log \{ (K B_{IF}) / f_o^2 \}$$

where:

$$K = \frac{(\Delta f_r)^2 \left( 1 + \frac{f_o^2}{f_c^2} \right)}{(f_{\max} - f_{\min}) + \frac{(f_{\max})^3 - (f_{\min})^3}{3 f_c^2}}$$

The measured noise power ratio also includes effects due to incidental FM and intermodulation distortion. However, at IF SNRs below 20 dB these effects are usually swamped out by the FM demodulator noise. This assumes that the receiver IF filter has nearly constant group delay over at least a bandwidth equal to 4 times the rms deviation.

Comparisons between measured NPRs and NPRs calculated using the equations presented in the first part of this subsection are shown in figures 3.7-28 through 3.7-33. White noise was used for the data in figures 3.7-28 and 3.7-29 while the noise was preemphasized at 6 dB/octave (23 kHz 3 dB point) for the data in figures 3.7-30 through 3.7-33. These figures show that the measured NPRs were almost always within 2 dB of the calculated values for IF SNRs above 10 dB. The exceptions were the NPRs at 14 kHz with a 500 kHz IF bandwidth (figure 3.7-30) and with a 1500 kHz IF bandwidth, 10.2 dB IF SNR, and 200 kHz rms deviation (figure 3.7-33). Therefore, the measured NPRs are in good agreement with the calculated NPRs when the rms deviation is less than approximately one-fifth of the IF bandwidth and the IF SNR is greater than 10 dB and less than 20 dB. The calculated and measured values of NPR also agree well at higher IF SNRs for the higher frequency notches.

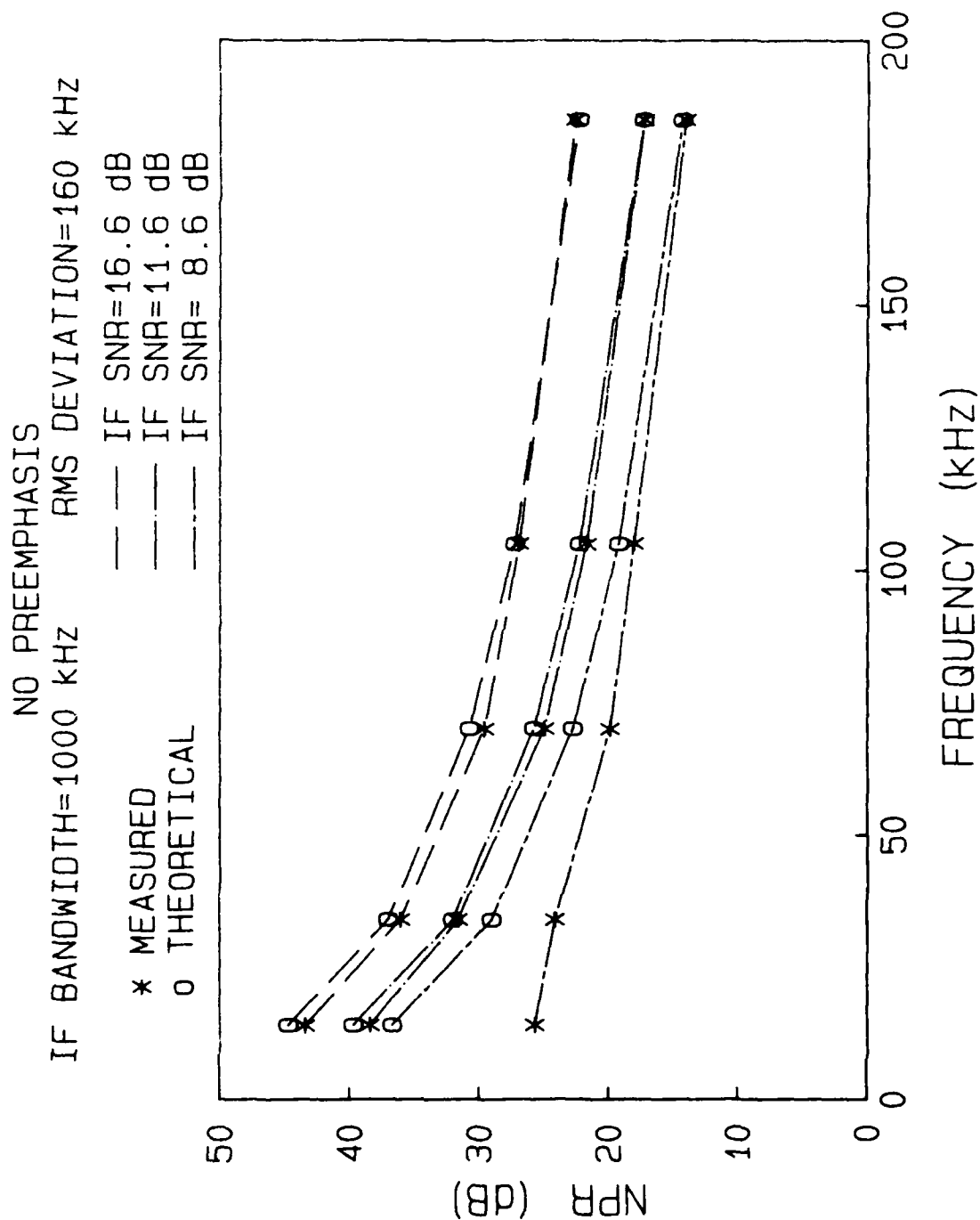


Figure 3.7-28. Measured and Theoretical NPRs (1000 kHz IF, 160 kHz Deviation).

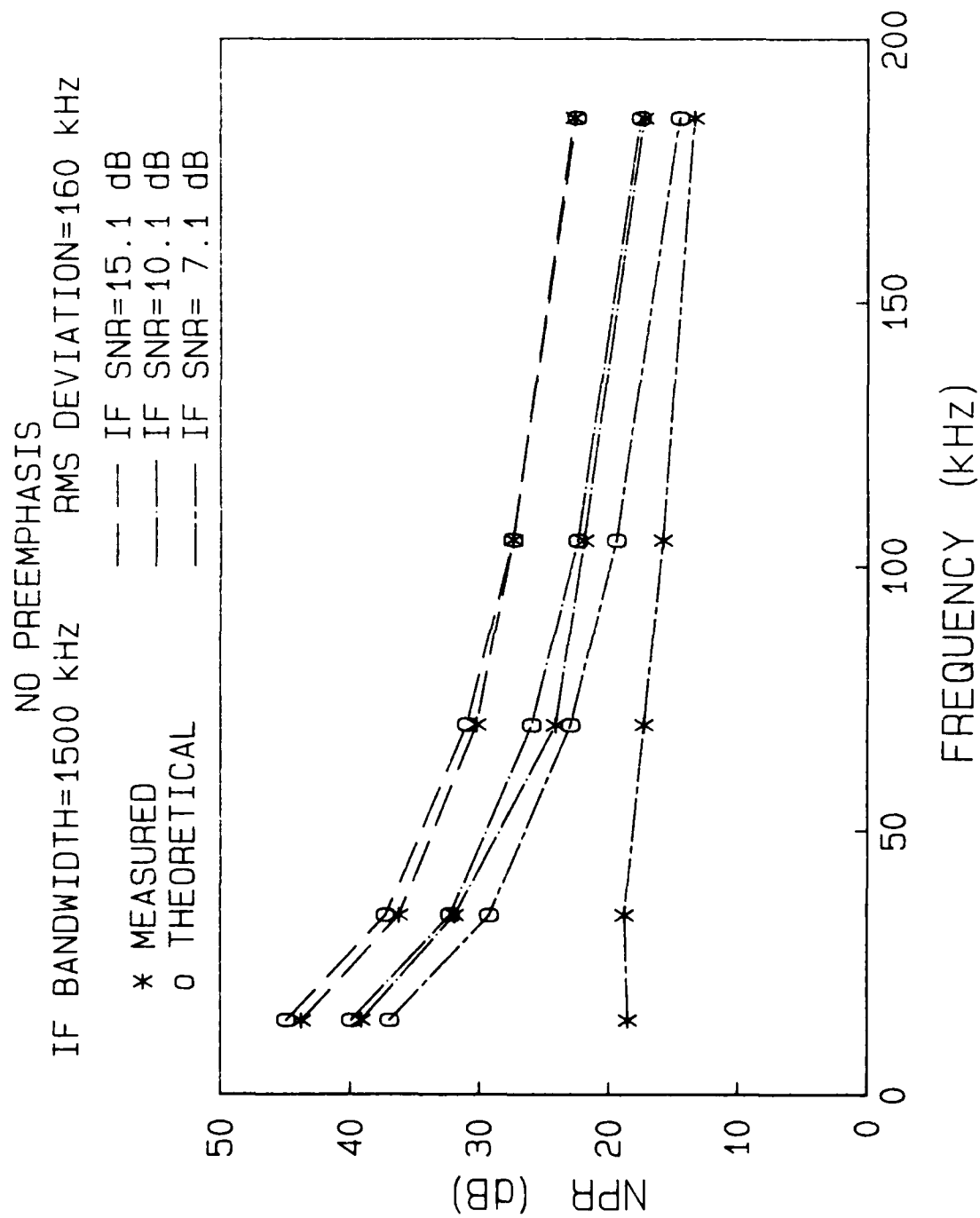


Figure 3.7-29. Measured and Theoretical NPRs (1500 kHz IF, 160 kHz Deviation).

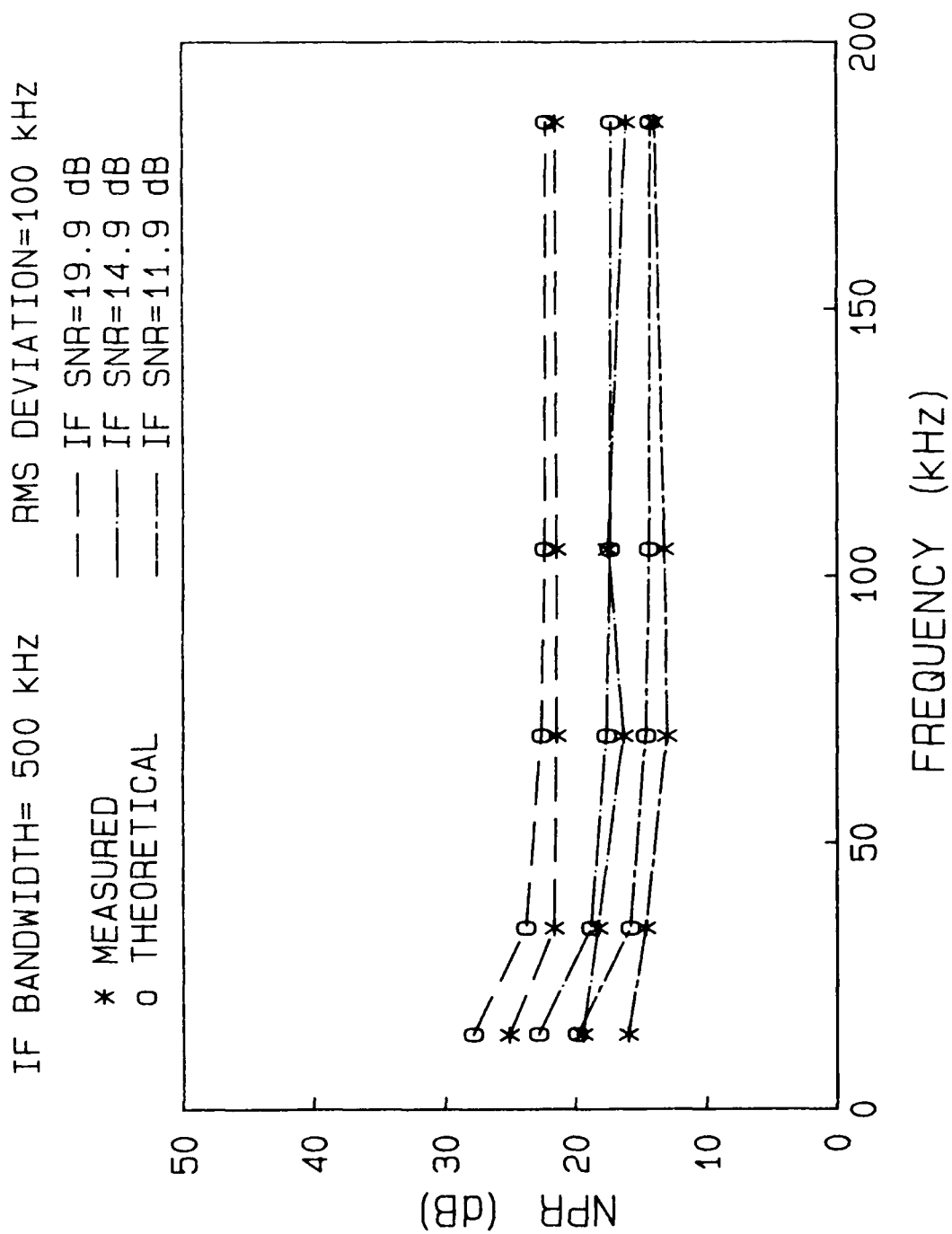


Figure 3.7-30. Measured and Theoretical NPRs (500 kHz IF, 100 kHz Deviation) .

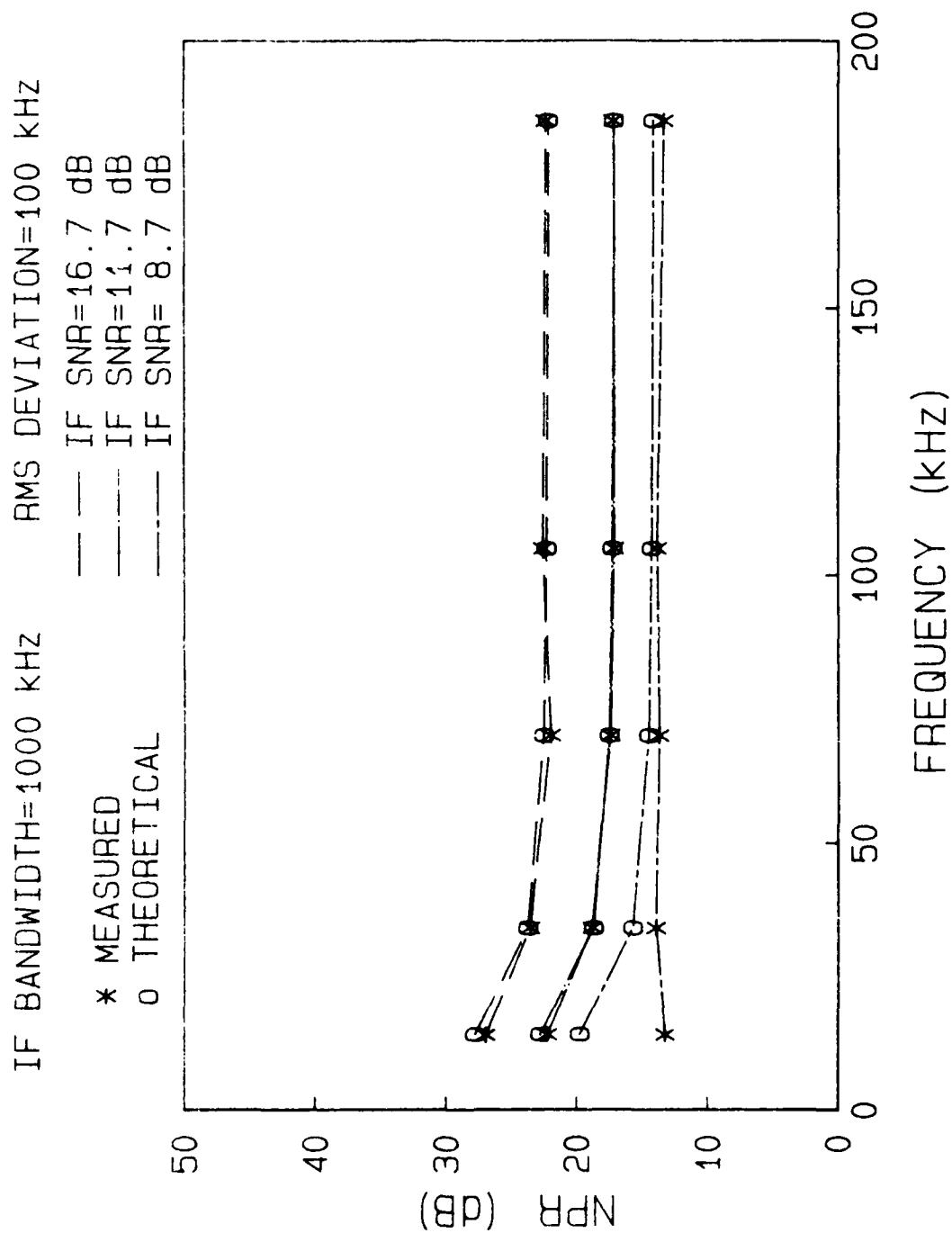


Figure 3.7-31. Measured and Theoretical NPRs (1000 kHz IF, 100 kHz Deviation).

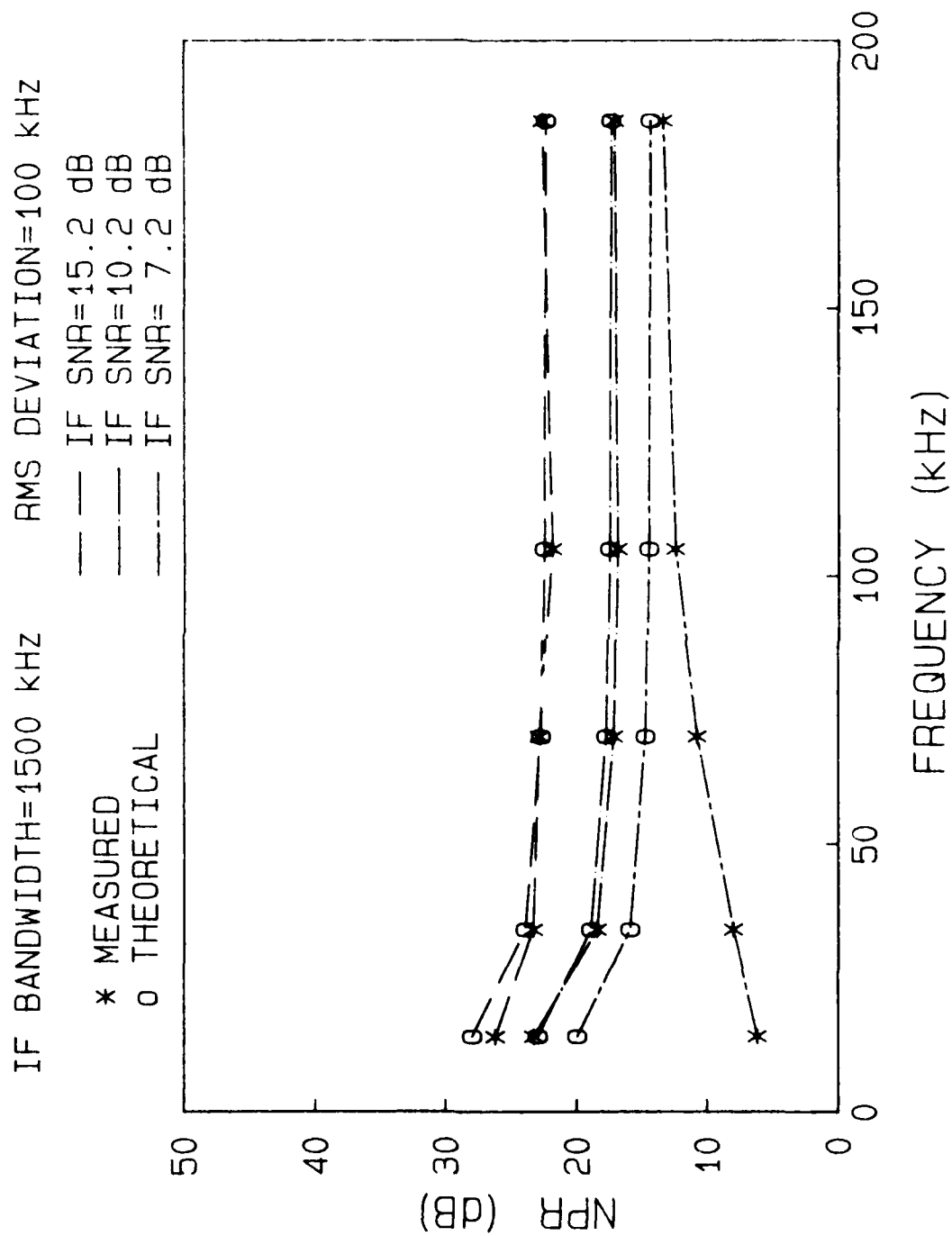


Figure 3.7-32. Measured and Theoretical NPRs (1500 kHz IF, 100 kHz Deviation).

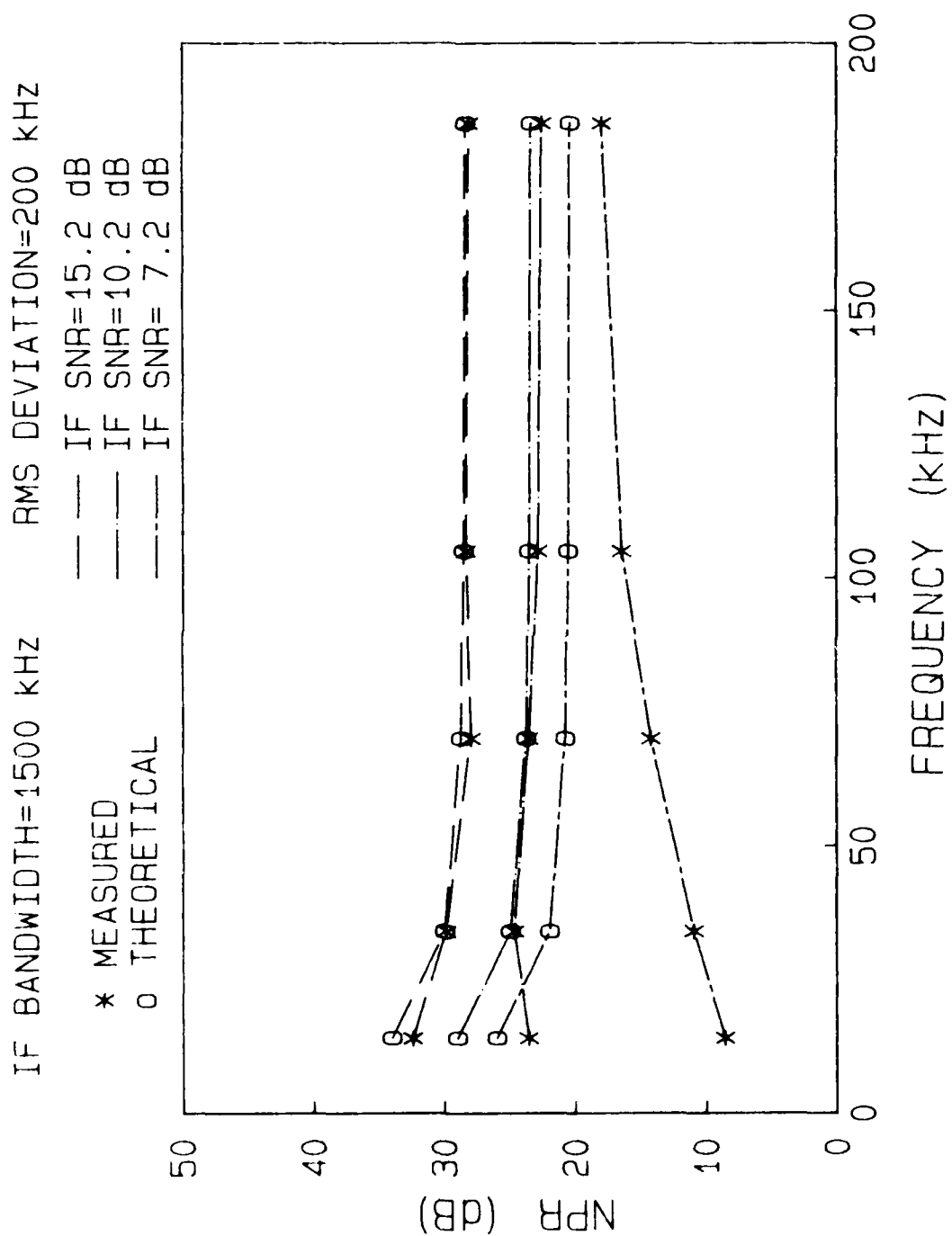


Figure 3.7-33. Measured and Theoretical NPRs (1500 kHz IF, 200 kHz Deviation).



### 3.8 HYBRID SYSTEMS

Hybrid systems are defined as systems in which more than one type of signal must be multiplexed together on the same transmitter. Hybrid systems can be designed and analyzed by using the information presented in subsections 3.1 through 3.7. An example of this is multiplexing subcarrier oscillators (SCOs) with a PAM or PCM signal on the same FM transmitter<sup>21</sup>. There are two ways of doing this:

1. The PAM or PCM signal can be put on the baseband with the SCOs at a higher frequency.
2. The SCOs can be at lower frequencies and the PAM or PCM signal can modulate another SCO.

An example of the first type of system would be a 256-kb/s randomized NRZ-L bit stream that needs to be transmitted along with two analog signals with 2 kHz of required bandwidth each. The baseband spectrum of such a system is shown in figure 3.8-1. The SCO frequencies ( $\pm 8$  kHz deviation) were chosen to be near the spectral null of the NRZ-L PCM signal. **CAUTION**, the PCM signal may have components at the bit rate if there are glitches at the clock rate, etc. Therefore, the use of a subcarrier that includes the bit rate within its channel bandwidth should be approached with **much** caution. The RF spectrum of this system is shown in figure 3.8-2. The IRIG -60 dBc bandwidth is approximately 1.5 MHz. Therefore, this signal will fit in an IRIG narrow band (1 MHz) channel.

The BER versus IF SNR in a 256-kHz bandwidth is shown in figure 3.8-3 for four IF bandwidths. It is interesting to note that the best PCM data quality is achieved with a 300-kHz IF bandwidth. This filter essentially rejects the two SCOs. The BER performance with all four filters is essentially what one would expect without the SCOs. This suggests that with this type of transmitted signal, one should use two receivers. A receiver with an IF bandwidth approximately equal to the bit rate to recover the PCM signal, and a receiver with a wider IF bandwidth to recover the SCO data. The output of the wider bandwidth receiver should also be predetection recorded to increase the probability of getting the best possible data quality. The SNR at the output of a 288-kHz discriminator with a 2-kHz linear phase output filter at a 34-dB IF SNR (1 MHz IF bandwidth) was 48 dB (full-scale sine wave rms/noise rms). The SNR was 35 dB at a 12.5-dB IF SNR. The SNRs at the output of a 256-kHz discriminator were 55 dB and 35 dB at IF SNRs of 34 dB and 12.5 dB, respectively. For comparison purposes, the IF SNR in a 256-kHz bandwidth required to achieve a  $10^{-5}$  BER with the 256-kb/s PCM signal modulating a 450-kHz SCO is approximately 19 dB (1.5 MHz IF bandwidth). The IRIG -60 dBc bandwidth would be approximately 3.5 MHz.

<sup>21</sup>Lantz, N. F., and M. H. Nichols. "Approximate Design Formulae and Procedures for Designing Hybrid Telemetry Systems Using an FM Carrier", in *Proceedings of the International Telemetry Conference*, Vol. XIII, pp 261-271, 1977.

256 kb/s NRZ-L PCM REFERENCE  
 PREMOD FILTER=200 kHz  
 256 kHz and 288 kHz SLOPE REFERENCE  
 RESOLUTION BW=3 kHz VIDEO BW=10 kHz

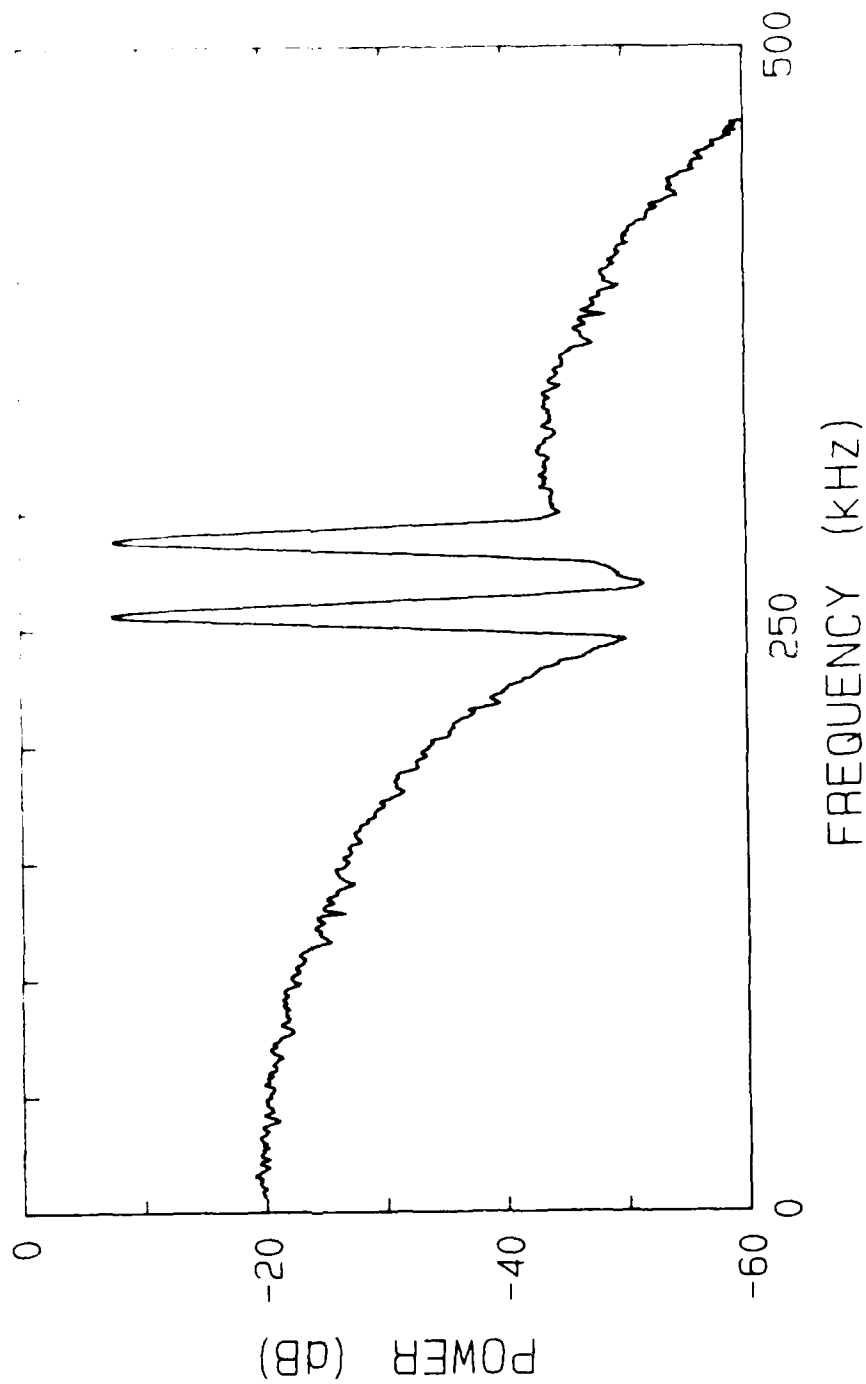


Figure 3.8-1. Baseband Spectrum 256 kb/s NRZ with 2 SCOs.

256 kb/s NRZ-L PCM/FM PEAK DEV=91 kHz  
PREMOD=200 kHz 5-POLE CD  
256 kHz and 288 kHz SCOs PEAK DEV=70 kHz  
RESOLUTION BW= 30 kHz VIDEO BW=100 Hz

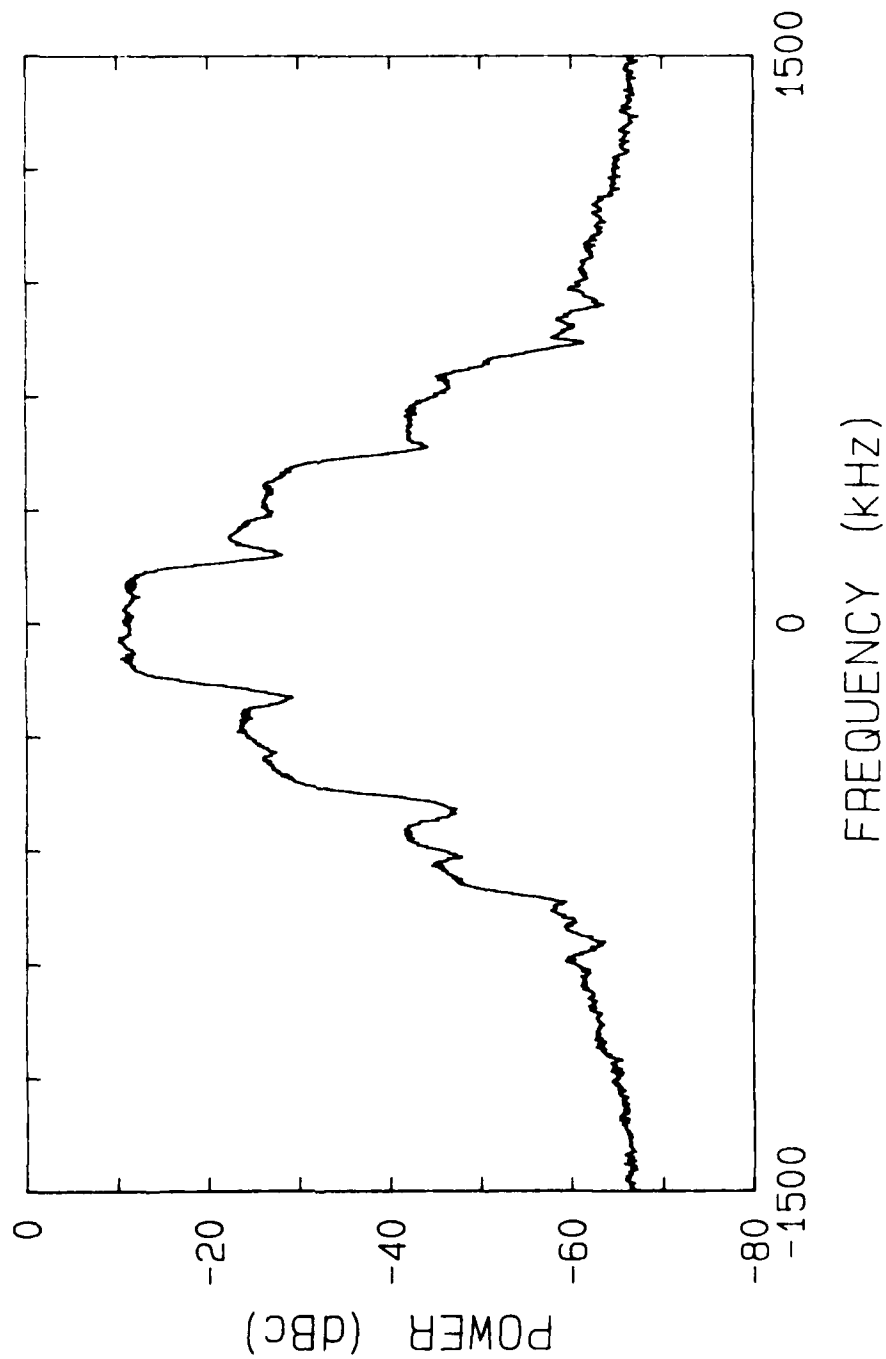


Figure 3.8-2. RF Spectrum 256 kb/s NRZ PCM/FM with 2 SCOs.

MODULATION TYPE	BIT RATE kb/s	IF BW kHz	PREMOD kHz	TYPE	PEAK DEV	BIT DET
0 NRZ-L PCM/FM	256	1500	200	CD	90	F/S
+ NRZ-L PCM/FM	256	1000	200	CD	90	F/S
o NRZ-L PCM/FM	256	500	200	CD	90	F/S
* NRZ-L PCM/FM	256	300	200	CD	90	F/S

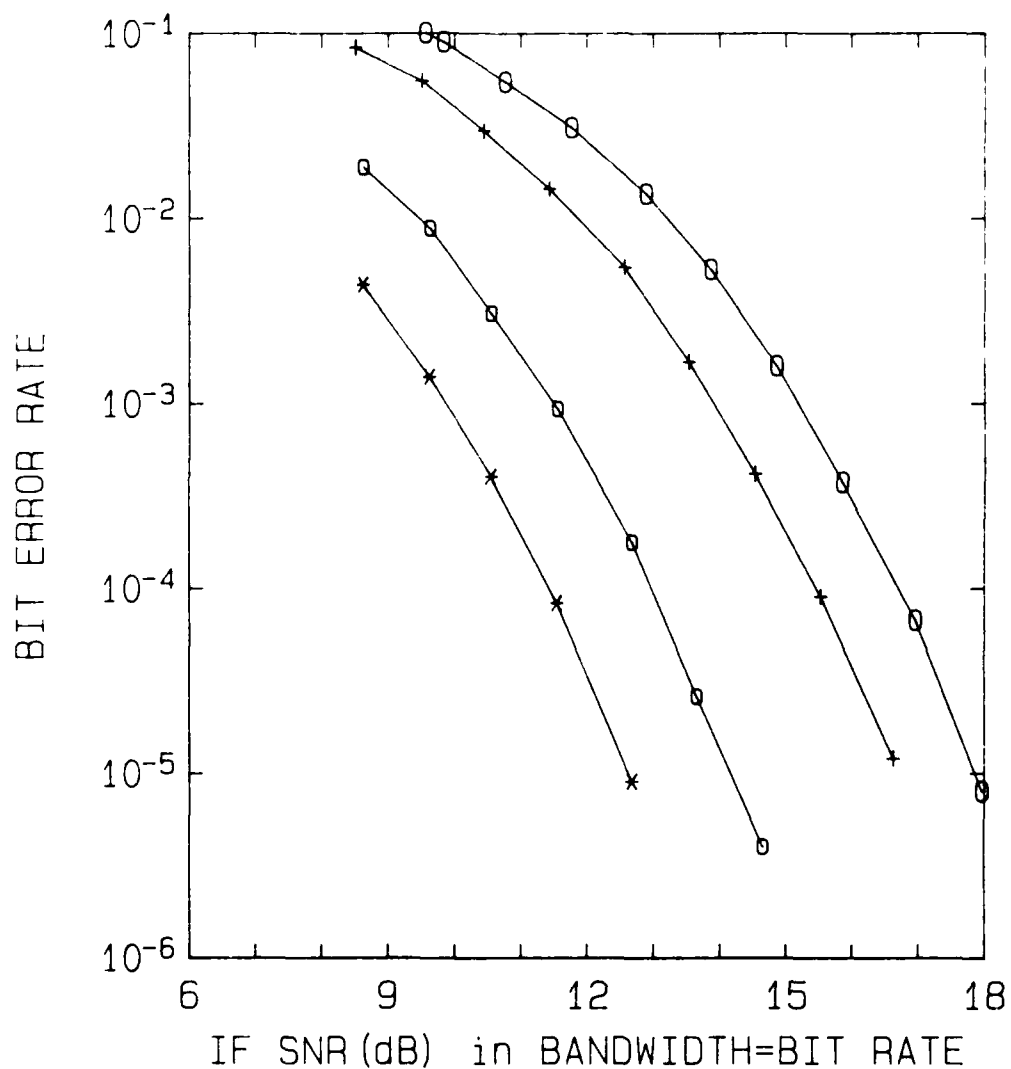


Figure 3.8-3. BER Versus IF BW for 256 kb/s NRZ PCM/FM and 2 SCOs.

### 3.9 LINK ANALYSIS

#### 3.9.1 Introduction

A typical telemetry link is shown in figure 3.9-1. The parameters that are important in predicting the expected performance of the link include:

1. Transmitter power
2. Cable loss between transmitter and antenna
3. Transmitting antenna gain. This is a function of direction and polarization and includes VSWR loss.
4. Communication channel losses. These losses include:
  - Free space propagation loss
  - Multipath
  - Ducting
  - Flame attenuation
  - Atmospheric attenuation (rain, fog, etc.)
5. Receiving antenna gain and noise temperature
6. Preamplifier gain and noise temperature
7. Telemetry receiver bandwidth and noise temperature
8. Modulation method and data type (FM, PM, PCM, PAM, FM/FM, etc.)
9. Data bandwidth.

**Radio Horizon** The equations presented in this section all assume that the transmitting and receiving antennas are within radio line-of-sight of each other. If one assumes the standard value of 4/3 for the ratio of effective earth radius to actual earth radius, the distance between the two antennas when they are at the radio horizon can be approximated by<sup>22</sup>:

$$D = 5280 ( (2h_T)^{1/2} + (2h_R)^{1/2} ) \text{ feet.}$$

where:

$h_T$  = height (feet) above mean local elevation (MLE) of transmitting antenna

$h_R$  = height (feet) above MLE of receiving antenna.

This is illustrated in figures 3.9-2 and 3.9-3.

<sup>22</sup>Reference Data for Radio Engineers, Howard W. Sams & Co., Inc., Indianapolis, IN, p 28-12, 1975.

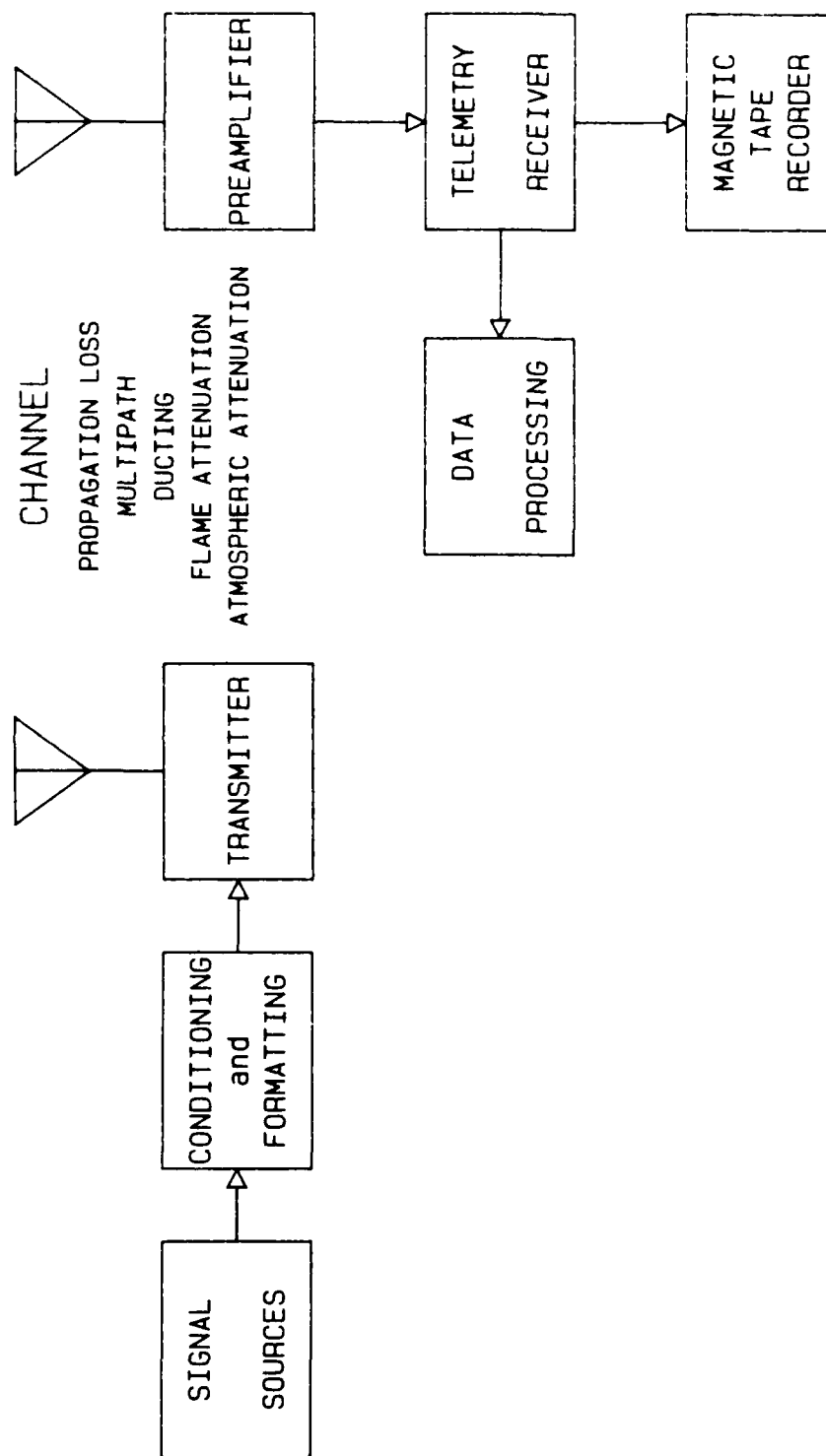


Figure 3.9-1. Block Diagram of Telemetry Link.

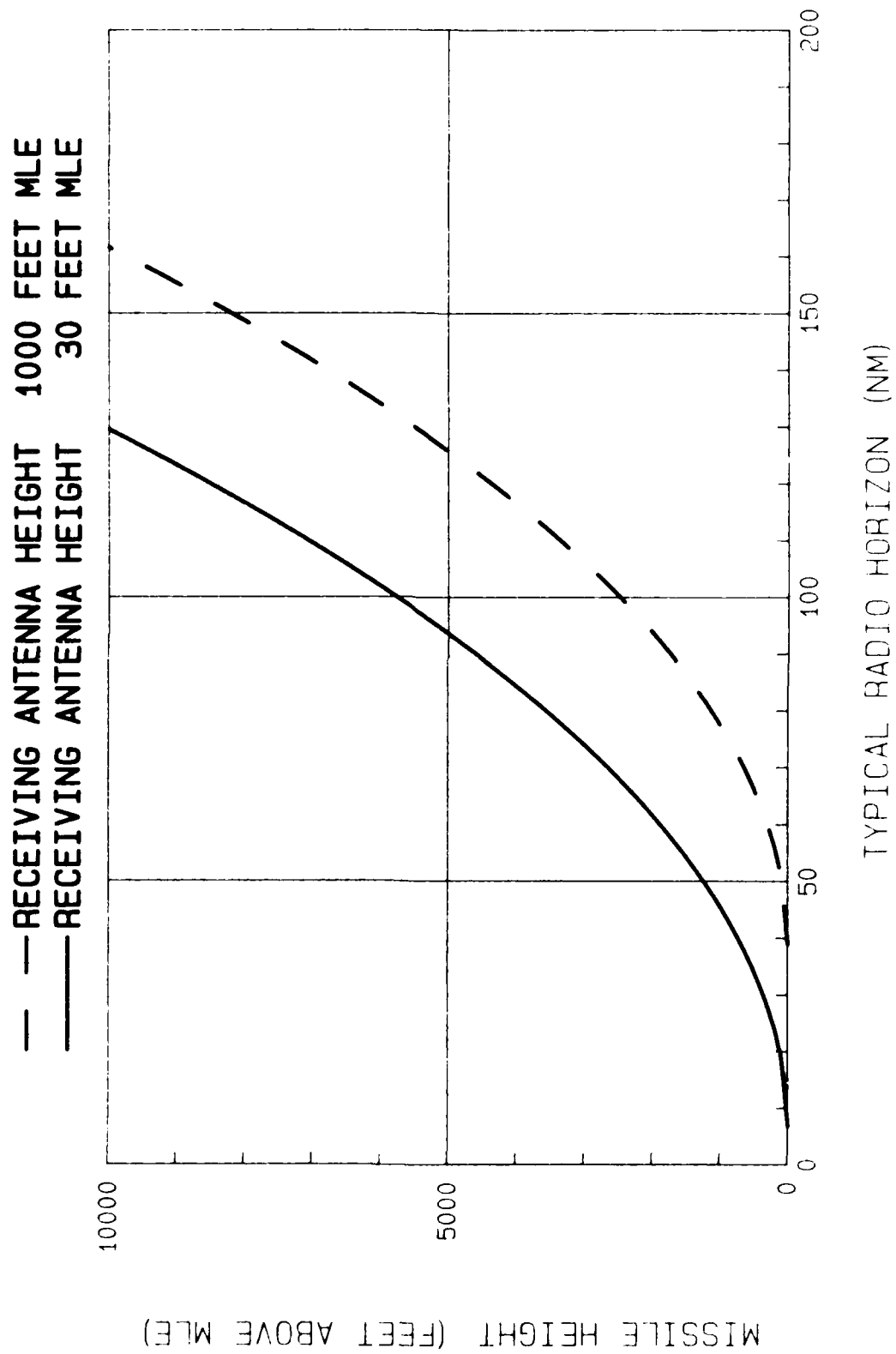


Figure 3.9-2. Typical Radio Horizon for Transmitter Less Than 10,000 Feet Above MLE.

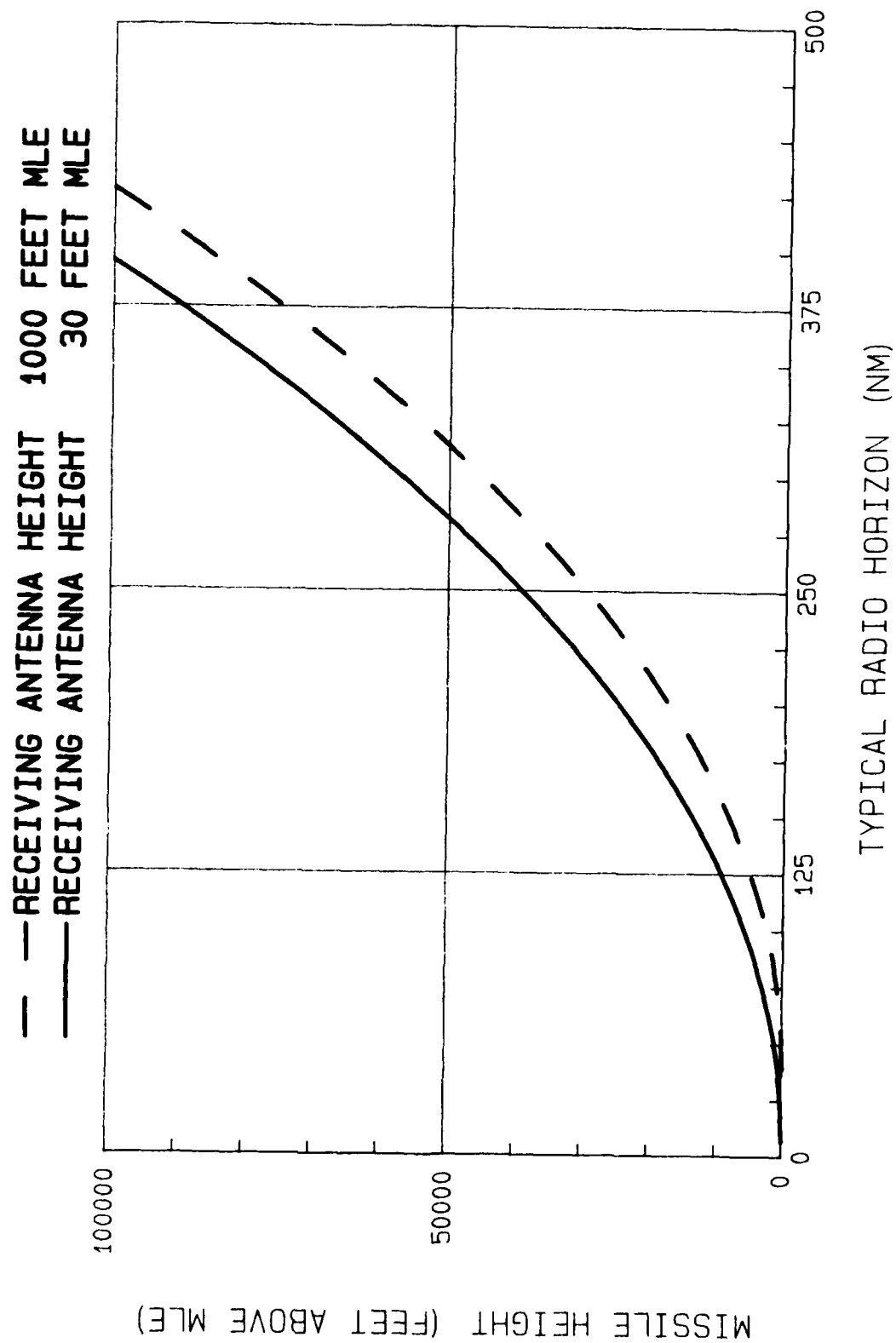


Figure 3.9-3. Typical Radio Horizon for Transmitter Less Than 100,000 Feet Above MLE.



### 3.9.2 Transmitting System

**Transmitter Power** The transmitter power is frequently determined by the available battery power. Most missile telemeters have transmitter powers between one and ten watts. The transmitter power is expressed in dBm in the equations in this section (1 watt = +30 dBm).

**Cable Loss** The loss of commonly used cables is typically 0.14 to 0.2 dB/foot at 2.25 GHz.

**Transmitting Antenna Gain** The transmitting antenna gain is usually expressed in dBi. Zero dBi is defined as the gain of a 100% efficient antenna which radiates power equally in all directions. The transmitting antenna gain is usually measured in an anechoic chamber. The gain is measured in all directions by rotating the transmitting antenna relative to the measurement antenna. The measurement antenna is usually a linear horn or a circularly polarized antenna. Measurements are commonly made for vertical and horizontal and/or left hand circular and right hand circular polarizations. The gain of typical missile telemetry antennas varies from +6 dBi to less than -40 dBi depending on the direction and polarization. Typical missile transmitting antenna gains (circular polarization) which are exceeded over a given percent of the sphere surrounding the missile are:

Coverage	Gain
90%	-12 dBi
95%	-16 dBi
99%	-22 dBi

This means that for a typical missile telemetry antenna 10% of the time the gain of left hand circular polarization is less than -12 dBi. These gains can be increased by typically 5, 7, and 9 dB at 90, 95, and 99 percent coverage respectively through the use of polarization diversity combining. Diversity signal combining is discussed in section 5.3. These values vary for different types of missiles and will also be different if only a part of the transmitting antenna pattern is used. For example, if missiles will always be fired away from a particular receiving site only the rear hemisphere is of interest. Missile transmitting antennas are typically linearly polarized and telemetry receiving antennas are typically circularly polarized. This tends to minimize the reception problems that occur with maneuvering missiles.

### 3.9.3 Communication Channel Losses

**Free Space Propagation Loss** The effective free space propagation loss can be calculated using:

$$L_p = 20 \log \left( \frac{4 \pi D}{\lambda} \right)$$

where:

$L_p$  is expressed in dB

$\lambda$  = wavelength =  $c/f$  = speed of light/transmitted frequency

$c = 3.00 \times 10^8$  meters/sec. or  $9.82 \times 10^8$  feet/sec.

$D$  = distance between transmitting and receiving antennas

$D$  and  $\lambda$  must be in the same units.

If  $f = 2250$  MHz and  $D = 1000$  meters then:

$$L_P = 20 \log \left\{ \frac{4 \pi 1000}{3 \times 10^8 / 2.25 \times 10^9} \right\} = 99.5 \text{ dB.}$$

If  $f = 2250$  MHz and  $D = 5280$  feet then  $L_P = 103.6$  dB.

A commonly used formula is:

$$L_P \text{ (dB)} = 36.6 + 20 \log f + 20 \log D$$

where  $f$  is expressed in MHz and  $D$  is expressed in statute miles.

**Multipath** Multipath occurs when the signal arrives at the receiving antenna by the direct path and also by one or more secondary paths (see chapter 28 of reference 22). Multipath losses can vary from a gain of 6 dB (-6 dB loss) or more if the signals add in-phase to a loss of 30 dB or more if the signals add out-of-phase. Multipath can be reduced by using a more directional antenna, by careful selection of mission profiles, and by use of diversity reception. Null steering antennas can also be used for multipath reduction but they are not available at telemetry receiving facilities at this time.

**Ducting** Ducting is a phenomena where an electromagnetic wave gets trapped between layers in the atmosphere which have a steep gradient in their index of refraction (see chapter 28 of reference 22). This can cause a signal which is beyond the radio horizon to be received clearly or conversely cause a nearby signal to be greatly attenuated. Ducting can be predicted from measurements of the index of refraction of the atmosphere. *Ducting loss is usually not included in link calculations.*

**Flame Attenuation** Flame attenuation occurs when the signal passes through the ionized gas cloud which many rocket boosters produce. The signal amplitude and phase are both modulated by passage through the ionized gas cloud. The modulation rates can be in the tens of kilohertz<sup>23</sup> and the attenuation can exceed 30 dB. The left and right hand circularly polarized components of the signal are not modulated identically by the passage through the ionized gas cloud. Therefore, a diversity combiner with wideband weighting signals can significantly improve the data quality during flame attenuation.

**Atmospheric Attenuation** Propagation through the atmosphere does not cause significant signal attenuation at frequencies between 1.4 and 2.3 GHz even during heavy rainstorms. An atmospheric attenuation of 1 dB is frequently assumed in these bands.

<sup>23</sup>Streich, R. G., D. E. Little, and R. B. Pickett, *Dynamic Requirements for Diversity Combiners*, in *Proceedings of the International Telemetry Conference*, Volume 8, pp. 635-642, October 1972.

### 3.9.4 Receiving System

**Receiving System Sensitivity** The receiving system sensitivity is usually characterized by measuring the ratio of antenna gain to receiving system noise temperature (G/T) (see section 5.0). This is expressed in decibels per degree Kelvin (dB/°K). The G/T of moderate size dishes (4 to 40 foot diameter) is usually measured by using the sun as a calibrated signal source. This method is described in RCC Document 118. Typical values of G/T for a modern receiving system with a 10 meter dish are 14 to 16 dB/°K at 1.5 GHz and 18 to 20 dB/°K at 2.25 GHz, when the antenna is pointed at least 5 degrees above the local horizon. The G/T is lower at lower elevations because the main lobe of the antenna starts to "see" the warm Earth in addition to the cold sky. This increases the system noise temperature.

The sensitivity of the receiving system can also be calculated by knowing the gain and noise figure of each element of the system (see section 5.2). The solar calibration method is preferred because the G/T can be measured in a few minutes any time the sun is above the local horizon. The measured G/T provides an excellent measure of the current "health" of the receiving system.

**Telemetry Receiver Bandwidth** The telemetry receiver bandwidth is needed to determine the total system noise power and also the IF SNR needed to achieve a desired data quality. The equivalent noise power bandwidth is usually within  $\pm 10\%$  of the quoted receiver IF bandwidth so the IF bandwidth can usually be used with an error of less than 0.5 dB. The total noise power is equal to  $kTB$  where:

$$\begin{aligned}k &= -198.6 \text{ dBm/}^\circ\text{K Hz (Boltzmann's constant)} \\T &= \text{system noise temperature (}^\circ\text{K)} \\B &= \text{equivalent noise power bandwidth (Hz).}\end{aligned}$$

However, we have included  $T$  in the  $G/T$  term so we will only use  $kB$  for the noise contribution.

**SNR for Desired Data Quality** The SNR required to achieve a given data quality is a function of the modulation method, data type, data bandwidth, and receiver bandwidth. This is discussed in sections 3.1 through 3.8 for various modulation methods. For example, if we need a BER of  $10^{-5}$  for 700 kb/s NRZ-L PCM/FM and the receiver bandwidth is 1000 kHz the required IF SNR is 12 dB in a 1000 kHz bandwidth. If you are unsure of what IF SNR is needed, 12 dB is usually a good estimate for most FM applications.

### 3.9.5 Link Margin Calculation

The predicted signal is equal to: transmitter power - cable loss + transmitting antenna gain - path loss - multipath loss - ducting loss - flame attenuation - atmospheric attenuation + receiving system antenna gain. The predicted noise is equal to Boltzmann's constant + receiving system temperature + receiver IF bandwidth (all quantities in dB). Combining the receiving system antenna gain and noise temperature into one term (G/T) we get the following equation for predicted SNR:

$$SNR_P = P_T - L_C + G_T - L_P - L_M - L_D - L_F - L_A + G/T - kB$$

where:

$SNR_P$  is the predicted IF SNR  
 $P_T$  is the transmitter output power in dBm  
 $L_C$  is the cable loss between the transmitter and the transmitting antenna  
 $G_T$  is the gain of the transmitting antenna in dBi  
 $L_P$  is the path loss in dB  
 $L_M$  is the estimated multipath loss in dB  
 $L_D$  is the estimated ducting loss in dB  
 $L_F$  is the estimated flame attenuation in dB  
 $L_A$  is the estimated atmospheric loss in dB  
 $G/T$  is the receiving system figure of merit in dBi per degree Kelvin  
 $kB$  is Boltzmann's constant times the equivalent noise power bandwidth

Link margin is defined as the excess SNR available in the link. It is calculated by subtracting the desired SNR from the predicted SNR. A sample calculation will be performed for a system with the following parameters:

Transmitter frequency	2250.5 MHz
Transmitter power	2 watts
Data type	NRZ-L PCM/FM
Bit rate	700 kb/s
Cable loss between transmitter and antenna	1 dB
Required probability of "good" data	95%
Desired data quality	$10^{-5}$ BER
Receiving system G/T	18 dB/°K
Receiving system IF bandwidth	1000 kHz
Maximum range	100 statute miles
Antenna elevation angle	2 degrees

Other assumptions:

Multipath loss	3 dB
Flame attenuation	10 dB single polarization 7 dB diversity combined
Atmospheric attenuation	1 dB
Ducting loss	0 dB

This gives us the following values:

P <sub>T</sub>	+33 dBm (2 watts)
L <sub>C</sub>	1 dB
G <sub>T</sub>	-16 dBi (LHC only)
	-9 dBi (LHC +RHC)
L <sub>p</sub>	143.6 dB
L <sub>M</sub>	3 dB
L <sub>D</sub>	0 dB
L <sub>F</sub>	10 dB (LHC only)
	7 dB (LHC + RHC)
L <sub>A</sub>	1 dB
G/T	17 dB/°K (1 dB loss for 2 degree elevation angle)
kB	-138.6 dB/°K (1000 kHz bandwidth)
SNR	12 dB (IF SNR for 10 <sup>-5</sup> BER with 700 kb/s NRZ-L PCM/FM and 1000 kHz IF bandwidth).

Margin = SNR<sub>p</sub> - SNR

LHC Margin = +33 -1 -16 -143.6 -3 -0 -10 -1 +17 +138.6 -12 = 2 dB

(LHC + RHC) Margin = +33 -1 -9 -143.6 -3 -0 -7 -1 +17 +138.6 -12 = 12 dB

### 3.10 RELAY SYSTEMS

#### 3.10.1 Introduction

There are several types of relay systems. These include both analog and digital point-to-point microwave links, relay aircraft and airborne relay pods that receive signals that may be over the horizon from the telemetry ground station, fiber optic and RF cable systems, etc.

Microwave links are frequently used to send data from the receiving site to the real-time data processing site. Both analog and digital microwave links are used. The analog links use either the received predetection or video signals for the modulation link inputs. Most analog microwave links multiplex several telemetry signals on one microwave link. Also, most analog microwave links have fairly limited bandwidth. This presents a problem with wideband signals. Coordination is required between the range user and the microwave link personnel to determine if there are potential bandwidth problems with the user's telemetry system. Most digital microwave links use intelligent asynchronous multiplexer/demultiplexers. This allows several asynchronous digital telemetry signals to be multiplexed together and sent over one microwave link. The signals are demultiplexed at the receiving end of the microwave link.

There are three major methods used in telemetry relay systems:

1. Frequency translation of the original signal
2. Demodulation of the original signal followed by modulation of a new carrier
3. Demodulation and reconstruction of the original signal followed by modulation of a new carrier.

An example of the first method would be to mix the final IF output of a telemetry receiver with a local oscillator to produce a new signal at the desired frequency. This method preserves the deviation and frequency response characteristics of the original transmitted signal if the bandwidths of the receiver and translation system are wide enough. The signal-to-noise effects of this method are discussed later in this subsection.

An example of the second method would be to use the demodulated video output of a telemetry receiver to modulate a second transmitter. This method preserves the characteristics of the original transmitted signal only if the demodulator sensitivity and the transmitter sensitivity are the same and the bandwidths are wide enough to pass the signal without attenuation. The signal and noise effects are discussed later in this subsection.

An example of the third method would be to follow the receiver video output with a bit synchronizer. The bit synchronizer output would modulate the second transmitter. The deviation is now determined by the combination of the bit synchronizer output amplitude, the gain of any filter section between the bit synchronizer output and the transmitter, and the deviation sensitivity of the transmitter. The system bit error rate (BER) is the sum of the BERs in links 1 and 2. Any error extension would apply equally to the errors generated in any link affected by the encoder/decoder causing the error extension.

### 3.10.2 Translation Relay SNR Calculation

The SNR in a given bandwidth at the output of a system which consists of an originating transmitter, a receiver, a translation of the receiver IF to a second RF frequency and transmission of the resulting signal, and a final receiver (see figure 3.10-1) is calculated in this section.

Assume that the signal (the units of S and N are power) at

IF<sub>1</sub> can be represented by:  $S_1 + N_1$

and the signal at IF<sub>2</sub> can be represented by:  $A (S_1 + C (N_1)) + N_2$

where:

$S_1$  is the signal power at the IF output of receiver #1

$N_1$  is the noise power at the IF output of receiver #1

$N_2$  is the noise power at the IF output of receiver #2 due to the downlink only

$C = B_{IF2} / B_{IF1}$  except C is never greater than 1

A is the net gain between the IF output of receiver #1 and the IF output of receiver #2.

$B_{IF1}$  is the equivalent noise power bandwidth of receiver #1 (uplink receiver)

$B_{IF2}$  is the equivalent noise power bandwidth of receiver #2 (downlink receiver)

The IF SNR of just the downlink is:  $A (S_1) / (N_2)$ .

The IF SNR of the entire link is then:

$$\frac{A (S_1)}{A (C (N_1)) + N_2} = \frac{(SNR_1) \times (SNR_2)}{(SNR_1) + C (SNR_2)}$$

Therefore, the predicted IF SNR of the entire link can be calculated from the predicted IF SNRs of the uplink and the downlink and the ratio of the IF bandwidths of the receivers.

If  $C = 1$  and the IF SNRs of both the uplink and the downlink are 20 dB then:

$$SNR_1 = 100 \quad \text{and} \quad SNR_2 = 100$$

$$\text{System IF SNR} = \frac{100 \times 100}{100 + 100} = 50 \quad \text{or} \quad 17 \text{ dB.}$$

If  $C = 0.5$   $SNR_1 = 10$  and  $SNR_2 = 100$  then:

$$\text{System IF SNR} = \frac{10 \times 100}{10 + 100/2} = 16.67 \quad \text{or} \quad 12.2 \text{ dB.}$$

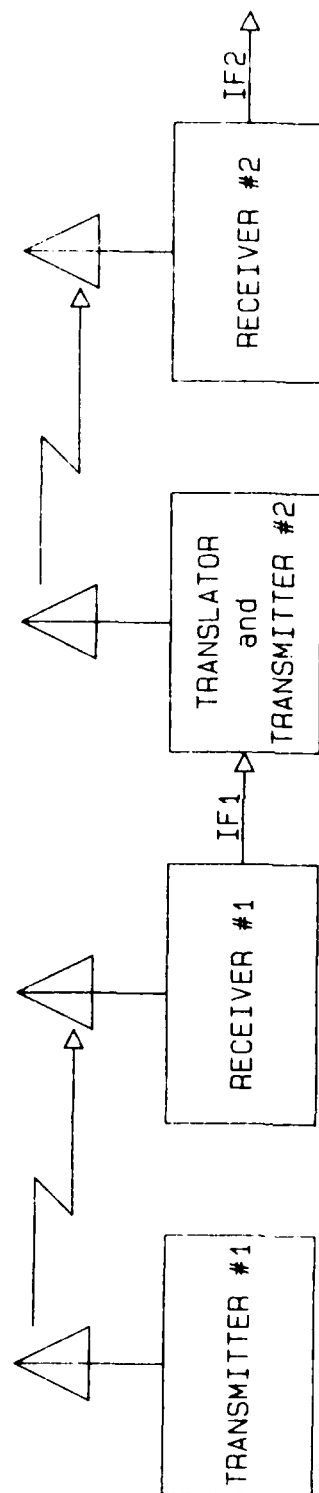


Figure 3.10-1. Block Diagram of Translation Relay Link.



### 3.10.3 FM Demodulation/Remodulation Relay SNR Calculation

The video SNR at the output of an FM system which consists of an originating transmitter, a receiver, a second transmitter, and a second receiver (see figure 3.10-2) is calculated in this section. The analysis presented here assumes that both links are above FM threshold. The method is valid below FM threshold but the equations for signal and noise are not. This means that these equations should not be used if the IF SNR of either link is below 12 dB. The actual system video SNR will be worse than predicted by these equations if the IF SNR of either link is below 12 dB.

$$\text{Signal at video 1: } S_{V1} = (K_1 \Delta f_1)^2 / 2$$

$$\text{Noise at video 1: } N_{V1} = (K_1 f)^2 / (\text{SNR}_{IF1} B_{IF1})$$

Where:

$S_{V1}$  is the signal power at the input to transmitter 2

$N_{V1}$  is the noise power at the input to transmitter 2

$K_1$  is the demodulator sensitivity (V/kHz) of demodulator 1

$\Delta f$  is the peak deviation of transmitter 1

$f$  indicates the video frequency

$\text{SNR}_{IF}$  is the IF SNR expressed as a power ratio

$B_{IF}$  is the receiver equivalent noise power bandwidth

Assume:

$K_2$  is the modulation sensitivity (V/kHz) of transmitter 2

$K_3$  is the demodulator sensitivity (V/kHz) of demodulator 2

$$\text{The signal at video 2 is then: } S_{V2} = (K_3 / K_2)^2 S_{V1}$$

$$\text{Noise at video 2: } N_{V2} = (K_3 / K_2)^2 N_{V1} + (K_3 f)^2 / (\text{SNR}_{IF2} B_{IF2})$$

$$\text{System video SNR} = S_{V2} / N_{V2}$$

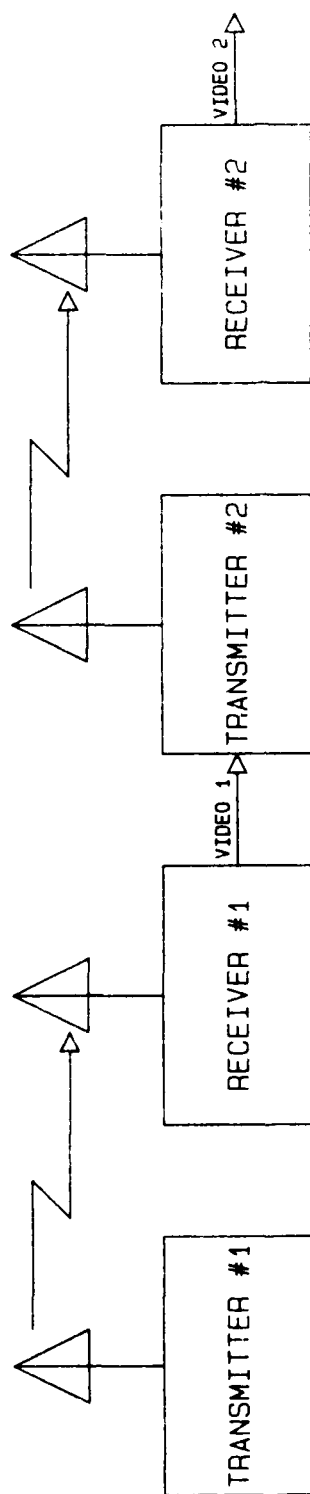
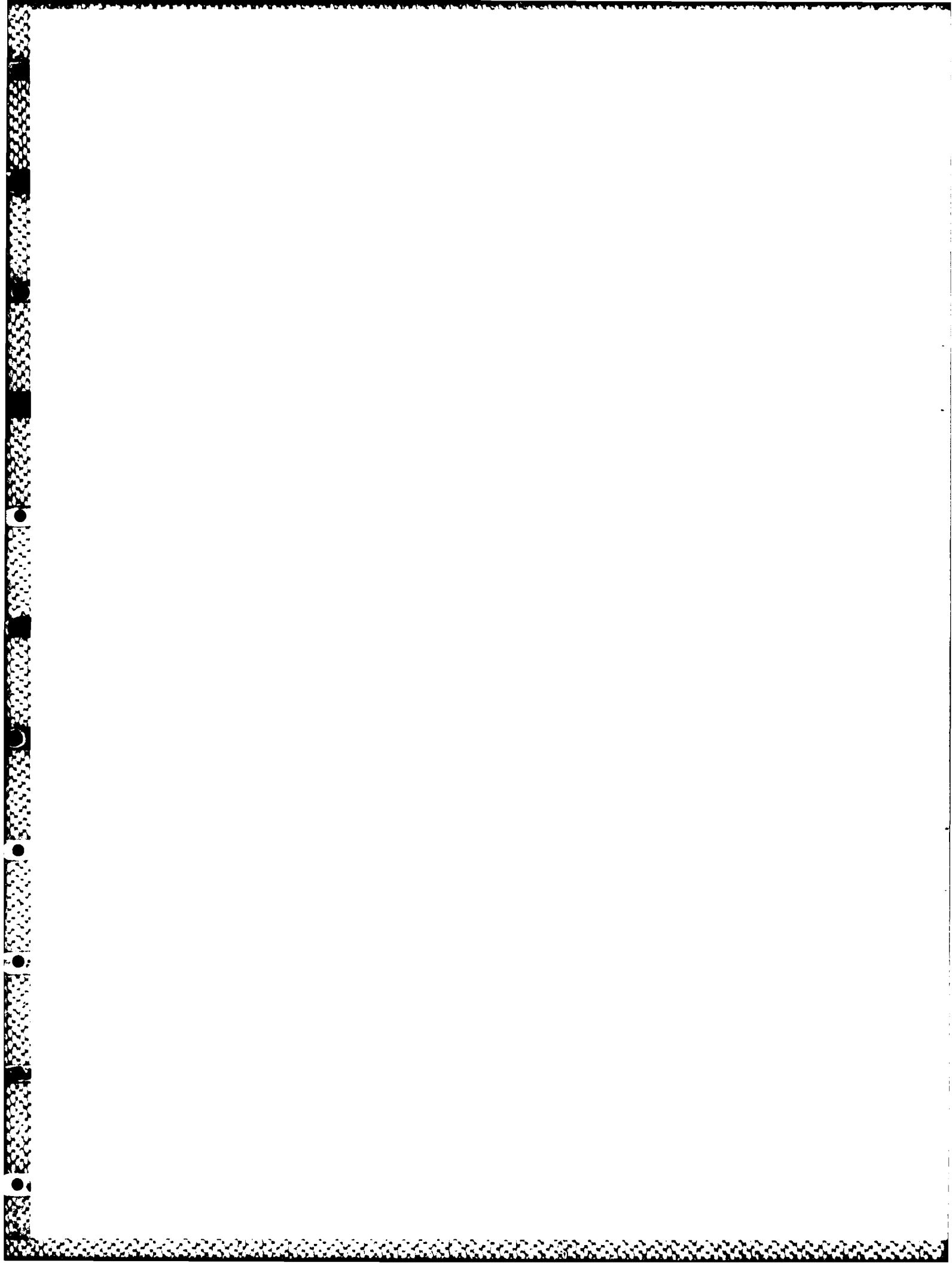


Figure 3.10-2. Block Diagram of Demodulation/Remodulation Relay Link.



### 3.11 FREQUENCY MODULATION NOISE CHARACTERISTICS

The two major types of noise signals present at the output of a frequency modulation (FM) demodulator are commonly called fluctuation noise and pop or click noise.<sup>24,25,26</sup> Fluctuation noise is defined as the error in the demodulated output caused by a noise vector being summed with the signal vector where the instantaneous noise amplitude is smaller than the signal amplitude. Pop noise is defined as the error in the demodulated output which occurs when the instantaneous vector sum of the signal plus noise encircles the origin (the noise amplitude has to be equal to or greater than the signal amplitude for this to occur).

A vector diagram illustrating fluctuation noise is presented in figure 3.11-1. The amplitude of the noise is 20% of the amplitude of the signal in figure 3.11-1. This limits the time rate of change of the angle  $\phi$  which is the FM demodulator output error signal (the signal vector is assumed to be stationary and the noise vector rotates with respect to the signal vector in this model). If we further assume that the instantaneous frequency of the noise is 400 kHz lower than the signal frequency, we can plot the vector sum and the demodulator error as a function of time. Figure 3.11-2 presents the sum of a signal with amplitude of 1 at a frequency of 10 MHz, and noise with an amplitude of 0.2 with a frequency of 9.6 MHz. The dots show the signal with no noise. The initial and final vector relationship is as shown in figure 3.11-1. Figure 3.11-3 shows the demodulator error signal for these conditions. In the real-world, the amplitude, phase, and frequency of the noise are random variables. The largest error is slightly larger than +100 kHz and occurs when the vectors are antiparallel. The mean value of the error is zero. Fluctuation noise dominates at high IF signal-to-noise ratios (SNRs), that is above approximately 12 dB.

Fluctuation noise is characterized as having a Gaussian amplitude distribution and a power spectrum proportional to:

$$f^2 N_0(f) / (A_c)^2$$

where:

$f$  = frequency of the noise

$N_0(f)$  = noise power spectral density at input to demodulator

$A_c$  = amplitude of the signal.

<sup>24</sup>Crosby, M. G. "Frequency Modulation Noise Characteristics". *Proc. IRE*, 25, 472-514 (1937).

<sup>25</sup>Stumpers, F. L. H. M. "Theory of Frequency-Modulation Noise". *Proc. IRE*, 36, 1081-1092 (1948).

<sup>26</sup>Rice, S. O. "Noise in FM Receivers". *Time Series Analysis*, ed. M. Rosenblatt, pp. 395-422 (Wiley 1963).

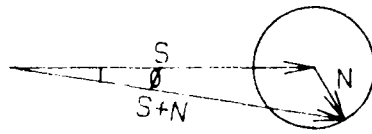


Figure 3.11-1. Fluctuation Noise Vector Diagram for  $N=0.2S$ .

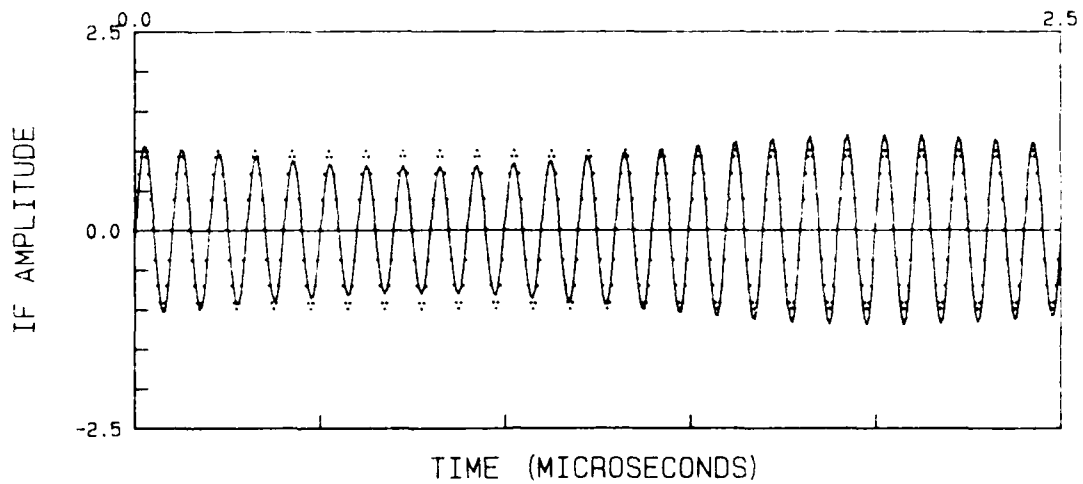


Figure 3.11-2. IF Amplitude ( $N=0.2S$ ).

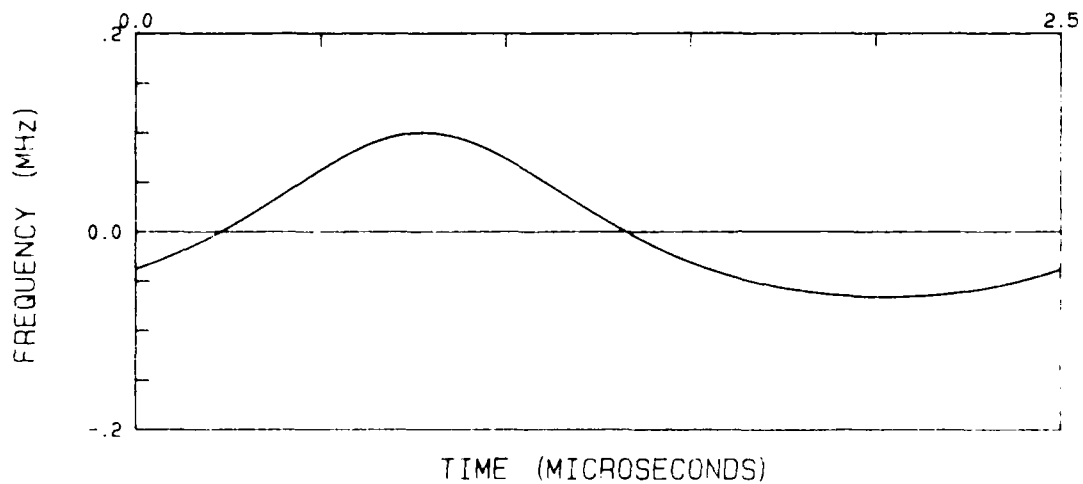


Figure 3.11-3. Demodulator Output for  $N=0.2S$ .

Therefore, the fluctuation noise at the output of the demodulator increases at 6 dB per octave when  $N_0(f)$  is constant, assuming no video filter. The frequency response characteristic of the IF filter is the main factor which determines  $N_0(f)$ . Examples of typical IF filter bandpass characteristics are shown in figures 3.11-4, 3.11-5 and 3.11-6. A time domain plot of fluctuation noise is shown in figure 3.11-7 and a spectral plot is shown in figure 3.11-8.

Pop noise occurs when the instantaneous vector sum of the signal plus noise encircles the origin causing a rapid change of  $2\pi$  radians in the angle  $\phi(t)$ . This is illustrated in figure 3.11-9. The signal amplitude in figure 3.11-9 is 1 while the instantaneous noise amplitude is 1.1. If we define the signal frequency to be 10 MHz and the instantaneous noise frequency to be 9.6 MHz, we can generate a time record of the IF amplitude for one cycle of  $\phi$ . This is shown in figure 3.11-10. Note that almost a full cycle of the 10-MHz signal (represented by dots) occurs between zero crossings of the vector sum of the signal plus noise when the amplitude of the signal plus noise is at a minimum. This causes the large pulse shown in figure 3.11-11. The energy contained in the center of the spike (0.34 microsecond duration) is  $\pi$  radians or 1/2 cycle. The signals shown in 3.11-10 and 3.11-11 do not include any effects due to IF bandpass filtering or video filtering. The effect of these filters would be to slow down the time rate of change of the demodulated output and reduce the total energy. Figures 3.11-12 and 3.11-13 show an actual noise "pop" and the corresponding linear IF signal. The test conditions included a 1-MHz IF bandwidth and 500 kHz/volt demodulator sensitivity for both figures. The video bandwidth was 1 MHz for figure 3.11-12 and 500 kHz for figure 3.11-13. The sudden change in  $\phi(t)$  causes a narrow pulse with an area of approximately  $2\pi$  radians to be generated. This is the same amount of energy that would be contained in an unfiltered PCM/FM bit with a peak deviation equal to the bit rate. The noise pops are usually in the direction to cause bit errors in PCM/FM. The reason is that the average frequency of the noise is usually near the center frequency of the IF filter. Therefore, when the carrier is deviated to a frequency which is higher than the center frequency, the instantaneous noise frequency will usually be lower than the signal frequency. This causes the pops to be in the direction towards the center frequency. This is illustrated in figures 3.11-14 and 3.11-15. Therefore, each pop will usually cause a bit error for PCM/FM with a peak deviation less than the bit rate. Figure 3.11-16 shows a noise pop that is in the direction away from the center frequency. The noise can also capture the demodulator for a long enough time to cause multiple cycles of  $\phi(t)$ . This is especially likely when the carrier is deviated away from the center frequency. This causes a noise pop with area approximately equal to the number of cycles of  $\phi(t)$ . The FM demodulator output with a center frequency input was 0 volts DC and the demodulator sensitivity was 625 kHz/volt for figures 3.11-13 through 3.11-19.

Figures 3.11-17 and 3.11-18 show the differences that occur in pop amplitude. The variation in pop amplitude is further illustrated by the superposition of several pops in figures 3.11-19 and 3.11-20. The test conditions for figure 3.11-19 were: IF SNR = 10 dB, IF bandwidth = 1 MHz, video bandwidth = 500 kHz, and RF input frequency = center frequency - 250 kHz. The amplitude of the pops varies greatly. The test conditions for figures 3.11-20 and 3.11-21 were: IF SNR = 10 dB, IF bandwidth = 10 MHz, video bandwidth = 6 MHz, demodulator sensitivity = 4 MHz/volt, and RF input frequency = center frequency. The area of all non-doublet pops was approximately 1 cycle under these conditions. Doublet pops are shown in figures 3.11-21 and 3.11-22. Doublets occur when the noise does not capture the demodulator for a long enough time to complete a  $2\pi$  swing of  $\phi(t)$ . Doublets have an area of approximately 0.

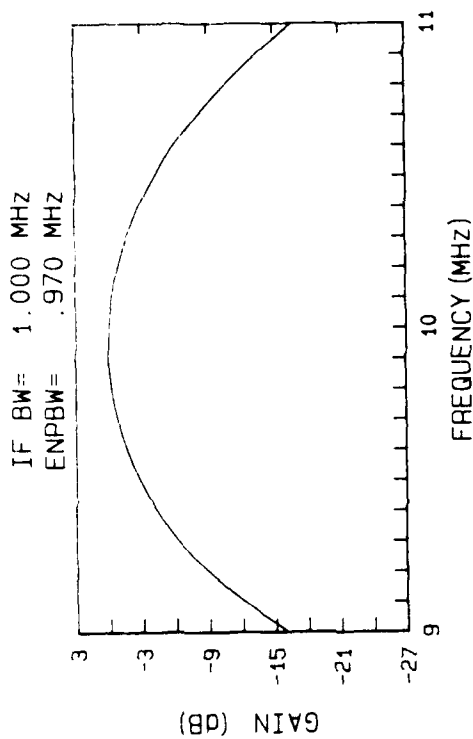


Figure 3.11-5. IF Filter Frequency Response (Filter B).

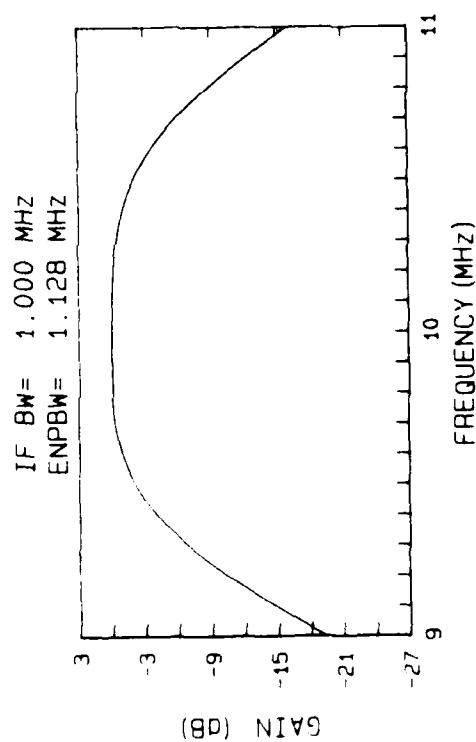


Figure 3.11-4. IF Filter Frequency Response (Filter A).

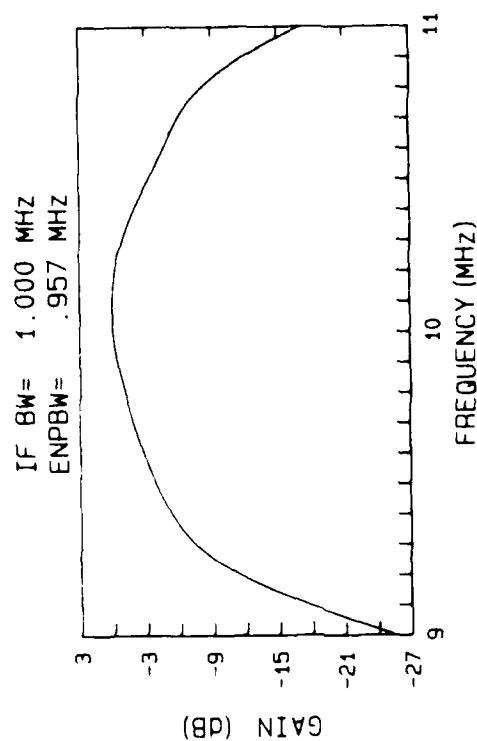
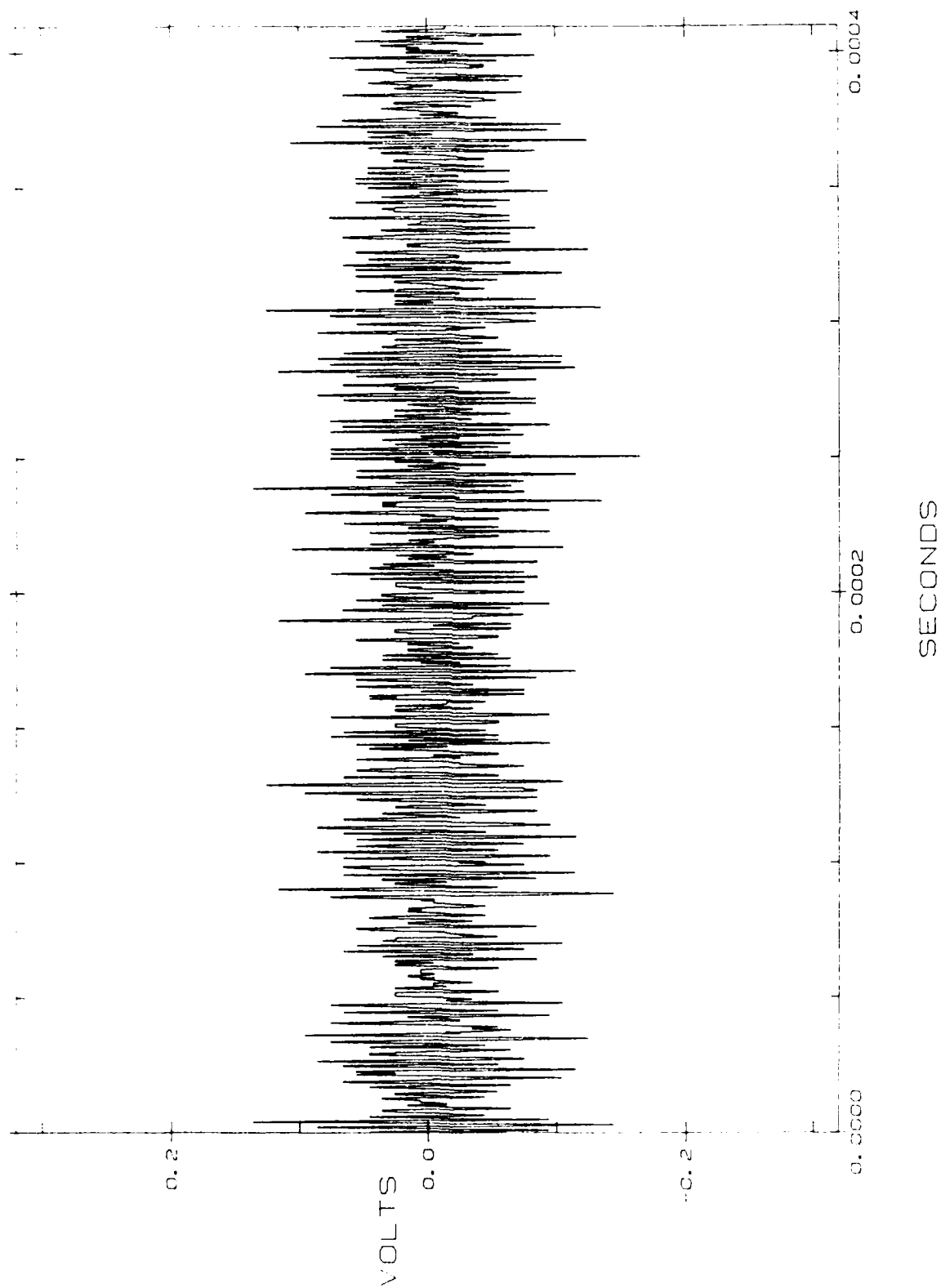


Figure 3.11-6. IF Filter Frequency Response (Filter C).



3.11- 5

Figure 3.11-7. Fluctuation Noise.



RECEIVER FM DEMODULATOR OUTPUT  
1000 kHz IF BW 500 kHz VIDEO BW

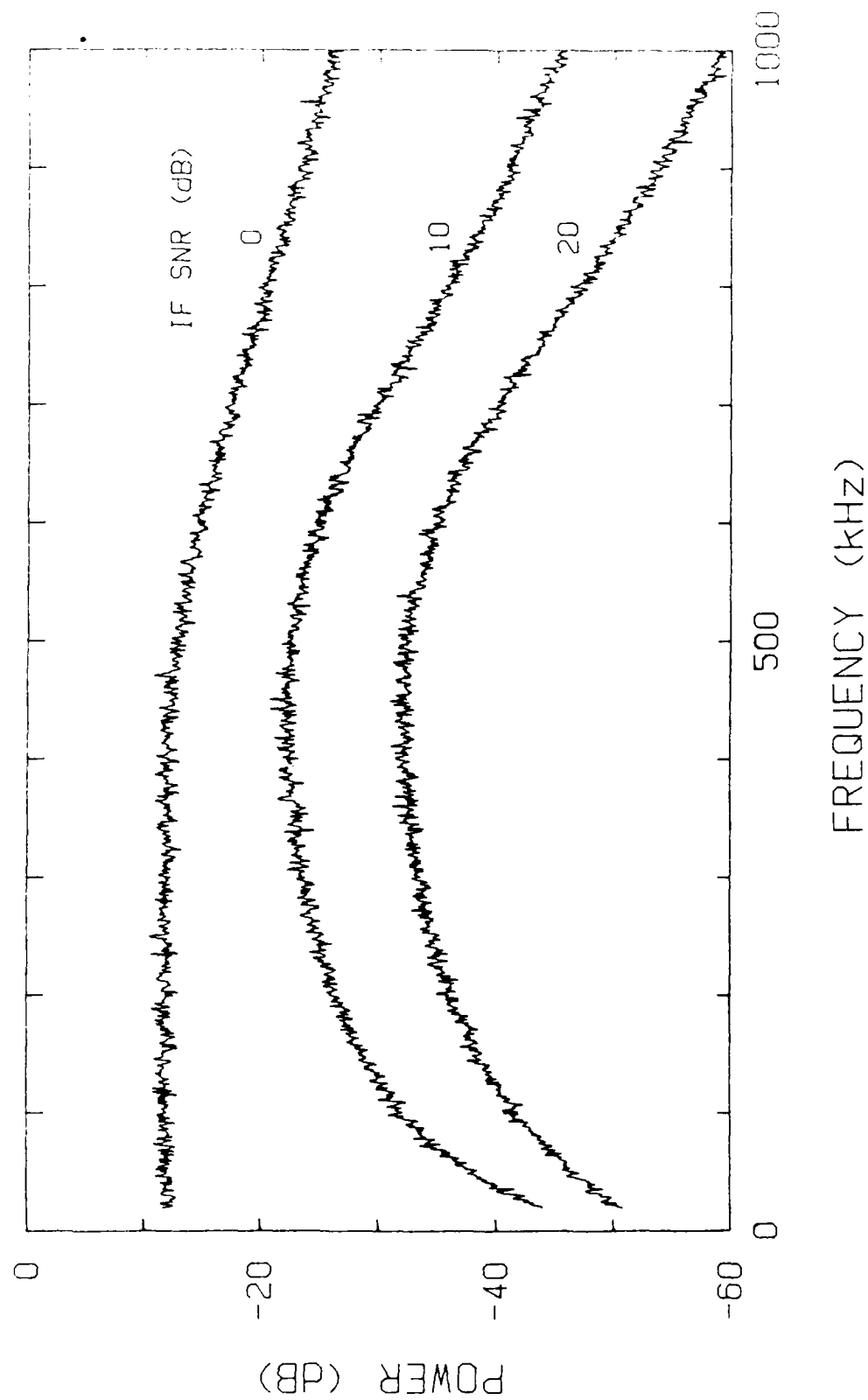


Figure 3.11-8. Receiver Video Noise Power Spectral Density.

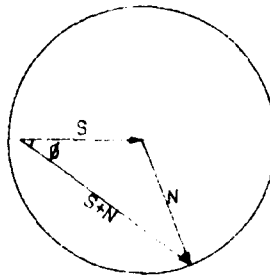


Figure 3.11-9. Vector Diagram of Pop Noise ( $N=1.1^\circ$ ).

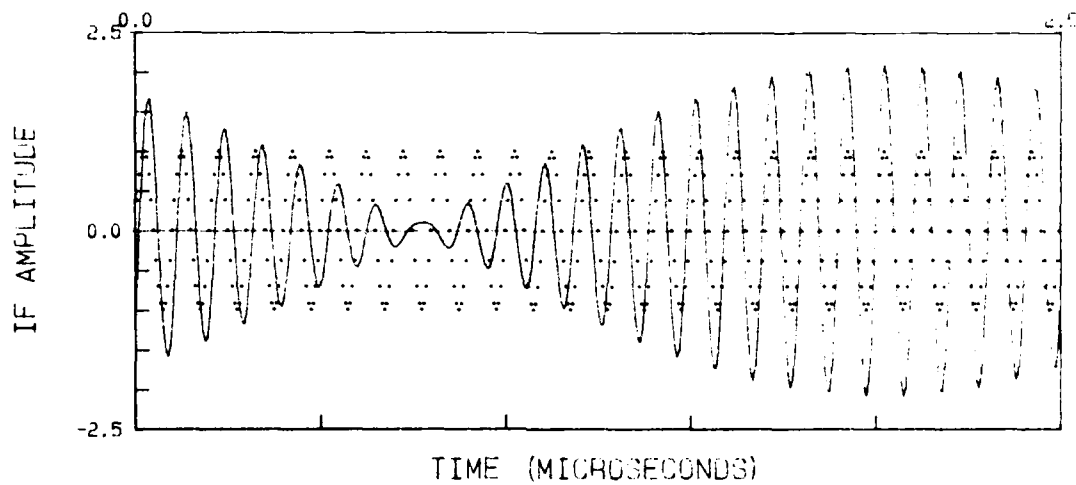


Figure 3.11-10. IF Amplitude ( $N=1.13^\circ$ ).

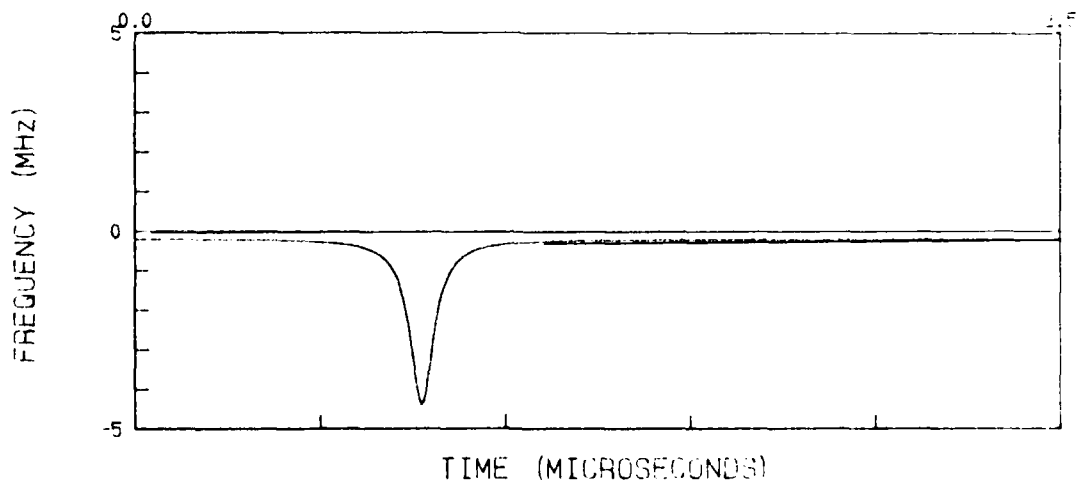


Figure 3.11-11. Demodulator Output ( $N=1.13^\circ$ ).

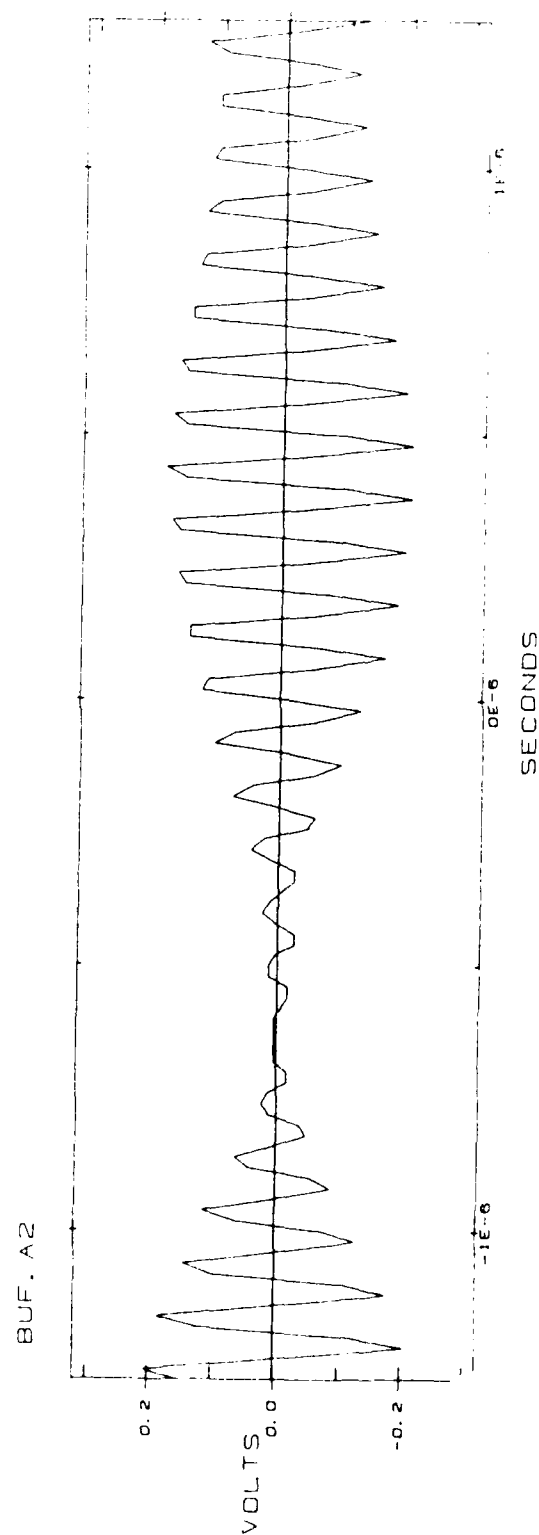
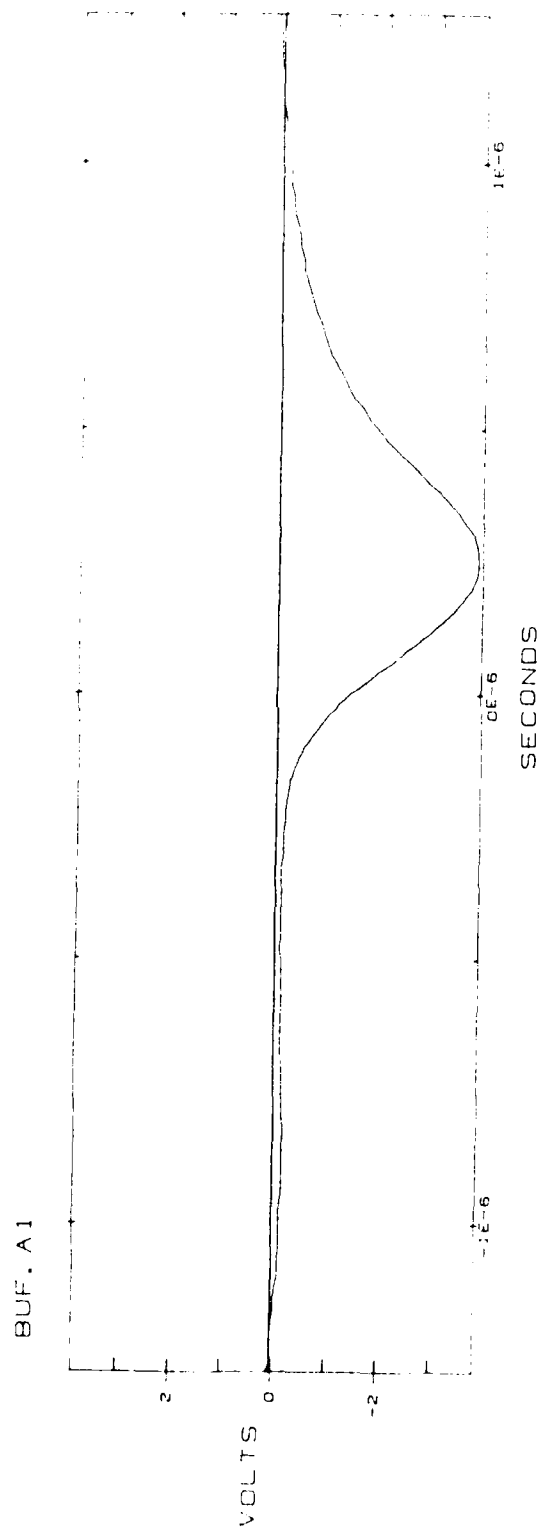


Figure 3.11-12. Noise Pop (Upper Trace Video BW=1 MHz) and IF Signal.

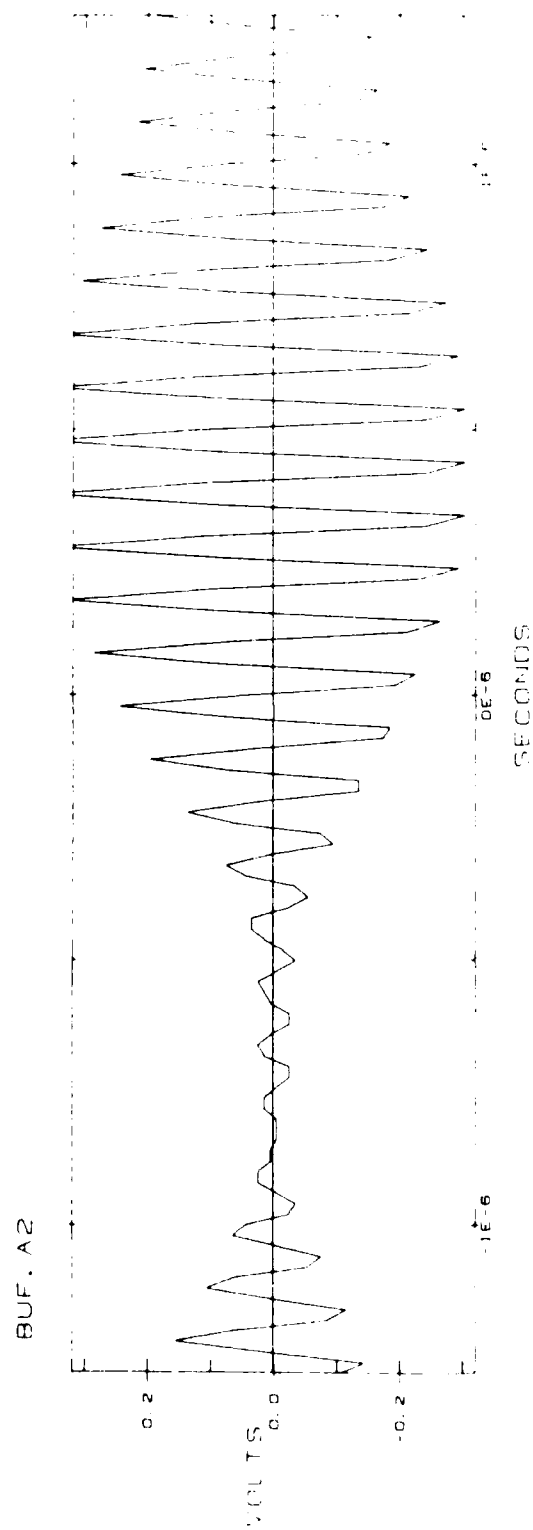
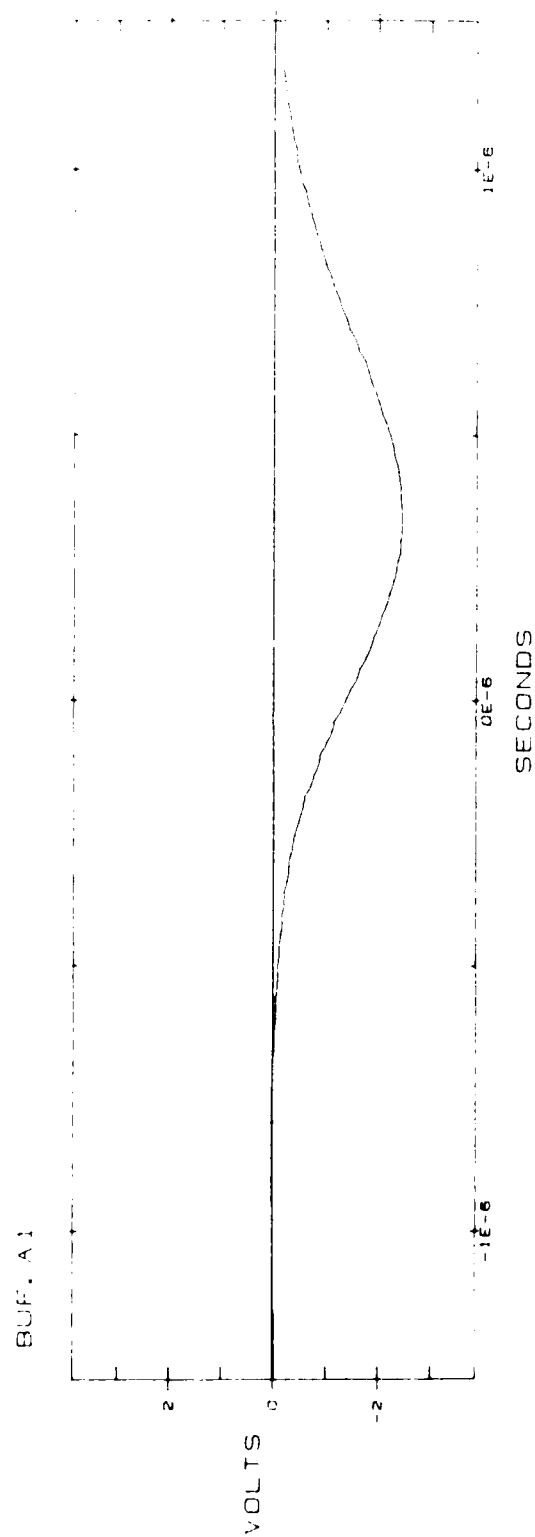


Figure 3.11-13. Pop Noise (Upper Trace Video BW=500 KHz) and IF Signal.

OUT. A1

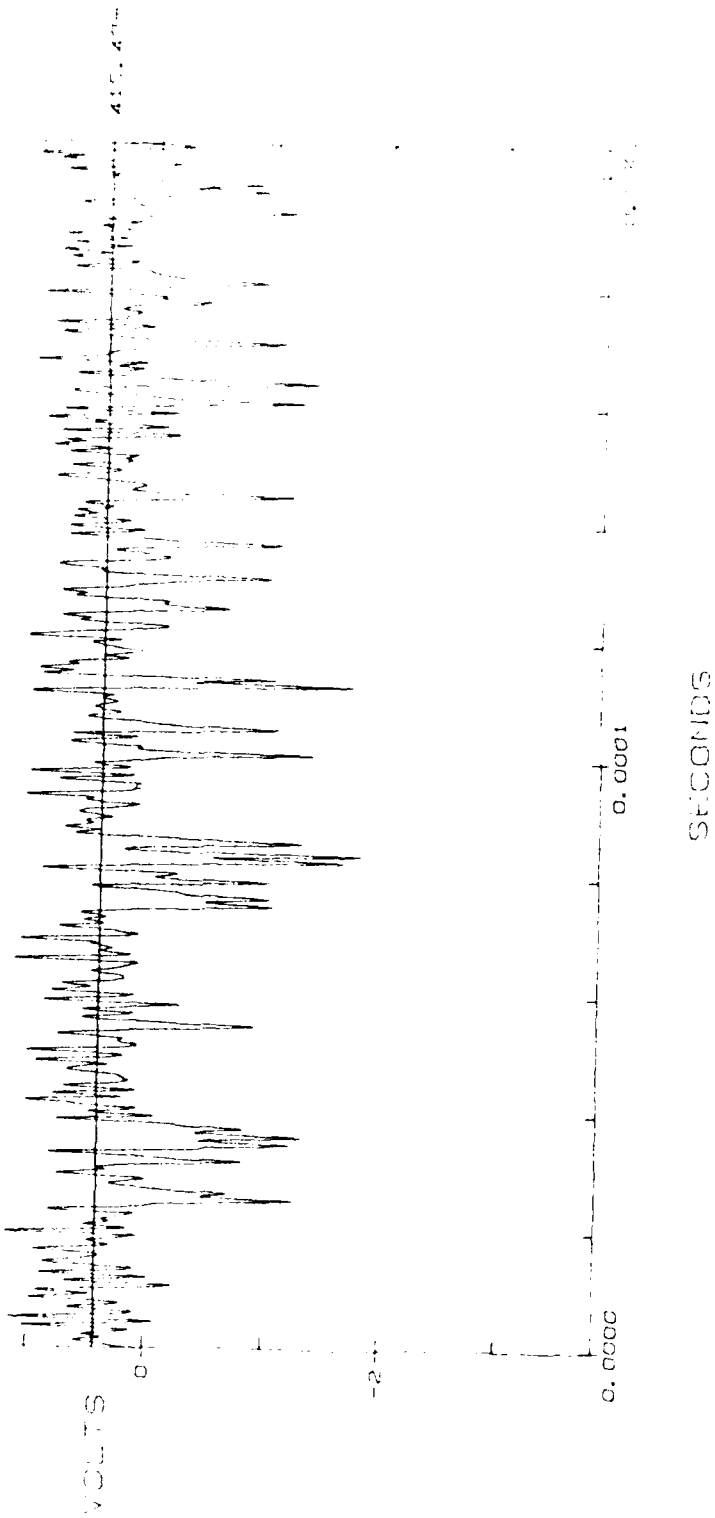


Figure 3.11-14. Pop Noise with IF Signal = 10.25 MHz.

BUF . A 1

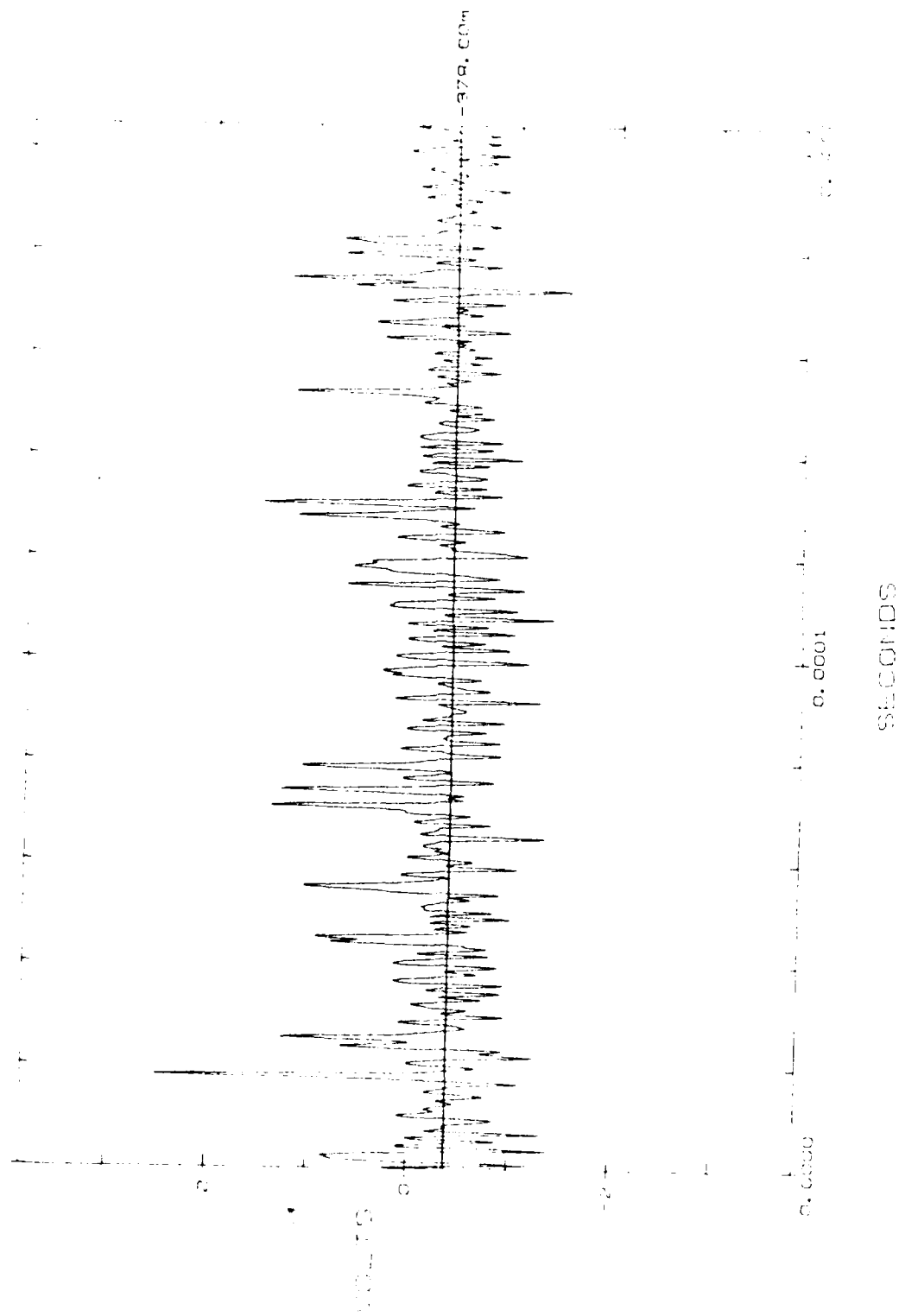


Figure 3.11-15. Pop Noise with 15 Signal = 9.75 MHz.

BUF. A1

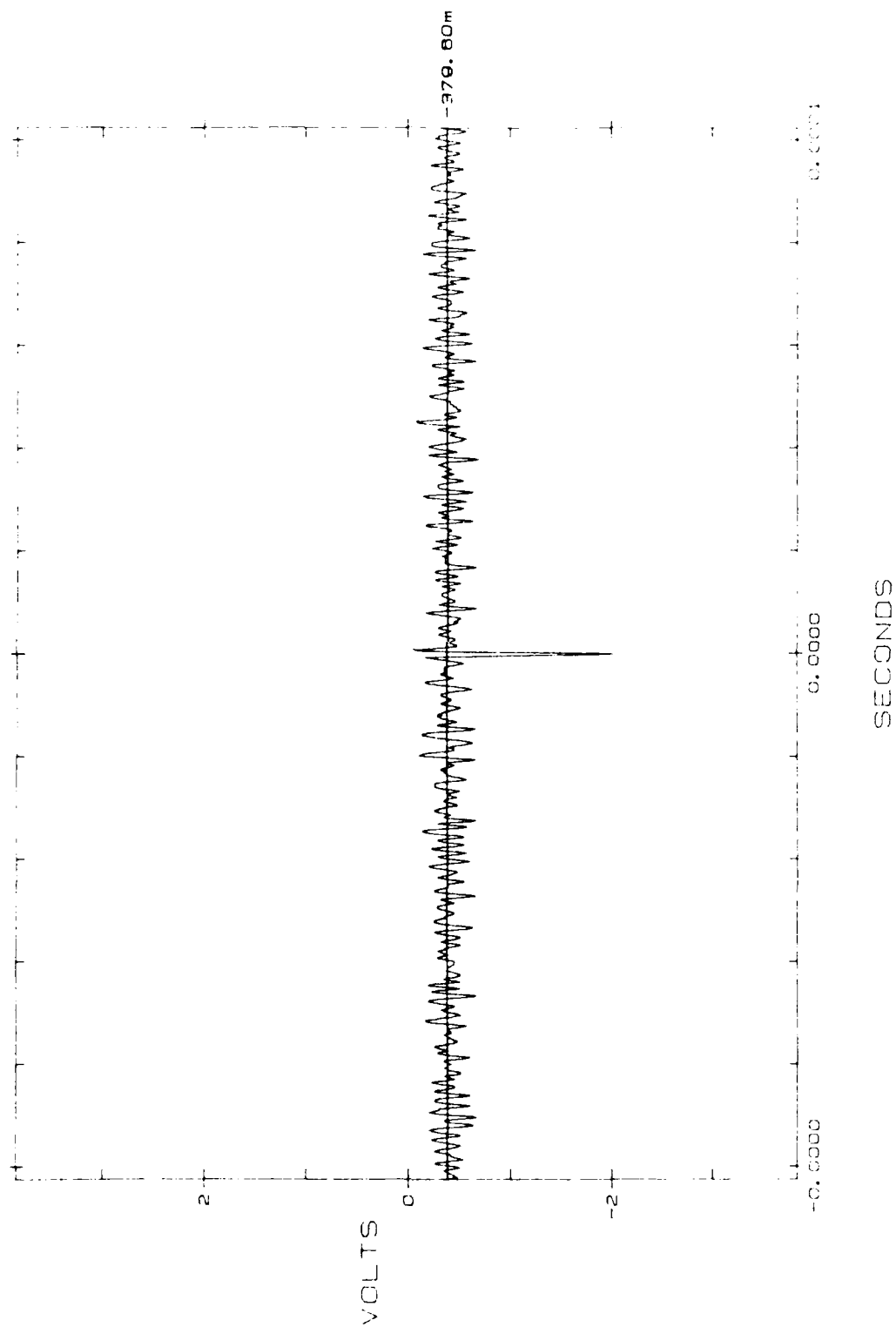


Figure 3.11-16. Noise Pop Away from Center Frequency.

BUF. A1

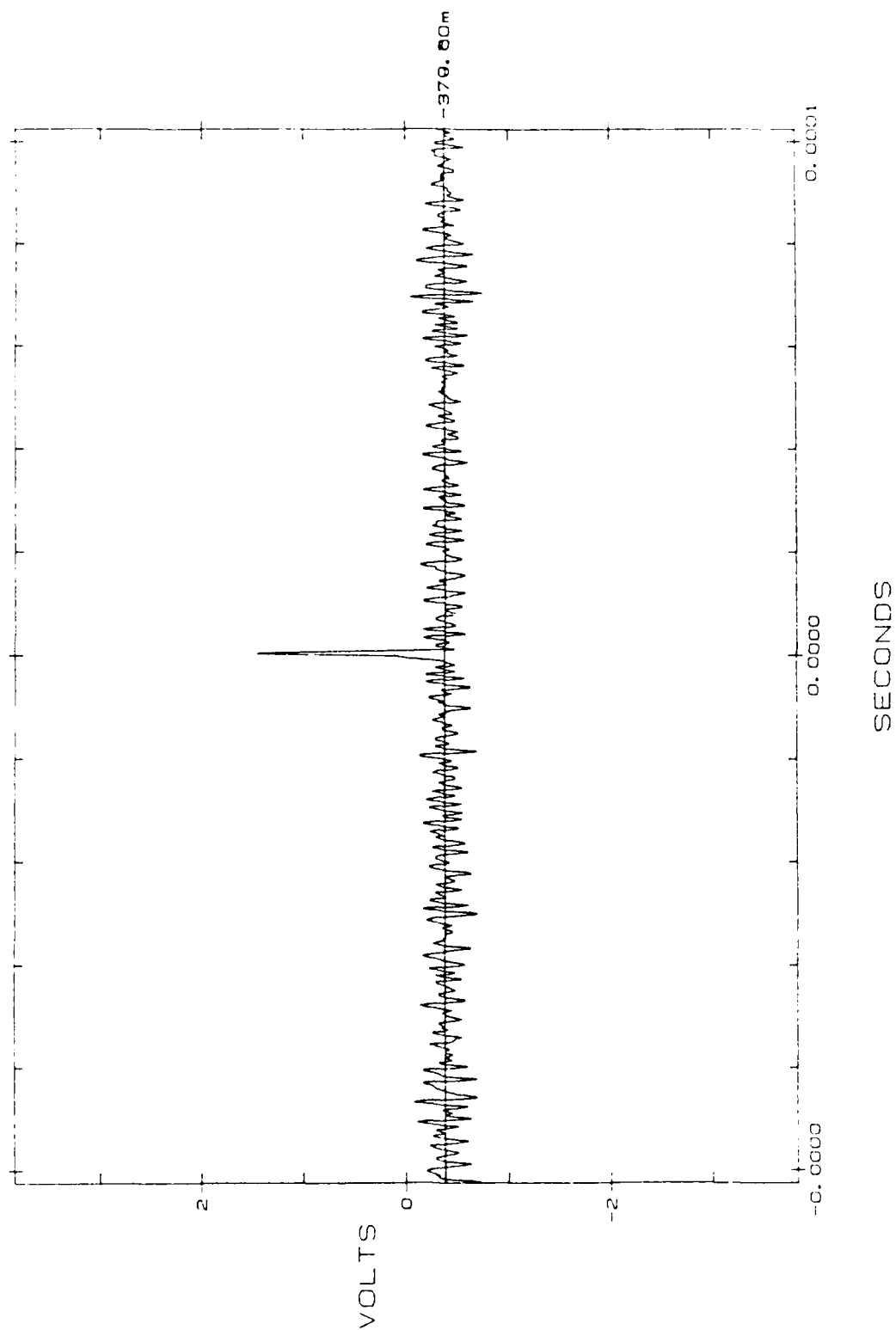


Figure 3.11-17. Noise Pop with Area = 2 PI.



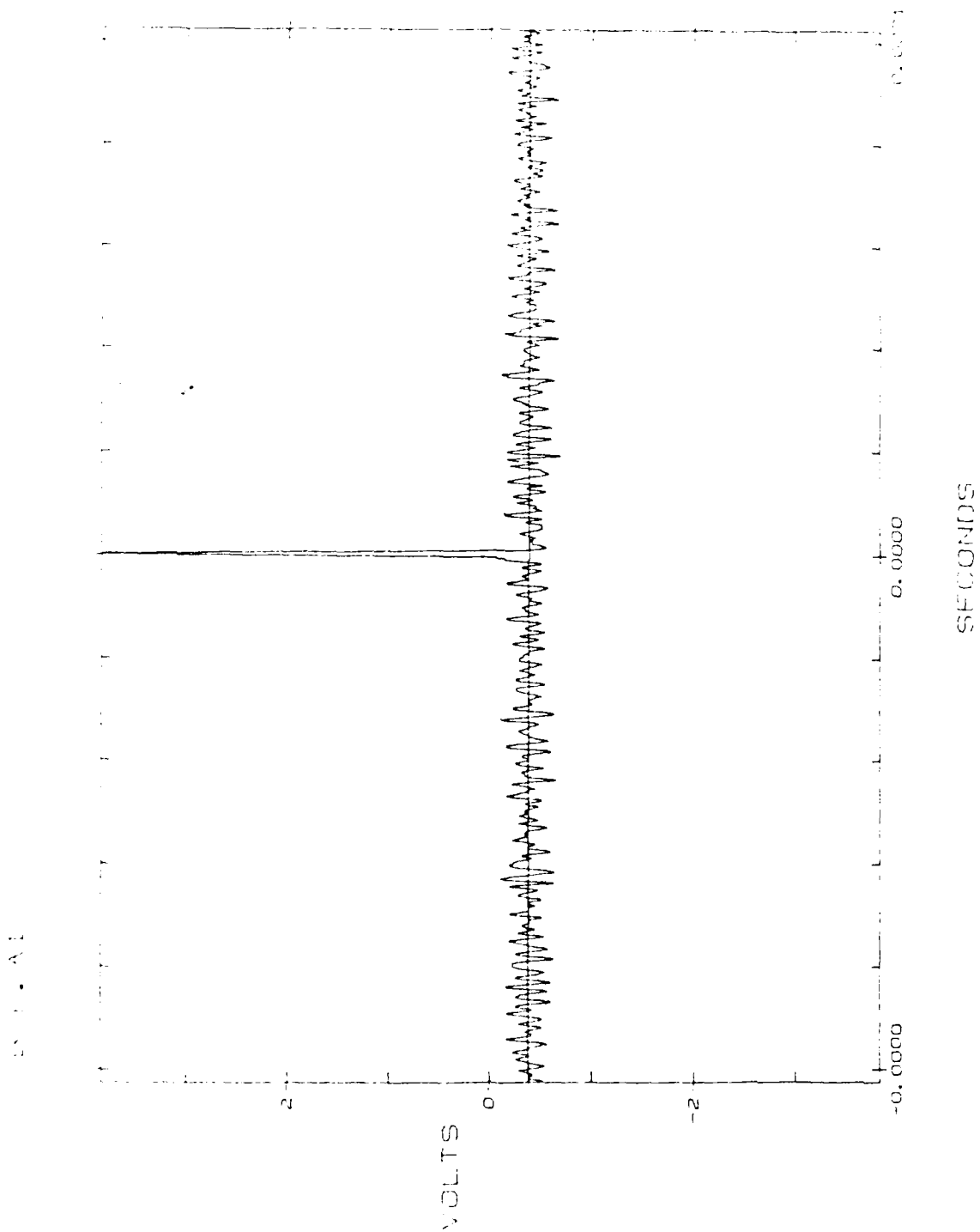


Figure 3.11-18. Noise Pop with Area > 2 PI.

BUF. A1

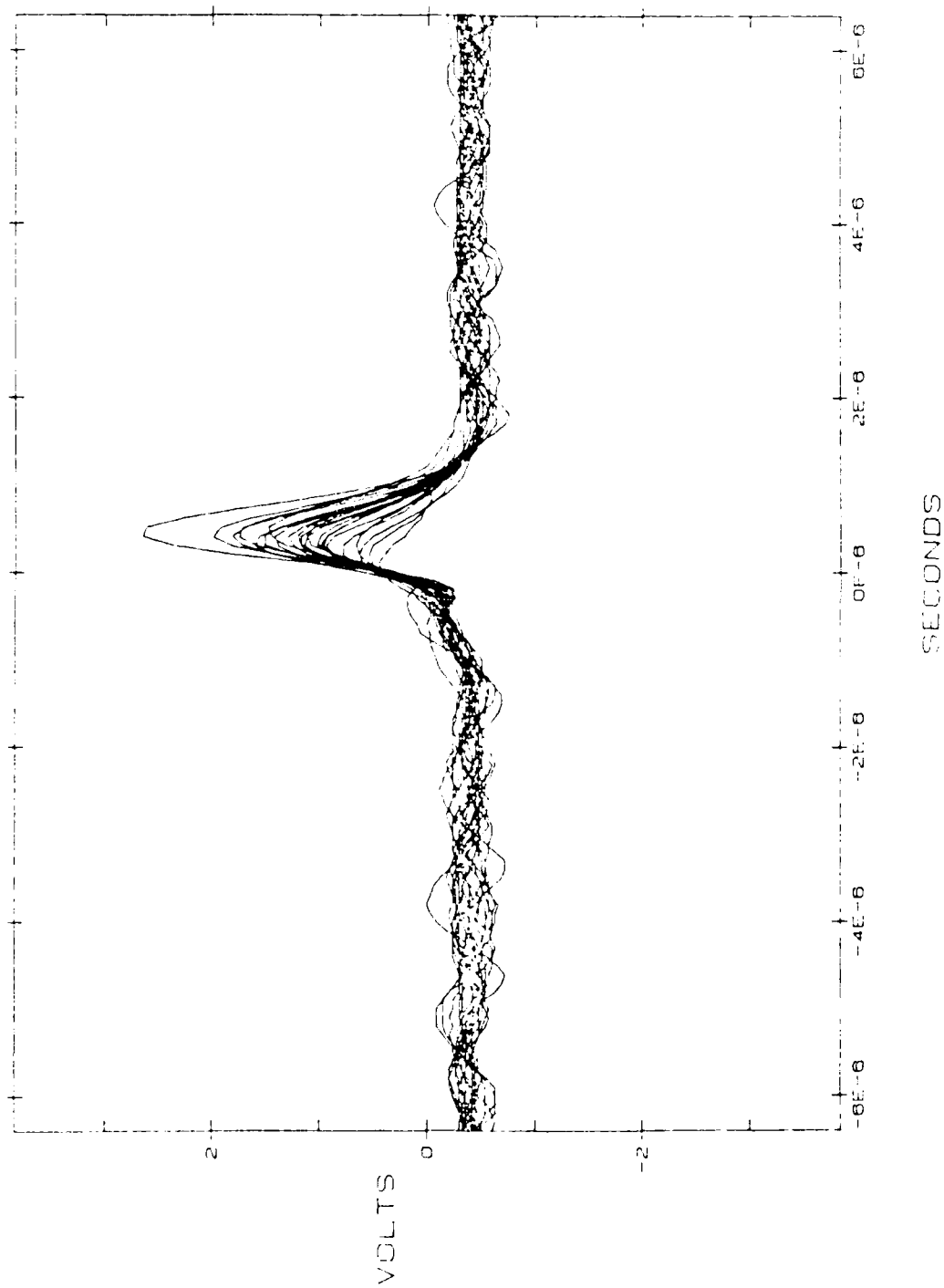


Figure 3.11-19. Superposition of Several Noise Pops (IF Bandwidth=1 MHz).

REF. A1

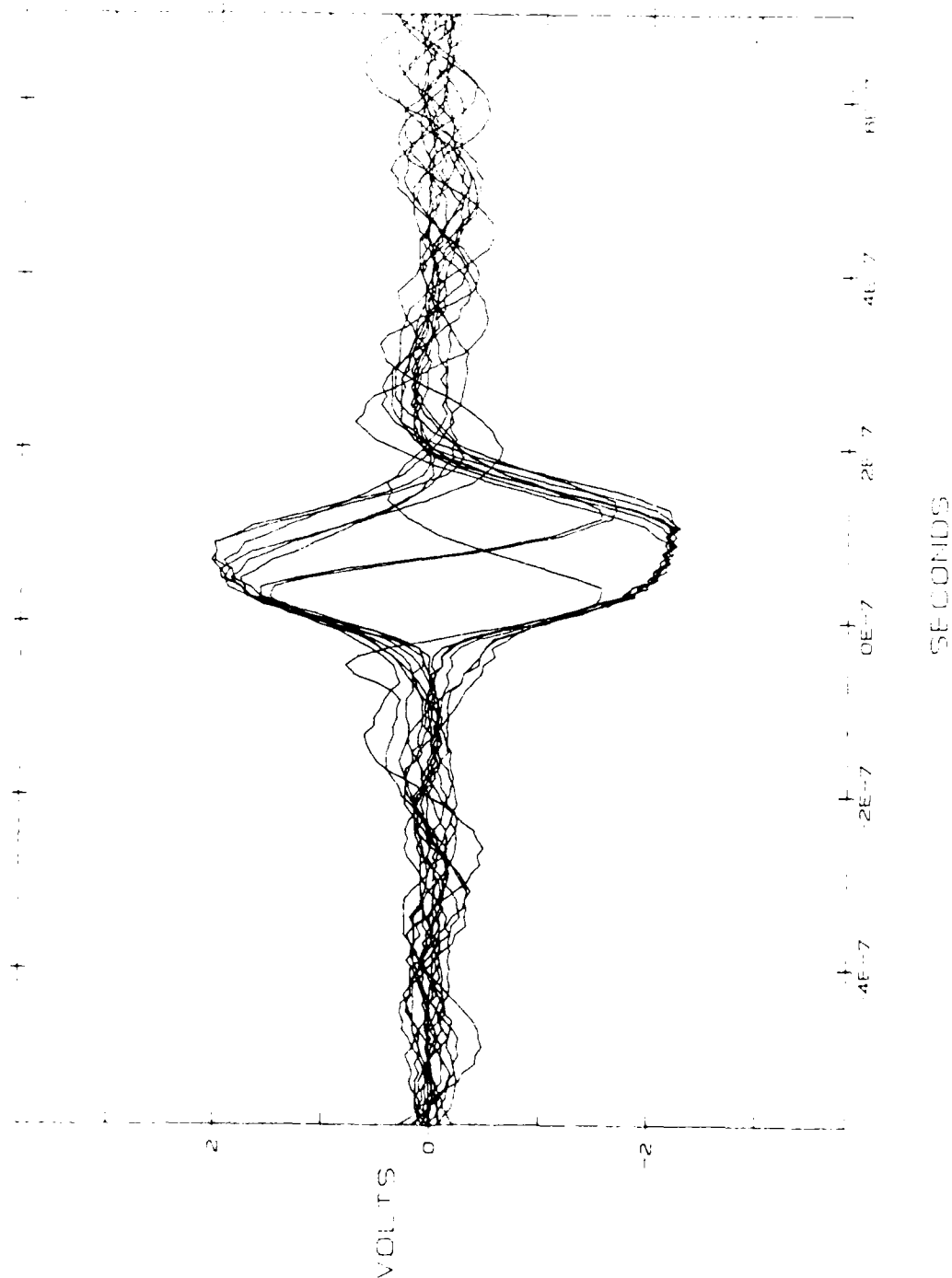
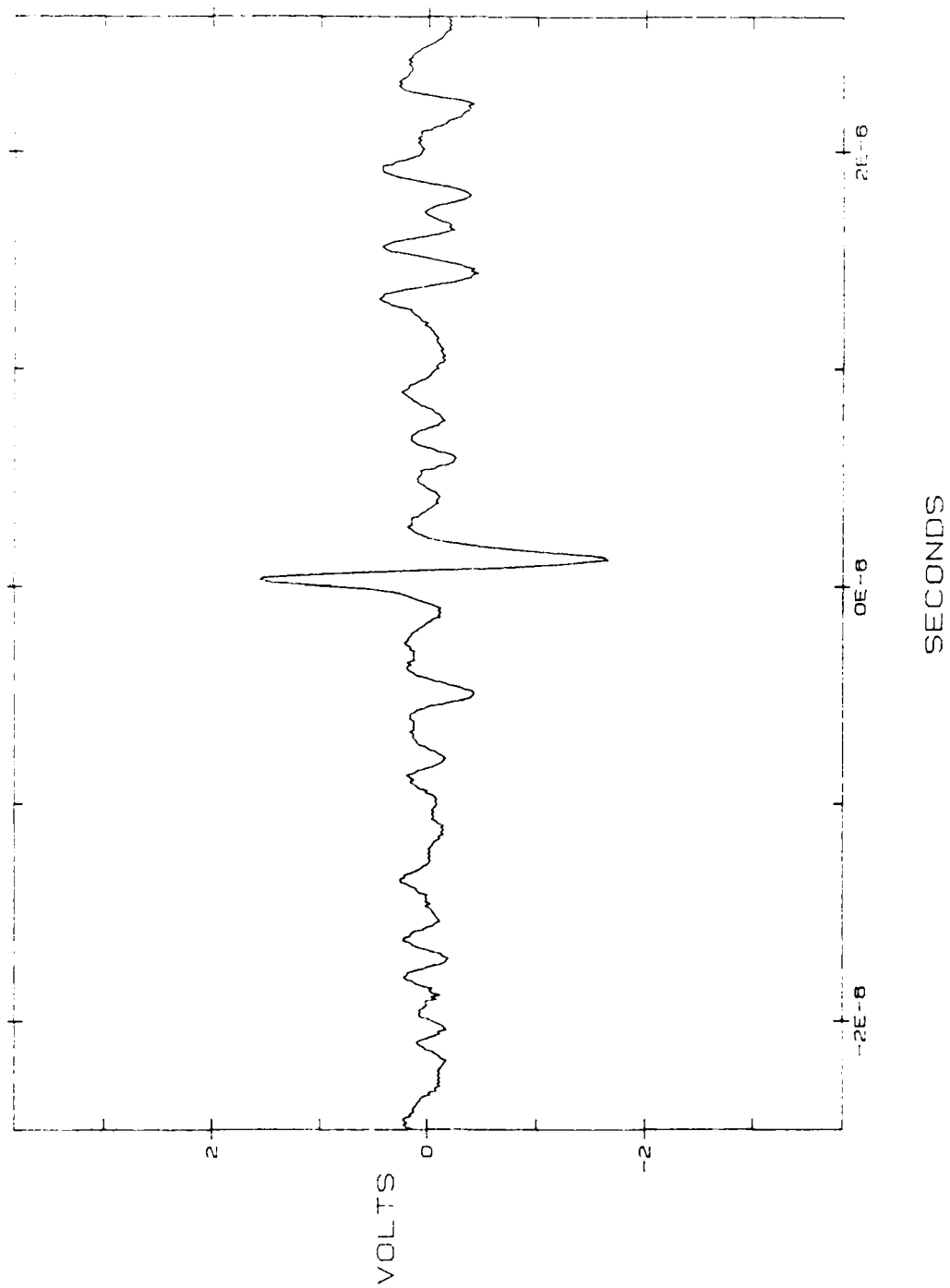


Figure 3.11-20. Superposition of Several Noise Pops (IF Bandwidth=10 MHz).

BUF. A1



3.11- 17

Figure 3.11-21. Doublet.

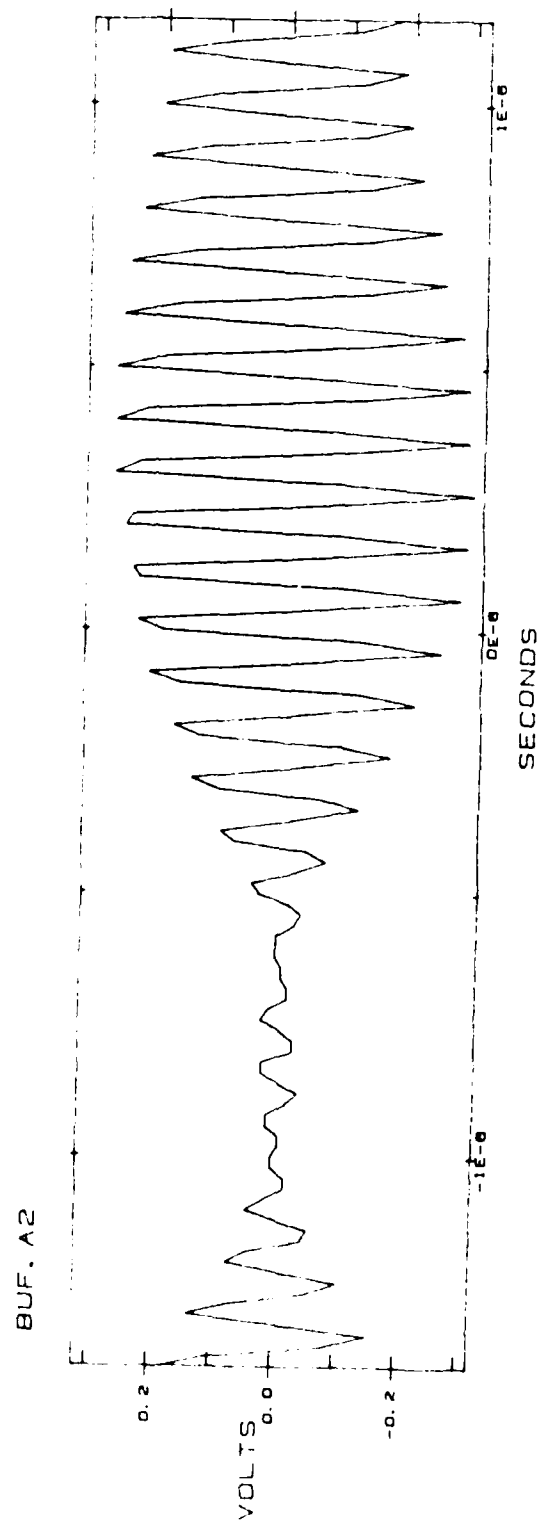
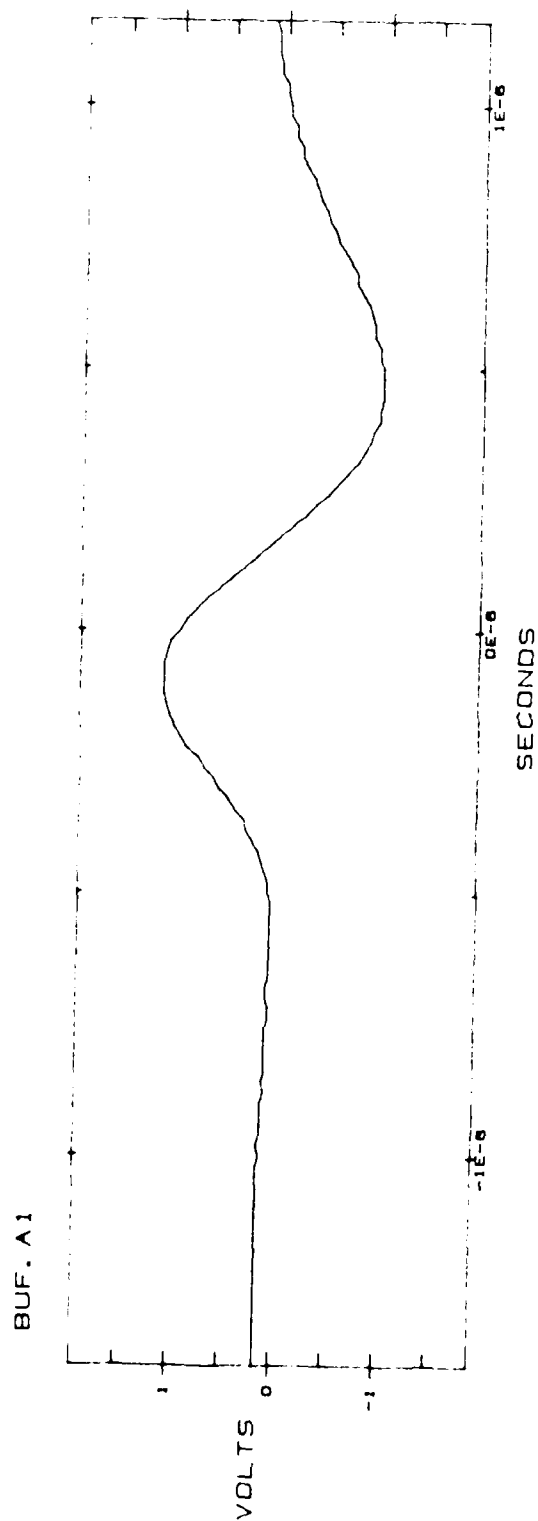


Figure 3.11-22. Doublet (Upper Trace) and IF Signal.

### 3.12 REFERENCES

- Secretariat, Range Commanders Council. Telemetry Standards. White Sands Missile Range, New Mexico, RCC, May 1986. (IRIG Standard 106-86).
- Kotelnikov, V. A. The Theory of Optimum Noise Immunity. Dover, New York, 1968.
- Gagliardi, R. M. Introduction to Communications Engineering. Wiley, New York, 1978.
- Tjhung, T. T., and Wittke, P. H. "Carrier Transmission of Binary Data in a Restricted Band," in IEEE Transactions on Communications, Vol. COM-18, pp. 295-304, August 1970.
- Cartier, D. E. "Limiter-Discriminator Detection Performance of Manchester and NRZ Coded FSK," in IEEE Transactions of Aerospace and Electronic Systems, Vol. AES-13, pp. 62-70, January 1977.
- Korn, I. "Error Probability and Bandwidth of Digital Modulation," in IEEE Transactions on Communications, Vol. COM-28, pp. 287-290, February 1980.
- Tan, C. H., T. T. Tjhung, and H. Singh. "Performance of Narrow-Band Manchester Coded FSK With Discriminator Detection," in IEEE Transactions on Communications, Vol. COM-31, pp. 659-667, May 1983.
- Lindsey, W. C. and M. K. Simon. Telecommunication Systems Engineering, Prentice-Hall, Inc., Englewood Cliffs, NJ, p64, 1973.
- Taub, H. and D. L. Schilling. Principles of Communication Systems, McGraw-Hill, New York, pp 162-179, 1971.
- Gregg, W. D. Analog and Digital Communication, John Wiley and Sons, New York, pp 267-294, 1977.
- Downing, J. J. Aerospace Telemetry, Volume I, (ed. by H. L. Stiltz), Prentice-Hall, Englewood Cliffs, NJ, pp 83-141, 1961.
- Hochman, D. Handbook of Telemetry and Remote Control, (ed. by E. L. Gruenberg), McGraw-Hill, New York, pp 9-2 to 9-198, 1967.
- Heberling, E. D. An Experimental Evaluation of the Characteristics of PAM-NRZ/FM Telemetry Systems, Naval Ordnance Laboratory Corona, Corona, California, September 1967. (NOLC Report 741).
- Nichols, M. H. and Rauch, L.L. Radio Telemetry, J. Wiley, 1956.
- Uglow, K. "Noise and Bandwidth in FM/FM Radio Telemetry", IRE Transactions, pp 19-22, May 1957.
- Rosen, C. "System Transmission Parameters Design for Threshold Performance", in Proceedings of the International Telemetry Conference, Vol. XIX, pp 145-182, 1983.

Rechter, R.J. "Summary and Discussion of Signal-to-Noise Ratio Improvement Formulae for FM and FM/FM Links", in Proceedings of the International Telemetry Conference, Vol. III, pp 221-255, 1967.

Panter, P. F. Modulation, Noise, and Spectral Analysis, McGraw-Hill, New York, pp. 236-270, 1965.

Law, E. L., E. T. Kimball, and M. H. Nichols. "Relationship of Noise Power Ratio to FM/FM Data Quality", in Proceedings of the International Telemetry Conference, Vol. XII, pp 234-250, 1976.

Law, E. L., E. T. Kimball, and M. H. Nichols. Relationship of Noise Power Ratio to Subcarrier Discriminator Signal-to Noise Ratio, Pacific Missile Test Center, Point Mugu, CA, 1 Aug 1975. PMTC TP-75-21.

Crosby, M. G. "Frequency Modulation Noise Characteristics". Proc. IRE, 25, 472-514 (1937).

Stumpers, F. L. H. M. "Theory of Frequency-Modulation Noise". Proc. IRE, 36, 1081-1092 (1948).

Rice, S. O. "Noise in FM Receivers". Time Series Analysis, ed. M. Rosenblatt, pp. 395-422 (Wiley 1963).

Sklar, B. "What the System Link Budget Tells the System Engineer or How I Learned to Count in Decibels", in Proceedings of the International Telemetry Conference, Vol. XV, pp 331-344, 1979.

Lantz, N. F., and M. H. Nichols. "Approximate Design Formulae and Procedures for Designing Hybrid Telemetry Systems Using an FM Carrier", in Proceedings of the International Telemetry Conference, Vol. XIII, pp 261-271, 1977.

Reference Data for Radio Engineers, Howard W. Sams & Co., Inc., Indianapolis, IN, p 28-12, 1975.

Streich, R. G., D. E. Little, and R. B. Pickett. "Dynamic Requirements for Diversity Combiners", in Proceedings of the International Telemetry Conference, Volume 8, pp. 635-642, October 1972.

Law, E. L. Pulse Code Modulation Telemetry, Properties of Various Binary Modulation Types, Pacific Missile Test Center, Point Mugu, CA, TP000025, June 1984.

Law, E. L. Analog Frequency Modulation Telemetry, Pacific Missile Test Center, Point Mugu, CA, TP000042, September 1987.

#### 4.0 TELEMETRY TRANSMITTING SYSTEM CHARACTERIZATION

This section will present a brief overview of telemetry transmitting systems followed by a discussion of system selection criteria and references. The telemetry transmitting system consists of several major subsystems:

1. Signal sources (frequently transducers)
2. Signal conditioning
3. Signal multiplexing (frequency and/or time division)
4. Signal coding (if used)
5. Modulation of carrier signal by multiplexed information signal (or recording of information signal on magnetic tape)
6. Transmitting antenna.

These subsystems must be properly interfaced to each other and must be properly designed in order to provide the desired information. The transmitting system must also be compatible with the receiving, recording, and data processing facilities.



#### 4.1 INTRODUCTION

This subsection will provide a brief overview of telemetry transmitting systems. The transmitting system basically converts one or more information sources into a predetermined format and transmits the information to a receiving facility. The information might include the temperature at a certain location in a missile, the vibration at another point, the position of a fin, the voltage provided by a battery, the digital outputs from a computer, or almost anything else that one may want to monitor.

The first link in the telemetry chain is frequently a transducer. A transducer is a device that converts energy from one form to another. An example is the conversion of the temperature at a point on a missile to a voltage that can be multiplexed with other voltages. There are many different types of transducers available. The Range Commanders Council (RCC) publishes a Directory of Transducer Users. This directory is updated periodically and includes a list of people who are knowledgeable about various types of transducers. This document is available from the Defense Logistics Agency, DTIC, Attn: FDRA, Cameron Station, Alexandria, VA 22304-6145. Government agencies can get a copy from the secretariat of the Range Commanders Council (AUTOVON 258-1107). The Telemetry Standards (IRIG Document 106) also includes a list of transducer related documents. The Vehicular Instrumentation/Transducer Committee of the Telemetry Group hosts a Transducer Workshop every two years. The proceedings of this workshop are also available from the RCC Secretariat. The North Atlantic Treaty Organization (NATO) Advisory Group for Aerospace Research and Development (AGARD) has also published a series of documents on transducers and flight instrumentation<sup>1</sup>.

The transducer outputs usually need to be modified into the desired form for sampling and/or multiplexing. This signal conditioning can include amplification, level shifting, filtering, buffering, rectification, logarithmic amplification, companding, etc. These topics are addressed in books on analog design and instrumentation and will not be discussed here.

The conditioned information signals are then combined with other signals. This is called multiplexing. The two most common types of multiplexing are frequency division multiplexing (FDM) and time division multiplexing (TDM). FDM is frequently used in simple systems where only a few channels of data are needed. It is also used in combination with TDM, especially for wideband vibration data, etc. The conditioned information signals are applied to different, compatible subcarrier oscillators (SCOs). These SCO outputs are then added together to form one composite signal. This signal then modulates the transmitter. FDM systems are discussed in subsection 3.7.

<sup>1</sup>Pool, A. and D. Bosman ed. Basic Principles of Flight Test Instrumentation Engineering. North Atlantic Treaty Organization, Advisory Group for Aerospace Research and Development, AGARD-AG-160-Vol. 1, April 1974.

Pulse code modulation (PCM) is the most popular form of TDM system. Various PCM systems are discussed in subsections 3.1 through 3.4 and sections 3.7 and 3.8. TDM systems sample the information signals at pre-determined times. Each signal has its own time slots for transmission. The sampling rate is typically 3 to 10 times the maximum expected signal frequency.<sup>2,3,4</sup> The required sampling rate is a function of the accuracy required, the roll-off rate of the signal and noise spectrums beyond the maximum expected signal frequency, and the type and roll-off rate of the anti-aliasing and signal reconstruction filters.

The telemetry transmitter converts the multiplexed signal into a modulated radio frequency (RF) signal. Telemetry transmitters usually use either linear frequency or phase modulation. The output power is usually limited by the available supply current or the possibility of interference with other systems or signals. The transmitting antenna radiates the RF energy to the outside world.

<sup>2</sup>Gardenhire, L. W. "Filtering and Sampling" in Basic Principles of Flight Test Instrumentation Engineering, ed. A. Pool and D. Bosman, North Atlantic Treaty Organization, Advisory Group for Aerospace Research and Development, AGARD-AG-160-Vol. 1 Chapter 6, April 1974.

<sup>3</sup>Capps, J. W., W. F. Link, C. D. Eatough, and D. G. Childers, Study and Experimental Investigation on Sampling Rate and Aliasing in Time-Division Telemetry Systems, by Aeronutronic for Wright-Patterson AFB, Ohio, Technical Report No. ASD-TR-61-553, June 1962.

<sup>4</sup>Handbook of Telemetry and Remote Control, E. L. Gruenberg ed., McGraw-Hill, New York, 1967.

## 4.2 TRANSMITTING SYSTEM SELECTION GUIDELINES

The type of transmitting system to use for a particular application depends on the number of signals to be monitored, the bandwidths of these signals, the required data accuracy, whether the signals are analog or digital, etc. If a large number of different signals must be monitored, a PCM or combination PCM and FM/FM system is usually the best choice. If only a few analog signals need to be monitored an FM/FM or PAM/FM system may be a good choice. FM/FM (or analog FM if there is only one very wideband signal) is usually a good choice for wideband analog signals (such as vibration data).

PCM can provide the best data quality with strong received signals because it is immune to many of the problems which can occur in the telemetry system. If the received IF SNR is 15 dB or greater, the data at the bit synchronizer output is essentially the same as it was at the commutator output. However, as the IF SNR decreases, the data quality of PCM does degrade faster than most other systems. Error correction and detection coding can also be added to the transmitted PCM signal to further extend the error free range. If much of the data to be transmitted is from digital computers or other digital data sources, PCM or a combination of PCM and FM/FM is the best method to consider. If the transmitted signal must be protected from unauthorized observers, PCM is also the best system to use. Overall, PCM is usually the best choice except for wideband analog signals. Most new telemeters use either PCM or a combination of PCM and FM/FM or PCM and analog FM.

The Telemetry Group of the Range Commanders Council has recently upgraded the PCM Standards<sup>5</sup>. The new standards will include methods for dealing with different formats during one mission, the MIL-STD 1553 bus, etc. It is essential that these standards be used as a guideline when designing PCM telemetry systems. Overly creative designs, which do not adhere to these standards, cause many problems for the telemetry processing systems and waste a lot of time and money.

The length of the PCM frame synchronization word, in a well designed system, should be a minimum of 16 bits. Short synchronization patterns lead to a high probability of false acquisition or a low probability of correct acquisition with noisy data. Recommended synchronization patterns are included in Appendix C of reference 1. The probability of correctly detecting synchronization<sup>6</sup> with a BER of  $p$  (independent errors assumed), a pattern length of  $n$  bits, and allowing  $q$  errors is:

$$P_{\text{sync}} = \sum_{r=0}^q \frac{n!}{(n-r)! r!} p^r (1-p)^{n-r}.$$

<sup>5</sup>Secretariat, Range Commanders Council, *Telemetry Standards*, White Sands Missile Range, NM, RCC, May 1986. (IRIG Standard 106).

<sup>6</sup>Hill, E. R., "Techniques for Synchronizing Pulse-Code-Modulated Telemetry", *Proceedings of the 1963 National Telemetry Conference*, paper 3-3.

This is illustrated in figures 4.2-1 and 4.2-2 for synchronization pattern lengths of 16, 24, and 32 bits. The data in figure 4.2-1 shows that if we desire to have a probability of 0.9 of detecting a 24-bit frame synchronization pattern when the BER is 0.1, we need to allow 4 errors in the pattern. If the BER is reduced to 0.01 (see figure 4.2-2), we will have a probability of greater than 0.97 of detecting the pattern if we allow 1 error.

The probability of randomly detecting false synchronization with random data, a pattern length of  $n$  bits, and allowing  $q$  errors is:

$$P_{\text{false sync}} = \frac{\sum_{r=0}^q \frac{n!}{(n-r)! r!}}{2^n}$$

Figure 4.2-3 presents data on the probability of false detection of the synchronization pattern for pattern lengths of 16, 24, and 32 bits. Assume we have a PCM minor frame which is 4000 bits long and we would like the probability of detecting a false synchronization pattern in one minor frame time to be less than 0.2. Therefore, the probability of false detection of the synchronization pattern in any location would have to be less than  $0.2/4000$  or 0.00005. The data in figure 4.2-3 shows that we could not allow any errors in search mode with a 16-bit pattern, we could allow 2 errors with a 24-bit pattern, and we could allow 4 errors with a 32-bit pattern. If the BER is 0.1, the probability of detecting the actual synchronization pattern with a 16-bit pattern and 0 errors allowed is only 0.19. Therefore, we are more likely to detect a false pattern than the correct pattern. The acquisition time may be long under these conditions. The probability of correctly detecting the 24-bit pattern while allowing 2 errors is 0.56, while the probability of correctly detecting the 32-bit pattern while allowing 4 errors is 0.79. This illustrates the advantage of long synchronization patterns when the data is noisy. It is extremely desirable to have the PCM decommutator synchronized to the transmission system's commutator because no useful data is possible when they are not synchronized.

The recommended peak deviations and premodulation filters for various types of systems are discussed in subsections 3.1 through 3.8. The transmitting system designer needs to be aware of the capabilities of the telemetry ground stations that will receive, record, and process the data. If possible the transmitting system should be designed to be compatible with the ground stations. In the rare cases where this is not possible, the transmitting system designer needs to give the ground station the maximum possible lead time to prepare for a new requirement. A link analysis (see subsection 3.9) should also be done for the various scenarios that are expected.

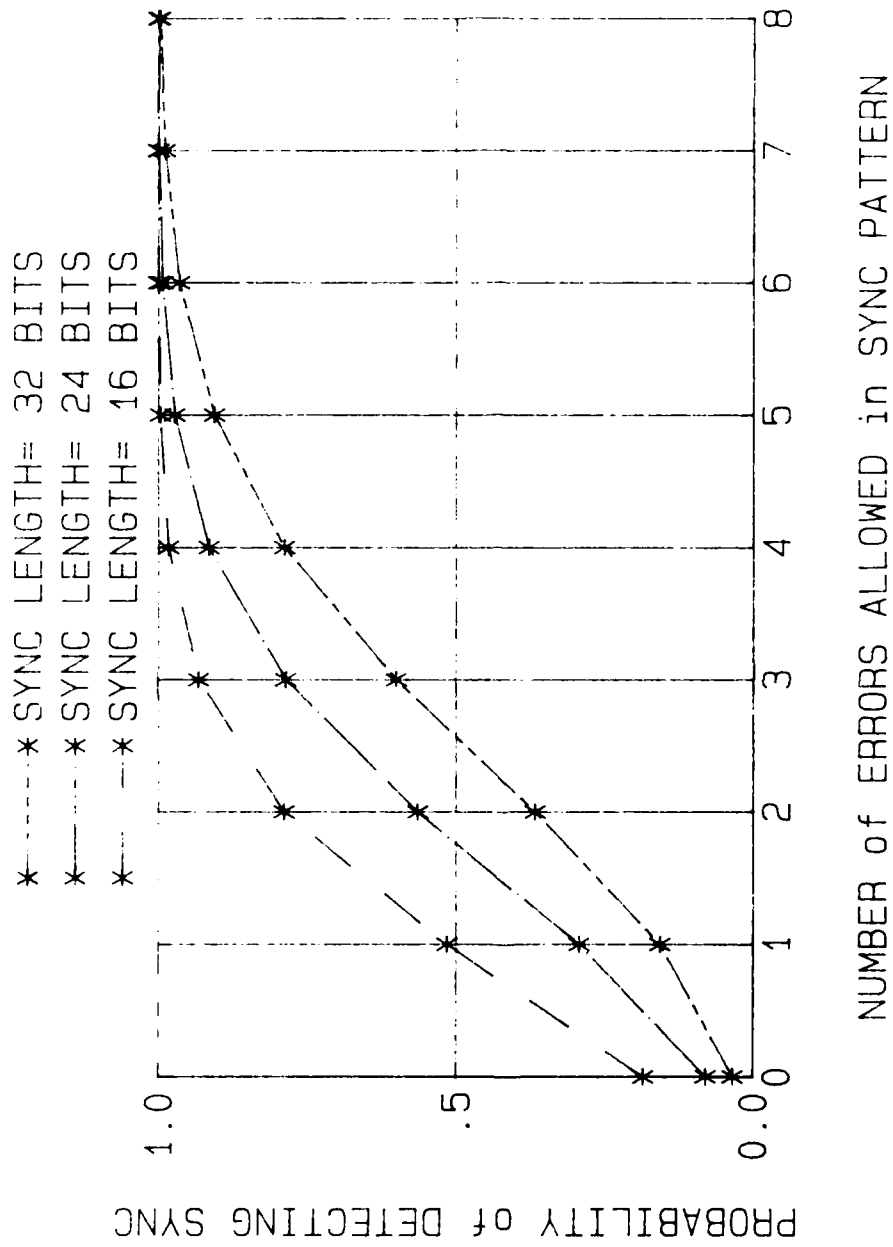


Figure 4.2-1. Probability of Detecting Sync Pattern with BER = 0.1.

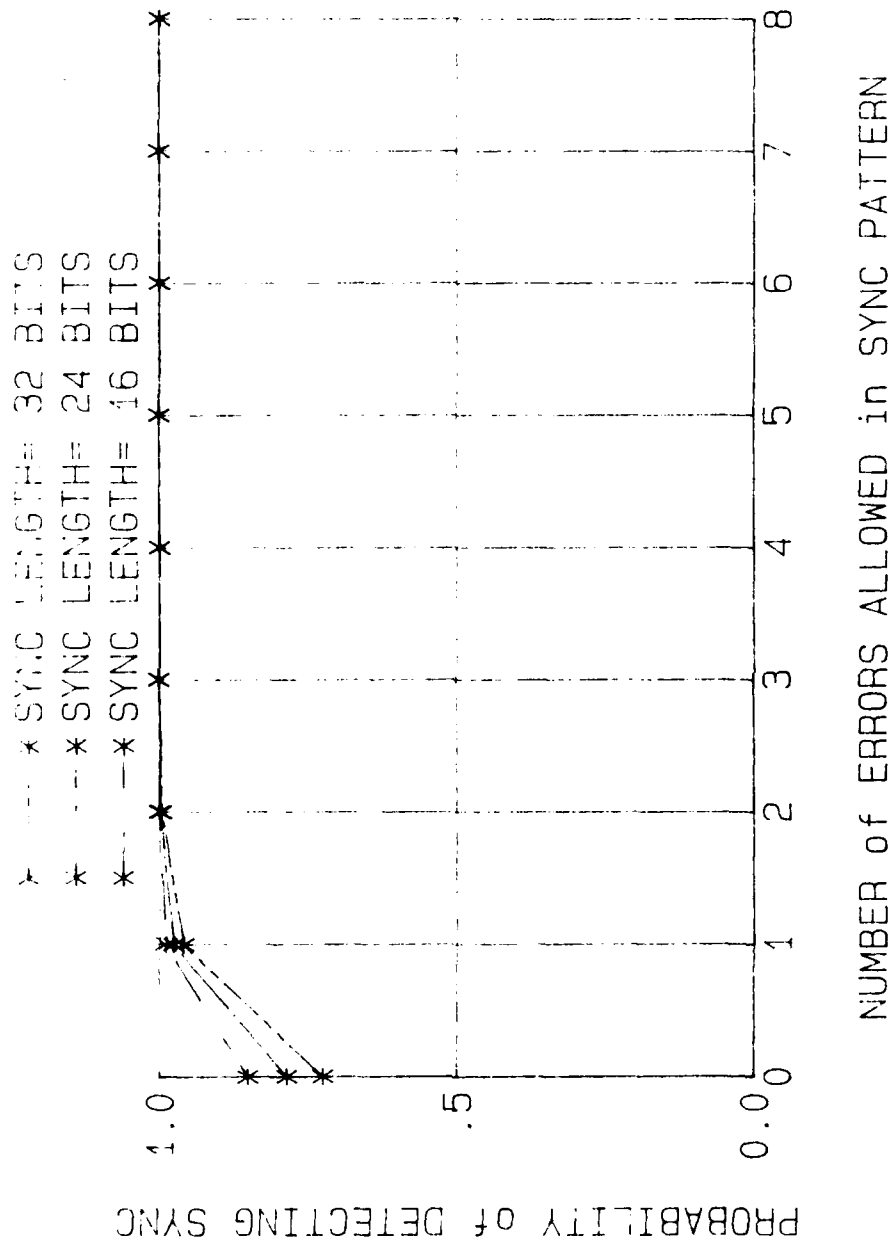


Figure 4.2-2. Probability of Detecting Sync Pattern with BER = 0.01.

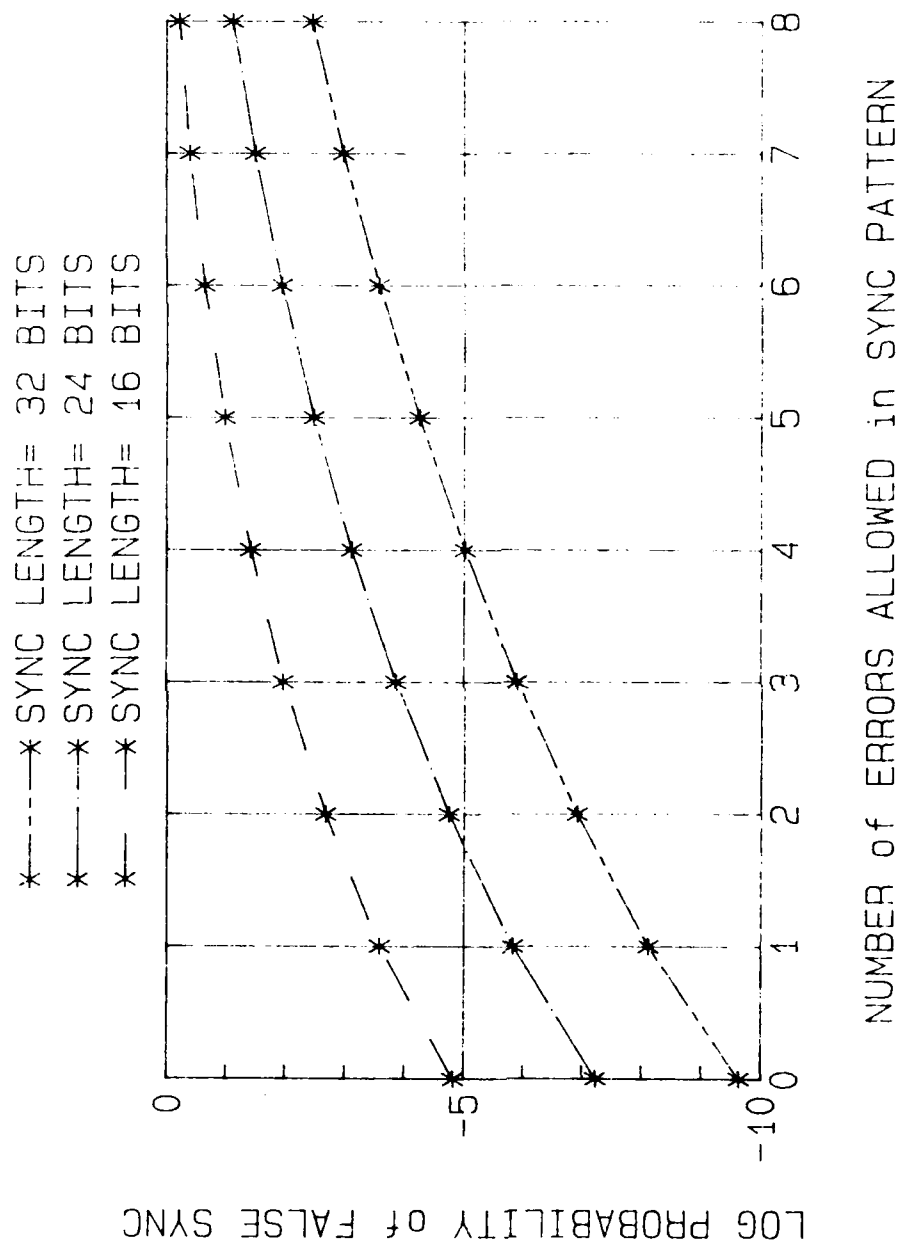
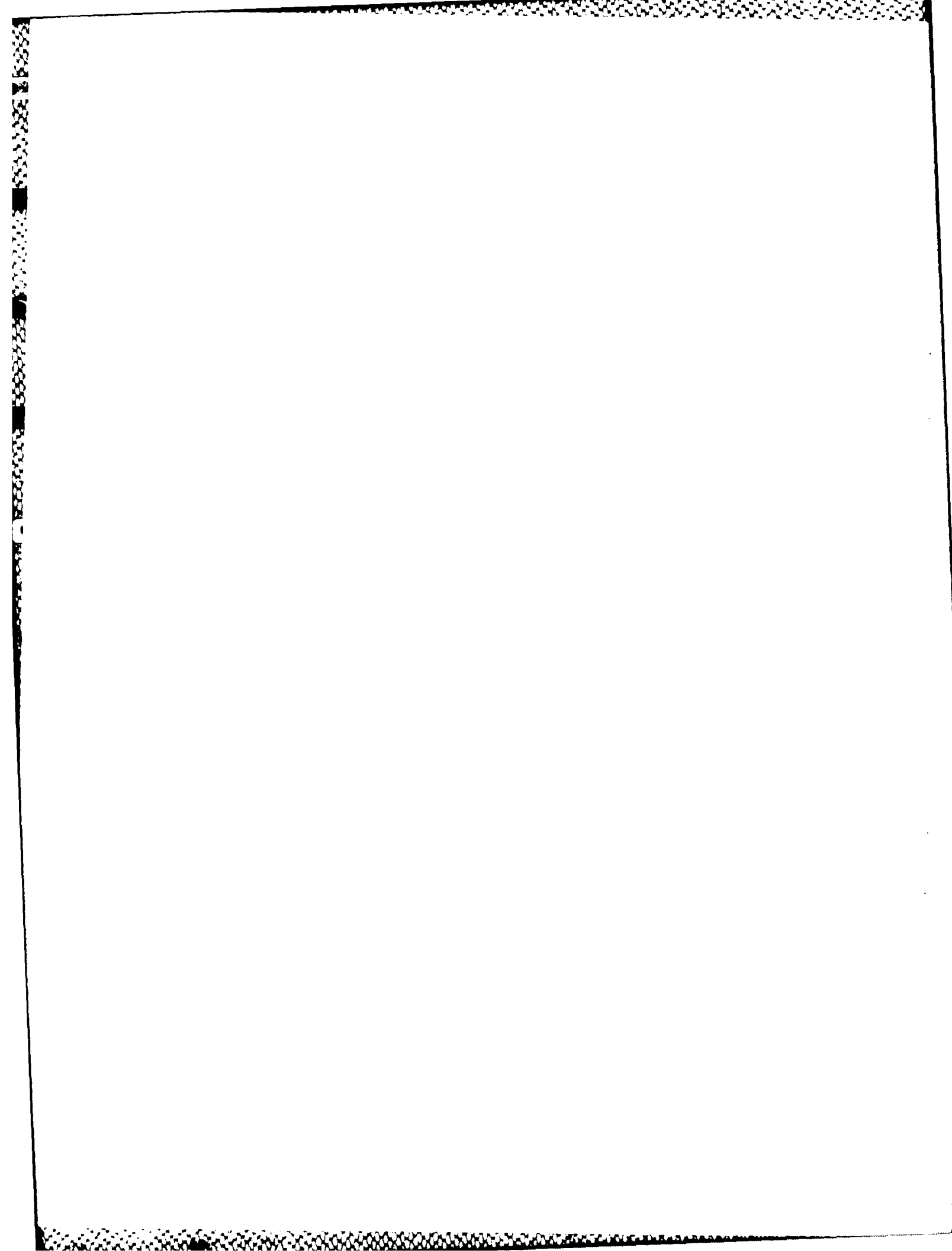


Figure 4.2-3. Probability of Detecting False Sync Pattern.





### 4.3 REFERENCES

- Secretariat, Range Commanders Council. Telemetry Standards. White Sands Missile Range, New Mexico, RCC, May 1986. (IRIG Standard 106-86).
- Secretariat, Range Commanders Council. Directory of Transducer Users(Seventh Edition). White Sands Missile Range, New Mexico. (IRIG Document 100-86).
- Secretariat, Range Commanders Council. End-to-End Test Methods for Telemetry Systems. White Sands Missile Range, New Mexico. (IRIG Document 118-79 vol. I).
- Secretariat, Range Commanders Council. Test Methods for Vehicle Telemetry Systems. White Sands Missile Range, New Mexico. (IRIG Document 118-82 vol. V).
- Borek, R. W. Practical Aspects of Instrumentation System Installation. North Atlantic Treaty Organization, Advisory Group for Aerospace Research and Development, AGARD-AG-160-Vol. 13, September 1981.
- Basic Principles of Flight Test Instrumentation Engineering. A. Pool and D. Bosman ed., North Atlantic Treaty Organization, Advisory Group for Aerospace Research and Development, AGARD-AG-160-Vol. 1, April 1974.
- Gagliardi, R. M. Introduction to Communications Engineering. Wiley, New York, 1978.
- Tjhung, T. T., and P. H. Wittke. "Carrier Transmission of Binary Data in a Restricted Band," in IEEE Transactions on Communications, Vol. COM-18, pp. 295-304, August 1970.
- Cartier, D. E. "Limiter-Discriminator Detection Performance of Manchester and NRZ Coded FSK," in IEEE Transactions of Aerospace and Electronic Systems, Vol. AES-13, pp. 62-70, January 1977.
- Korn, I. "Error Probability and Bandwidth of Digital Modulation," in IEEE Transactions on Communications, Vol. COM-28, pp. 287-290, February 1980.
- Tan, C. H., T. T. Tjhung, and H. Singh. "Performance of Narrow-Band Manchester Coded FSK With Discriminator Detection," in IEEE Transactions on Communications, Vol. COM-31, pp. 659-667, May 1983.
- Taub, H. and D. L. Schilling. Principles of Communication Systems. McGraw-Hill, New York, pp 162-179, 1971.
- Gregg, W. D. Analog and Digital Communication. John Wiley and Sons, New York, pp 267-294, 1977.
- Downing, J. J. Aerospace Telemetry, Volume I, (ed. by H. L. Stiltz), Prentice-Hall, Englewood Cliffs, NJ, pp 83-141, 1961.

Handbook of Telemetry and Remote Control, E. L. Gruenberg ed., McGraw-Hill, New York, 1967.

Heberling, E. D. An Experimental Evaluation of the Characteristics of PAM-NRZ/FM Telemetry Systems, Naval Ordnance Laboratory Corona, Corona, California, September 1967. (NOLC Report 741).

Nichols, M. H. and L. L. Rauch. Radio Telemetry, J. Wiley, 1956.

Ugnow, K. "Noise and Bandwidth in FM/FM Radio Telemetry", IRE Transactions, pp 19-22, May 1957.

Rosen, C. "System Transmission Parameters Design for Threshold Performance", in Proceedings of the International Telemetry Conference, Vol. XIX, pp 145-182, 1983.

Rechter, R.J. "Summary and Discussion of Signal-to-Noise Ratio Improvement Formulae for FM and FM/FM Links", in Proceedings of the International Telemetry Conference, Vol. III, pp 221-255, 1967.

Sklar, B. "What the System Link Budget Tells the System Engineer or How I Learned to Count in Decibels", in Proceedings of the International Telemetry Conference, Vol. XV, pp 331-344, 1979.

Lantz, N. F., and M. H. Nichols. "Approximate Design Formulae and Procedures for Designing Hybrid Telemetry Systems Using an FM Carrier", in Proceedings of the International Telemetry Conference, Vol. XIII, pp 261-271, 1977.

Hill, E. R., "Techniques for Synchronizing Pulse-Code-Modulated Telemetry". Proceedings of the 1963 National Telemetry Conference, paper 3-3.

Capps, J. W., W. F. Link, C. D. Eatough, and D. G. Childers. Study and Experimental Investigation on Sampling Rate and Aliasing in Time-Division Telemetry Systems, by Aeronutronic for Wright-Patterson AFB, Ohio, Technical Report No. ASD-TR-61-553, June 1962.

## 5.0 TELEMETRY RECEIVING SYSTEM CHARACTERIZATION

This section will discuss the performance characteristics of telemetry receiving and recording systems. The discussions will be brief and will include references to more detailed discussions. A simplified block diagram of a telemetry receiving and recording system is shown in figure 5.0-1.

### 5.0.1 Gain/System Noise Temperature (G/T)

The receiving system sensitivity is commonly specified as the system G/T. The G/T is usually obtained by measuring the power from a hot and a cold signal source. The sun is frequently used as the hot source ( $P_{\text{sun}}$ ) and the sky as the cold source ( $P_{\text{sky}}$ ). This technique is presented in IRIG document 118<sup>1</sup>. The system G/T is very useful for problem detection and link analysis. One equation for calculating the system G/T is:

$$G/T = 10 \log \left\{ \frac{8\pi k L P_r}{F \lambda^2} \right\}$$

where:

$k = 1.38 \times 10^{-23}$  watts/°K/Hz

$L = 1 + 0.38 (0.5 / \text{antenna half-power beamwidth in degrees})^2$

$P_r = (P_{\text{sun}} / P_{\text{sky}}) - 1$

$F$  = Solar flux at test frequency

$\lambda$  = Wavelength of test frequency in meters.

The aperture correction factor (L) used above is based on the use of a simultaneous lobing antenna. The solar flux is measured daily at 1415 ( $F_{1415}$ ) and 2695 ( $F_{2695}$ ) MHz along with several other frequencies. One can get the current solar flux values by calling AUTOVON 271-5871. There are several methods for estimating the flux at the test frequency from the measured flux at other frequencies<sup>1,2,3</sup>. The "best" estimate appears to be:

$$F = F_{2695} (F_{1415} / F_{2695})^\Gamma$$

where:

$$\Gamma = \frac{\log (f / 2695)}{\log (1415 / 2695)}$$

$f$  = Test frequency (MHz).

<sup>1</sup>Secretariat, Range Commanders Council, End-to-End Test Methods for Telemetry Systems, White Sands Missile Range, NM, RCC Document 118-79 Volume I.

<sup>2</sup>Hedeman, W. R. "The Sun as a Calibration Source for L- and S-band Telemetry", in Proceedings of the International Telemetry Conference, Vol. IV, pp. 330-342, 1977.

<sup>3</sup>Guidice D. A. and J. P. Castelli, "The Use of Extraterrestrial Radio Sources in the Measurement of Antenna Parameters", IEEE Transactions on Aerospace and Electronic Systems, Vol. AES-7 No. 2, March 1971.

If we measure the following values at a frequency of 2250.5 MHz:

$$P_{\text{sun}} = 100 \text{ microwatts}$$

$$P_{\text{sky}} = 4 \text{ microwatts}$$

and the solar flux values are:

$$F_{1415} = 60 \times 10^{-22} \quad \text{and} \quad F_{2695} = 80 \times 10^{-22} \text{ W/m}^2/\text{Hz}$$

then:

$$G/T = 10 \log \left\{ \frac{8 (3.1416) (1.38 \times 10^{-23}) (1.1) (100/4 - 1)}{80 \times 10^{-22} (60/80)^{0.28} (3.0 \times 10^8 / 2.2505 \times 10^9)^2} \right\}$$

$$G/T = 18.4 \text{ dB/}^\circ\text{K.}$$

The system sensitivity can also be determined by the use of a controlled source at a known distance. This method is not dependent on time of day.

#### 5.0.2 Bit Error Rate Testing

The performance of the telemetry receiving and recording system can be checked by performing a bit error rate (BER) test. This test consists of frequency or phase modulating an RF generator with the standard IRIG 2047 bit pseudo-random sequence. The RF generator output is either applied to the preamplifier or to a boresight tower. The RF power can be varied and the BER measured at the receiver and recorder outputs. The results can be compared to theoretical value and/or previous test results. This test is described in detail in IRIG Document 118 volume IV<sup>4</sup> chapter 2. This test is not sensitive to moderate levels of noise, spurious signals, intermodulation distortion, phase noise, or nonlinearities. It is sensitive to increases in system noise, improper system bandwidths, and equipment failures.

#### 5.0.3 Noise Power Ratio Testing

The performance of the telemetry receiving and recording system can also be checked by performing a noise power ratio (NPR) test. This test uses bandlimited noise to simulate an FM/FM multiplex. This test is also described in reference 4. The NPR test and some applications are also discussed in subsection 3.7. The NPR test is sensitive to moderate levels of noise, intermodulation distortion, phase noise, nonlinearities, spurious signals, improper bandwidths, and equipment failures.

<sup>4</sup>Secretariat, Range Commanders Council, Test Methods for Data Multiplex Equipment, White Sands Missile Range, NM, RCC Document 118-79 Volume IV.

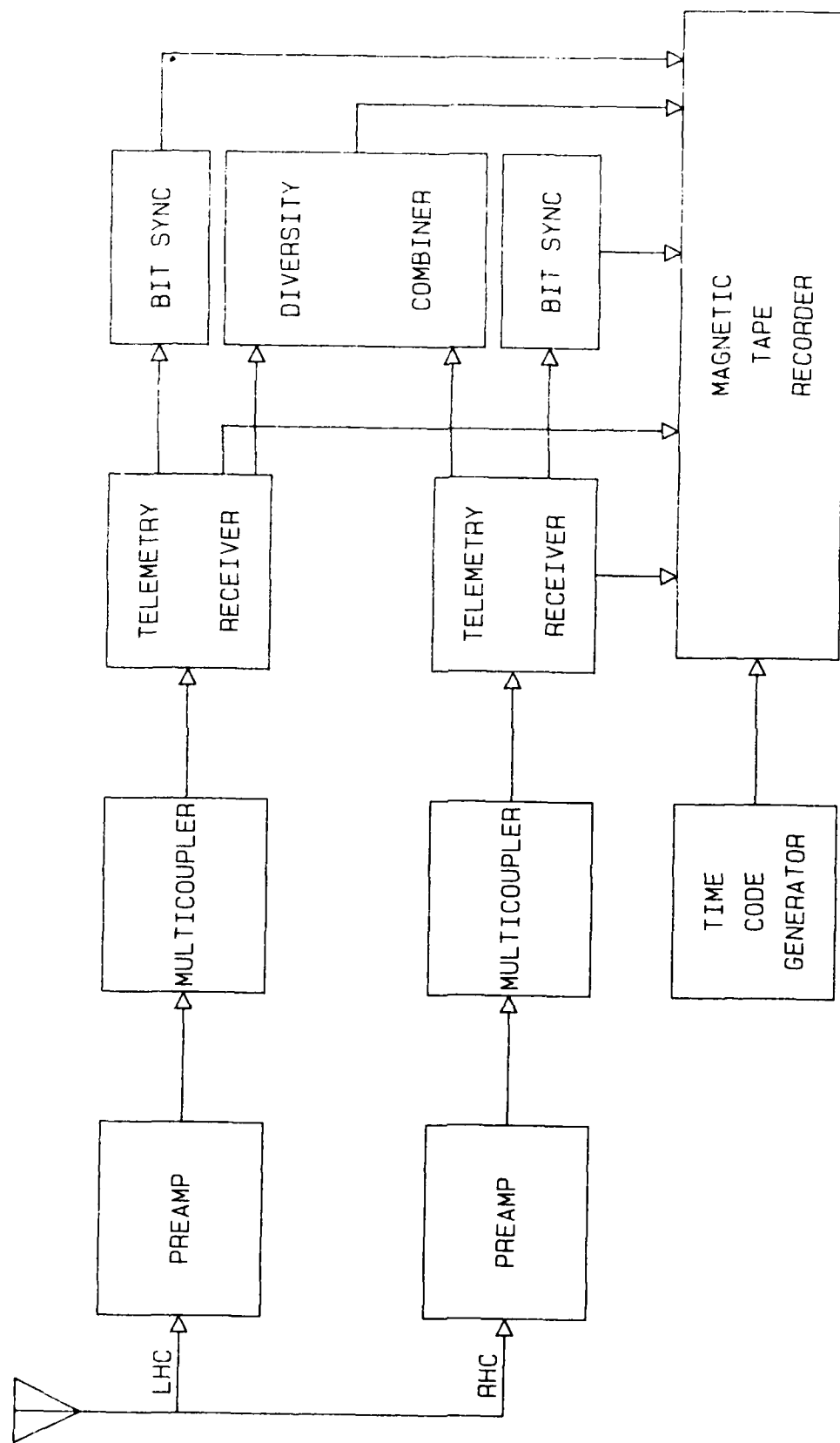


Figure 5.0-1. Simplified Telemetry Receive/Record Station.

## 5.1 RECEIVING ANTENNAS

The telemetry receiving antenna collects the impinging electromagnetic energy and makes it available for further processing. The important characteristics of a telemetry receiving antenna include: gain, beamwidth, frequency, polarization, sidelobe levels, tracking performance, and noise contribution.

### 5.1.1 Gain

The power gain of a parabolic dish telemetry receiving antenna can be approximated by<sup>5,6</sup>:

$$G = 0.5(\pi D/\lambda)^2$$

where:

D is the diameter of the antenna

D and  $\lambda$  are in the same units

the antenna efficiency is assumed to be 50 percent.

The approximate gain of an 8 foot dish at 2250 MHz would be:

$$G = 1654 \text{ or } 32.2 \text{ dBi.}$$

Gain is plotted as a function of diameter in figure 5.1-1.

### 5.1.2 Beamwidth

The 3-dB beamwidth (degrees) of an antenna can be approximated by<sup>5,6</sup>:

$$\Theta = 70\lambda/D.$$

This gives an approximate beamwidth of 3.8 degrees for an 8 foot dish at 2250 MHz. Beamwidth is plotted as a function of diameter in figure 5.1-2.

### 5.1.3 Noise Temperature

The noise temperature of a parabolic dish antenna at 2250 MHz varies from approximately 200 degrees Kelvin for a 0 degree elevation angle to as little as 10 degrees Kelvin at large elevation angles.

### 5.1.4 Polarization

Most telemetry receiving antenna systems are configured to receive two orthogonal polarizations. These polarizations are typically left- and right-hand circular or vertical and horizontal. Any set of two orthogonal polarizations contains all of the available power.

<sup>5</sup>Johnson, R. C., and H. Jasik *Antenna Engineering Handbook*, Second Edition, McGraw-Hill, New York, 1984.

<sup>6</sup>Stutzman, W. L., and G. A. Thiele *Antenna Theory and Design* John Wiley, New York, 1981.

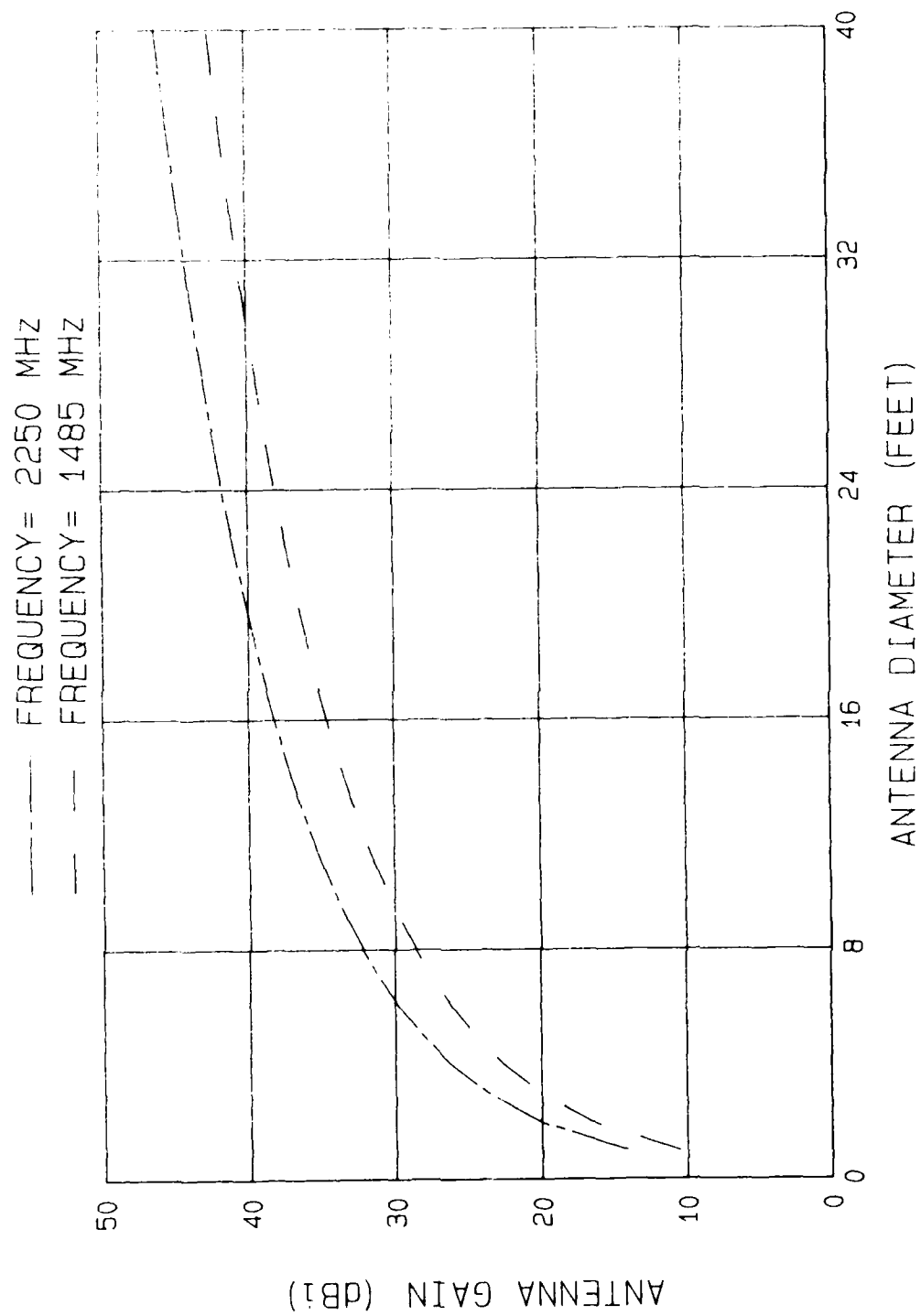


Figure 5.1-1. Antenna Gain Versus Diameter (50% Efficiency)

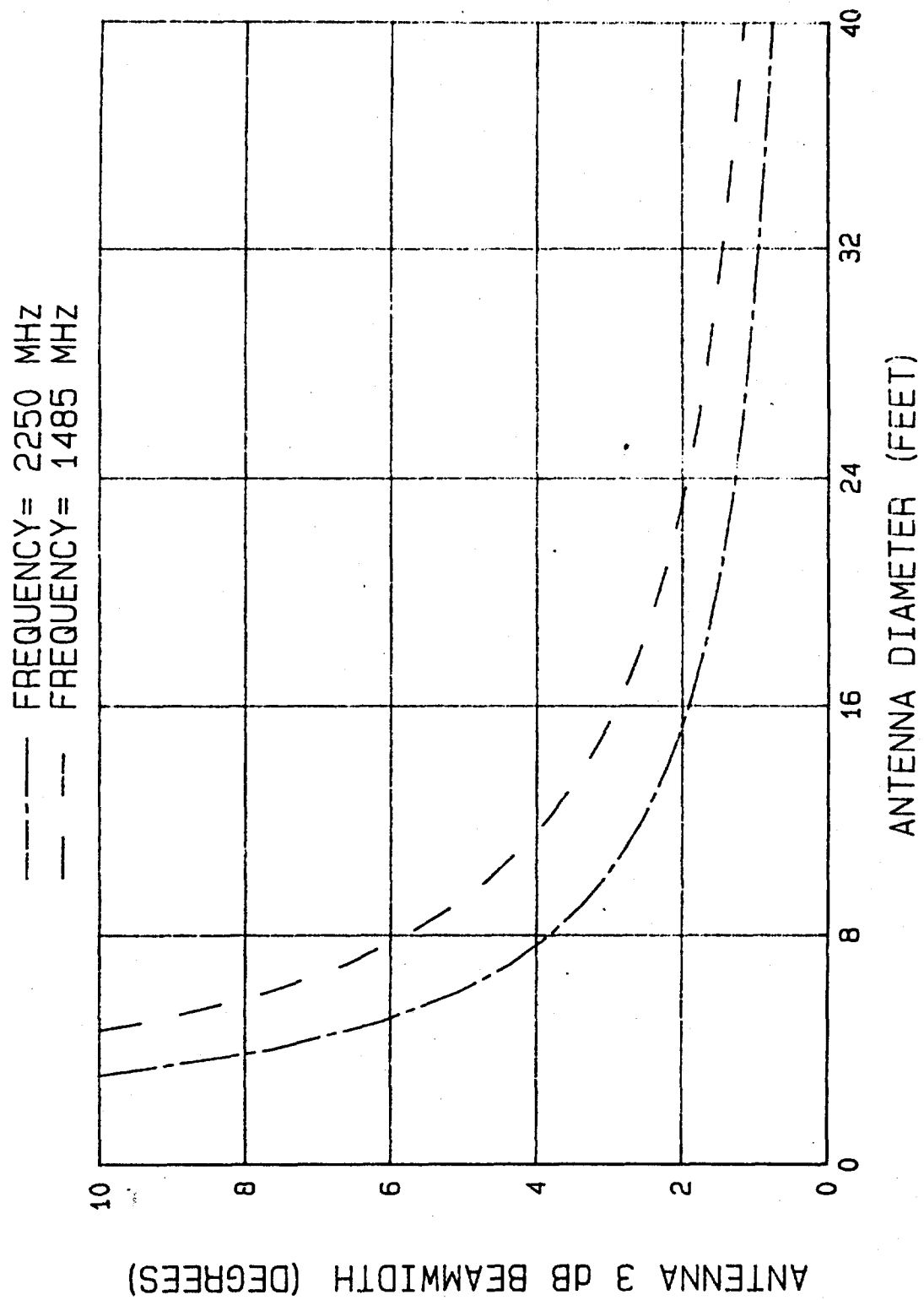


Figure 5.1-2. Antenna Beamwidth Versus Diameter (50% Efficiency)



## 5.2 PREAMPLIFIERS, DOWNCONVERTERS, and MULTICOUPLERS

### 5.2.1 Preamplifier

The purpose of the preamplifier is to amplify the signals received by the antenna while adding as little extra noise as possible. Therefore, the preamplifier should be mounted very near the antenna to minimize attenuation prior to amplification. The noise temperature (noise figure) of the preamplifier should be low to minimize the noise power. System noise temperatures are often specified at the preamplifier input. The preamplifier is often preceded by a bandpass filter and/or limiter to minimize the interference from strong out-of-band signals. A directional coupler is also frequently placed in front of the preamplifier to allow test signals to be injected at the preamplifier input.

### 5.2.2 Noise Figure/Noise Temperature

The noise figure (F) is a measure of the noise added by a device. It is defined<sup>7,8,9</sup> as the ratio of total output noise to output noise due only to input noise when the input source is at a specified temperature of 290 °K.

$$F = 1 + T_e/290$$

$$F \text{ (dB)} = 10 \log (1 + T_e/290)$$

where  $T_e$  is the effective noise temperature of the device.

The noise figure (dB) of a lossy cable at room temperature is equal to the cable loss (dB). Therefore, a cable with 1 dB attenuation has an effective noise temperature of  $(10^{0.1} - 1) 290 = 75$  °K when the cable is at a temperature of 290 °K. If the cable is at a different temperature, the noise temperature is calculated by replacing 290 by the actual cable temperature.

If we have a signal passing through a series of devices each with a separate gain  $G_i$ , noise figure  $F_i$ , and noise temperature  $T_{ei}$ , the overall noise figure and temperature are:

$$F = F_1 + (F_2 - 1)/G_1 + (F_3 - 1)/G_1 G_2 + \dots$$

$$T_e = T_{e1} + T_{e2}/G_1 + T_{e3}/G_1 G_2 + \dots$$

<sup>7</sup>Pettai, R. *Noise in Receiving Systems*. Wiley, New York, 1984.

<sup>8</sup>Gregg, W. D. *Analog and Digital Communication*. Wiley, New York, 1977.

<sup>9</sup>Gagliardi, R. M. *Introduction to Communications Engineering*. Wiley, New York, 1978.

As an example let us analyze the system shown in figure 5.2-1. We will use the preamplifier input as our reference point. We can combine the bandpass filter (BPF), directional coupler, and cable losses together to get a loss of 0.9 dB before the preamplifier.

Antenna:  $T_A = 70 \text{ }^\circ\text{K}$   
 BPF, directional coupler, cable:  $F_1 = 0.9 \text{ dB} = 1.23$      $G_1 = 0.81$   
 Preamplifier:  $F_2 = 1.0 \text{ dB} = 1.26$      $G_2 = 1000$   
 Cable:  $F_3 = 12 \text{ dB} = 15.85$      $G_3 = 0.063$   
 Receiver:  $F_4 = 9 \text{ dB} = 7.94$

We can calculate the equivalent system noise temperature as follows:

$$\begin{aligned} T_1 &= (1.23 - 1) 300 = 69.0 \text{ }^\circ\text{K} \\ T_2 &= (1.26 - 1) 290 = 75.4 \text{ }^\circ\text{K} \\ T_3 &= (15.85 - 1) 290 = 4306.5 \text{ }^\circ\text{K} \\ T_4 &= (7.94 - 1) 290 = 2012.6 \text{ }^\circ\text{K} \end{aligned}$$

$$T_{\text{system}} = 70/1.23 + 69.0/1.23 + 75.4 + 4306.5/1000 + 2012.6/63$$

$$T_{\text{system}} = 56.9 + 56.1 + 75.4 + 4.3 + 31.9 = 224.6 \text{ }^\circ\text{K}.$$

The system noise temperature can be changed by varying the gain and/or noise temperature of the system components. Increasing the noise figure of the receiver to 12 dB would increase the system noise temperature by 36 degrees and reduce the sensitivity by 0.6 dB. Increasing the gain of the preamplifier by 6 dB would decrease the system noise temperature by 27 degrees and increase the sensitivity by 0.6 dB. Decreasing the loss before the preamplifier by 0.2 dB would decrease the noise temperature by 10 degrees and increase the sensitivity by 0.4 dB ( 0.2 dB due to less noise and 0.2 dB due to more signal).

If we assume the antenna gain is 32.2 dBi, the system G/T can be calculated from the ratio of the effective signal gain at the preamplifier input to the effective system noise temperature at the preamplifier input:

$$G/T = (32.2 - 0.9) - 10 \log (224.6)$$

$$G/T = 7.8 \text{ dB/}^\circ\text{K}.$$

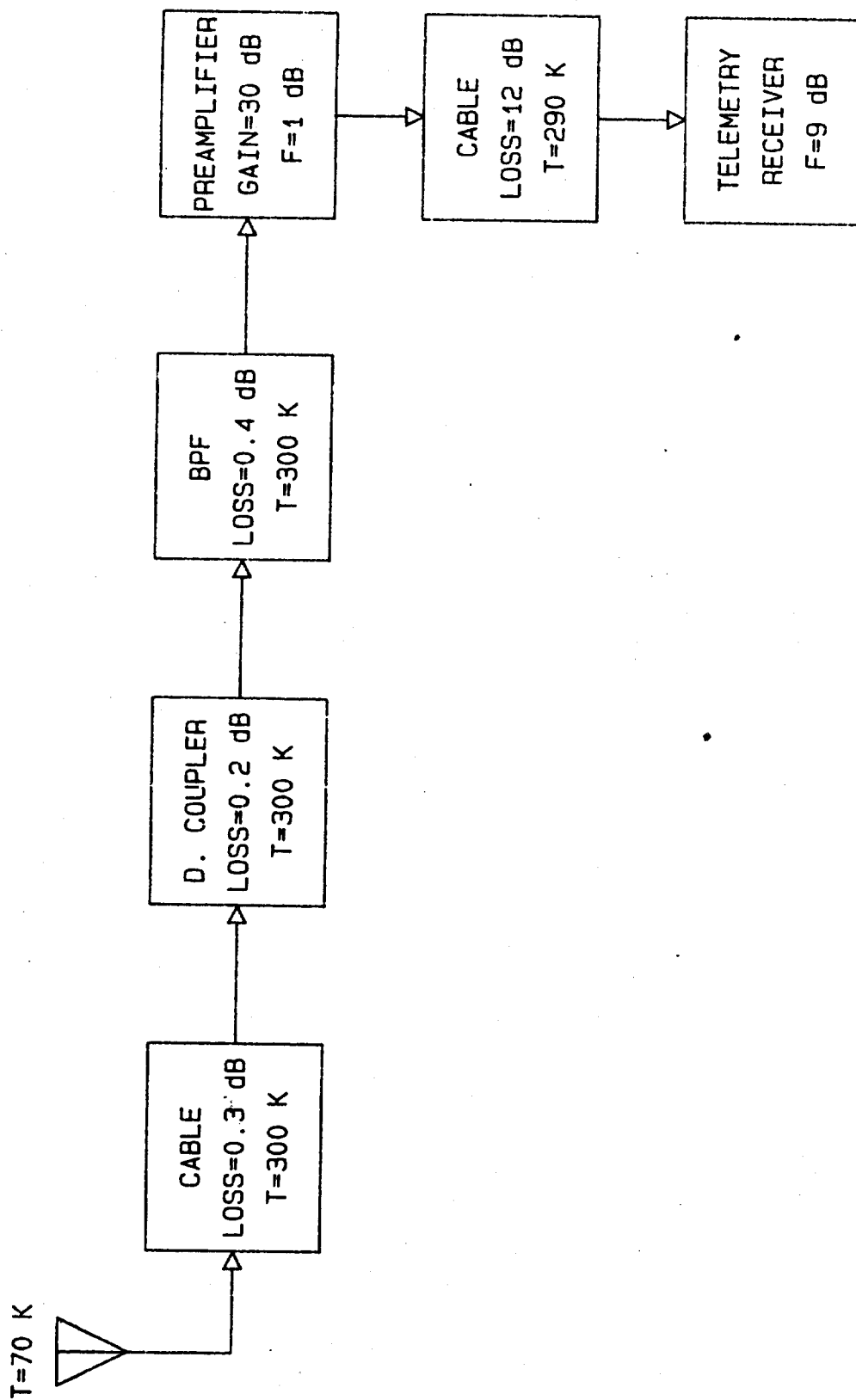


Figure 5.2-1. Receiving System Noise Temperature.

### 5.2.3 Downconverter

The purpose of the downconverter is to translate the input signal to a lower frequency. A typical example is to translate the 2200 to 2300 MHz band to 215 to 315 MHz. This is useful because it reduces the cable loss (dB) by a factor of approximately 3. Telemetry signals are currently transmitted in four separate bands 1435 to 1540 MHz, 1700 to 1850 MHz, 2200 to 2300 MHz, and 2310 to 2390 MHz. If the signals are all downconverted to 215 to 320 MHz, then a single receiver tuner can be used for all four telemetry bands. The disadvantage is that a separate cable is needed for each frequency band after the downconverter. The important parameters include: noise figure, VSWR, gain, 1 dB gain compression point, 60 dB intermodulation distortion point, bandwidth, gain, and local oscillator stability, accuracy, and phase noise.

### 5.2.4 Multicoupler

The purpose of the multicoupler is to provide several, isolated outputs from one input. This allows one RF signal to be applied to several receivers. These receivers can be redundantly receiving one signal or be tuned to several frequencies. The important parameters include: noise figure, VSWR, 1 dB gain compression point, 60 dB intermodulation distortion point, bandwidth, gain, and isolation between outputs.

## 5.3 TELEMETRY RECEIVERS AND DIVERSITY COMBINERS

### 5.3.1 Introduction

A telemetry receiver takes an incoming radio frequency (RF) signal and translates the desired portion of the spectrum to a lower frequency. This lower frequency is called the final intermediate frequency (IF) frequency. Most telemetry receivers include 2 or 3 stages of frequency translation. The multiple stages make it easier to reject image and spurious signals. The receiver final IF output frequency is typically 10 or 20 MHz (some receivers use a 70 MHz final IF frequency). This signal is then routed to a demodulator (FM, AM, PM, or PSK), a predetection downconverter, and frequently a diversity combiner. The demodulated and/or predetection signals are recorded on magnetic tape and also sent to the data processing and display facility.

The important characteristics of a telemetry receiver include:

1. Frequency accuracy, stability, and phase noise.
2. Noise figure
3. Overall amplitude and phase response
4. Spurious and image rejection
5. Automatic gain control (AGC) linearity, stability, and transient response
6. Demodulator linearity, stability, acquisition time, and noise performance.

Diversity signal combining is a method of "adding" 2 or more independent signals. The most common type of diversity in telemetry signals is polarization diversity. Most telemetry receiving antennas have 2 independent outputs, usually left- and right-hand circular polarization or horizontal and vertical polarization. A properly aligned predetection polarization diversity combiner will allow the receiving system to perfectly match the polarization of the incoming signal. Another common type of telemetry diversity is space diversity. This involves the use of 2 or more separate telemetry antennas. The signals from these antennas are typically selected rather than combined because of the problems encountered in keeping the signals time aligned. Space diversity is especially helpful when multipath or flame attenuation is encountered. Other types of diversity include frequency and time diversity.

The two types of telemetry combiners are predetection combiners and postdetection combiners. A predetection polarization diversity combiner must phase align the input signals and then weight the signals proportionally to the ratio of the signal to mean square noise in each channel. A postdetection polarization diversity combiner does not have to phase align the signals.

However, the signals still need to be time aligned. Most telemetry combiners weight the signals based on the receiver AGC voltages. A wideband AM signal can be summed with the AGC signal<sup>10</sup> to improve performance when the RF signal fluctuates in amplitude rapidly. Another method of combiner weighting is to use detected noise to weight the channels.

### 5.3.2 Receiver Noise Figure

The receiver is usually preceded by amplifiers with low noise figures. As long as the net gain between the input to the first amplifier and the input to the receiver is large, the effect of the receiver noise figure is small because the receiver noise contribution is proportional to the receiver noise temperature divided by the net power gain. Typical receiver noise figures vary from 6 to 12 dB.

### 5.3.3 Receiver Local Oscillators

Most new telemetry receivers include synthesized local oscillators. This usually means that the receiver's frequency accuracy and stability versus time and temperature is good (provided that the basic crystal does not drift). Frequency synthesizers can have problems with phase noise and spurious signals. These problems can usually be detected by monitoring the local oscillator output using a spectrum analyzer.

### 5.3.4 Receiver IF and Video Filters

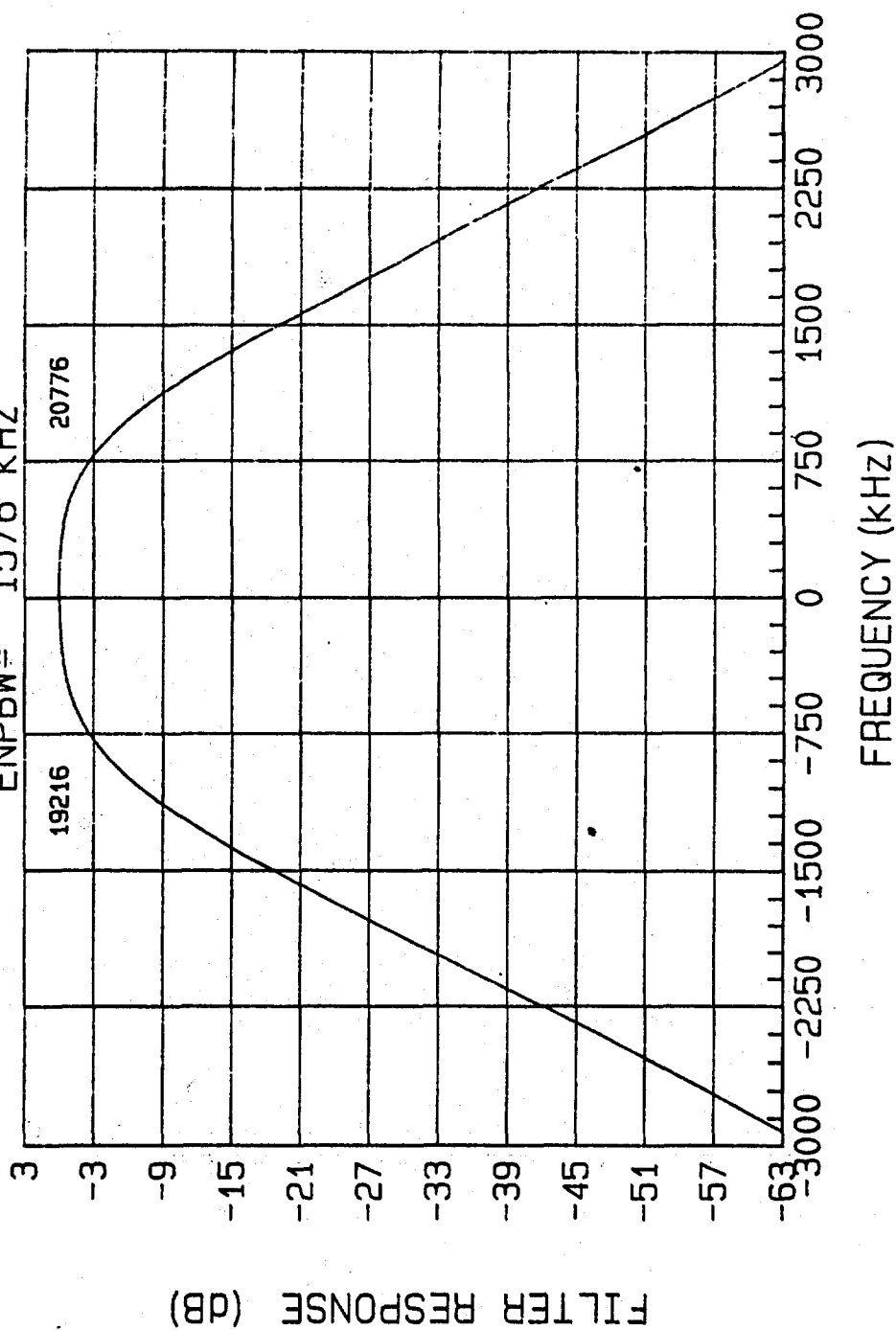
The overall frequency and phase response of the receiver predetection and video outputs are largely determined by the IF bandpass filters and the lowpass filters at the video and predetection outputs. The step response of linear phase filters is better than that of maximally flat amplitude response filters. This is especially important when receiving signals with baseband PAM. Most receiver IF and video filter bandwidths are available with only a few fixed bandwidths. The standard IRIG bandwidths are: 300, 500, 750, 1000, 1500, 2400, 3300, 4000, 6000, and 10,000 kHz. A few narrower bandwidths are listed in the Telemetry Standards but they are rarely used for receiving data. All IF bandwidths are probably not available at one receiving site. The "best" choices of receiver bandwidths for various received signals are discussed in section 3 of this handbook. A sample receiver IF filter amplitude versus frequency response is shown in figure 5.3-1. The output amplitude rolls off rapidly outside of the 3 dB passband.

### 5.3.5 AGC Time Constant

The receiver AGC time constant for data receivers should be the fastest available (usually 0.1 ms). Fast AGC time constants minimize the amount of time the receiver is captured by noise during signal fades and saturated during signal increases. There do not seem to be any disadvantages of fast AGC time constants for data receivers (receiver assumed to be stable for all available time constants).

<sup>10</sup>Hill, E.R. "AM/AGC Weighted Pre-Detection Diversity Combining," in *Proceedings of International Telemetry Conference*, Vol. 13, pp 215-238, Oct. 1977.

FILTER SETTING= 1500.0 KHZ  
 3 dB BW= 1560 KHZ  
 ENPBW= 1576 KHZ



CENTER FREQUENCY= 20000.6 KHZ

Figure 5.3-1. Sample Receiver IF Filter Amplitude Response.

### **5.3.6 Demodulator Loop Bandwidth (PM and PSK)**

The best loop bandwidth is a function of expected fade rate, frequency stability, and data rate. If flame attenuation is expected, a relatively wide loop bandwidth should be used, e.g., 10 kHz. The disadvantage of wide loop bandwidths is that a higher IF SNR is required to keep the loop in lock. If the signal is predetection recorded, the loop bandwidth can be varied in post-flight mode to recover the maximum amount of data.

### **5.3.7 Automatic Frequency Control (AFC)**

The receiver AFC circuit attempts to keep the incoming signal centered within the receiver passband. However, using AFC at low IF SNRs usually degrades the data quality. Another problem with AFC occurs when two receivers with independent local oscillators in AFC mode are used with a predetection combiner. The AFC circuits introduce excess phase modulation which the combiner phase-locked loop (PLL) has difficulty tracking.

### **5.3.8 Predetection Carrier**

The predetection carrier signal is a replica of the RF signal which has been bandpass filtered and translated to a lower frequency. The predetection carrier is mainly used to record a replica of the transmitted signal with the least processing before recording. This allows the data reduction center to modify bandwidth and demodulator parameters to attempt to improve data quality. Once the data has been demodulated using less than optimum parameters it is usually impossible to correct the degradation! One example of this is the use of a PM demodulator loop bandwidth that is too wide to track the incidental phase changes which occur during a mission. Each time the demodulator loses lock the data will be useless until lock is reacquired. Therefore, predetection recording is often specified by the data users. The IRIG 106-86 standard predetection carrier center frequencies are: 112.5, 150, 225, 300, 450, 600, 900, 1200, 1800, and 2400 kHz. Normally, frequencies of 450 kHz and higher are used. The receiver IF bandwidth should be less than or equal to twice the predetection carrier center frequency. The disadvantage of predetection recording is that it requires at least twice the bandwidth of baseband recording techniques. This is a problem for missions that last a long time and missions with wide data bandwidths. The preferred method of demodulation is to use an upconverter and playback receiver. Unfortunately, this hardware is not available at many telemetry data reduction centers. These centers usually use tuneable discriminators. These discriminators have less frequency response capability than playback receivers plus their bandpass filter response characteristics are often not very good.

### **5.3.9 Pop Noise Symmetry**

Pop noise is discussed in subsection 3.11 of this handbook. If the receiver is improperly tuned or the IF filter characteristic is non-symmetrical the pop noise will be non-symmetrical.

### **5.3.10 Signal Strength**

The receiver AGC voltages are linearly related to input signal power from approximately a +6 dB SNR (lower if a synchronous detector is used) to a high signal level. If the AGC voltages are properly calibrated, they provide a good indication of the received SNR at a given time. Since the AGC system responds to



power at the receiver input rather than to SNR, the AGC signal is only a relative measure of SNR until it is calibrated. Many receiver AGC systems tend to be influenced by temperature. Therefore, the AGCs are not stable until the receiver temperature stabilizes. The AGC signals are typically used as weighting signals for diversity combiners and as inputs to antenna tracking systems. In addition, the AGC signals are usually FM multiplexed with the timing and voice signals and recorded on the magnetic tape along with the telemetry data.

### 5.3.11 Diversity Combining

An optimal ratio diversity predetection combiner has a theoretical output SNR (power ratio) equal to the sum of the input SNRs (expressed as power ratios). This improvement results from adding the signals coherently while adding the noise non-coherently. The theoretical improvement that can be achieved by an optimal ratio predetection combiner relative to the best input signal is shown in figure 5.3-2 for differences in input SNR between 0 and 10 dB. The theoretical improvement that can be achieved by an optimal ratio predetection combiner relative to a given fixed input signal is shown in figure 5.3-3 for the independent signal varying from 10 dB worse than the reference to 10 dB better than the reference. A properly designed and aligned predetection combiner used with a properly matched receiving system performs very close to the theoretical limit. However, the AGC systems in many telemetry receivers tend to change with receiver temperature and tuning frequency. Therefore, the combiner and the receiving system need to be carefully aligned for optimum performance. The degradation from optimum performance for a 3 dB weighting error is shown in figure 5.3-4. This data shows that 0.5 dB is the maximum degradation from optimum with a 3 dB weighting error. The maximum degradation with a 6 dB weighting error is 2 dB. The degradation from optimum performance for phase alignment errors between 0 and 90 degrees is shown in figure 5.3-5. The degradation is approximately 0.5 dB with a 40 degree misalignment and 3 dB with a 90 degree misalignment.

A two channel polarization diversity combiner can offer more than 3 dB of improvement relative to one of the incoming polarizations. The amount of improvement depends on the transmitting antenna design and the aspect angle between antennas. Typical values<sup>11</sup> for circular polarization reception and random aspect angles are shown in table 5.3-1.

**Table 5.3-1. Typical improvement of polarization diversity compared to single channel for missile antennas.**

<u>Percent Coverage</u>	<u>Improvement over single channel (dB)</u>
50	3
90	5
95	7
99	9

<sup>11</sup>Berns, K.L. "Benefits of Polarization Diversity Reception," in *Proceedings of International Telemetry Conference*, Vol. 20, pp 627-642, Oct. 1984.

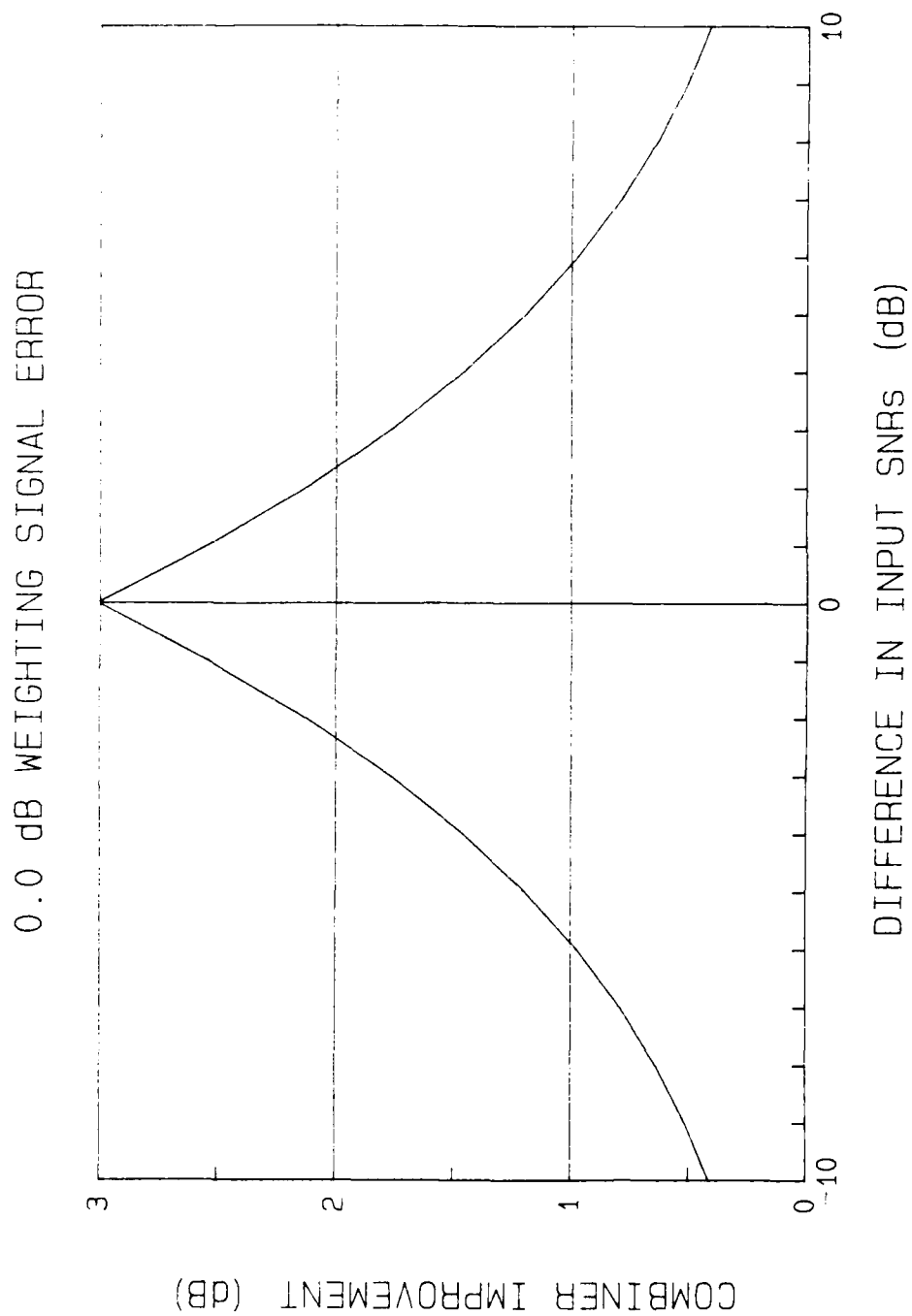


Figure 5.3-2. Combiner Improvement Relative to Best Input Signal.

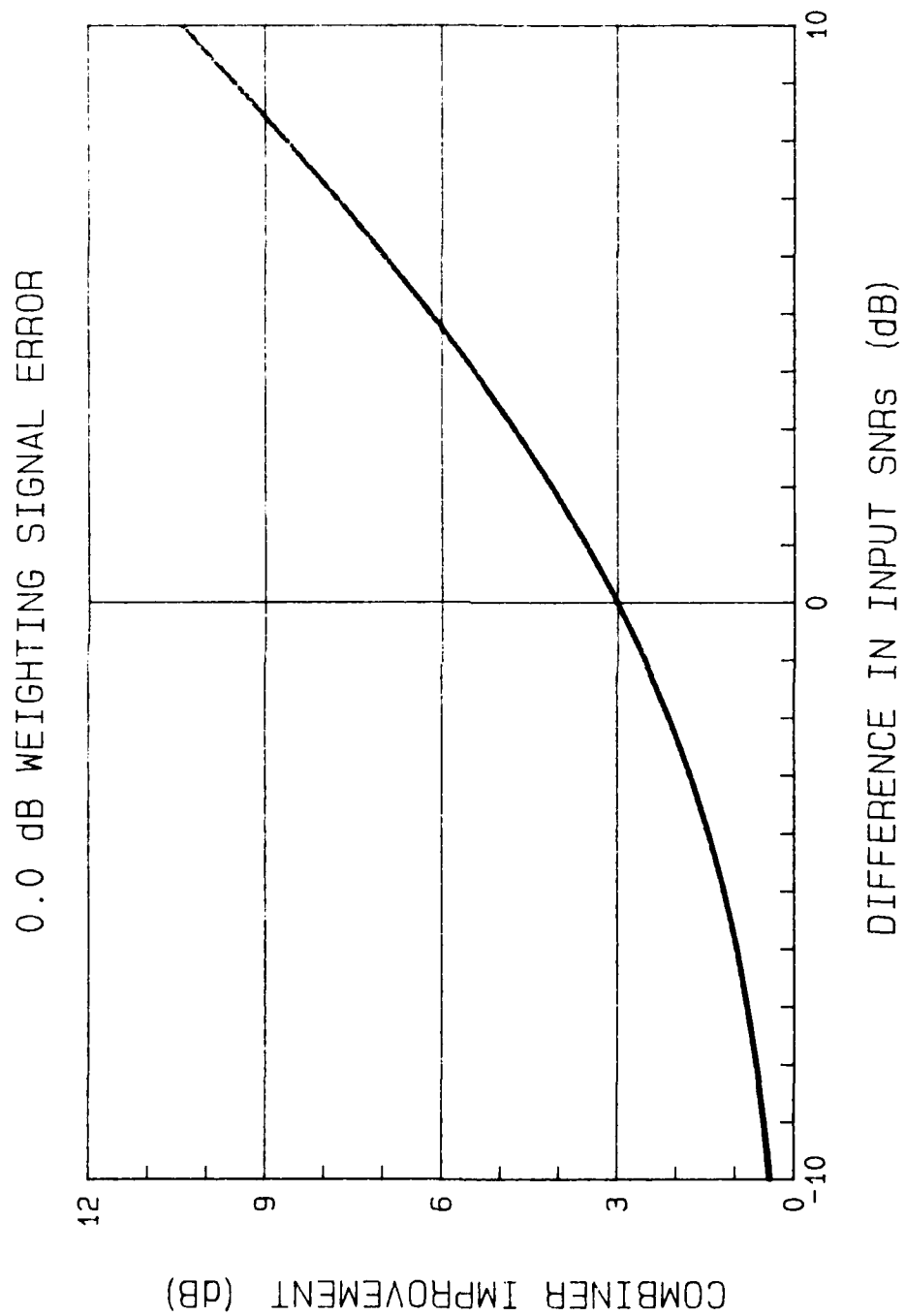


Figure 5.3-3. Combiner Improvement Relative to Fixed Input Signal.

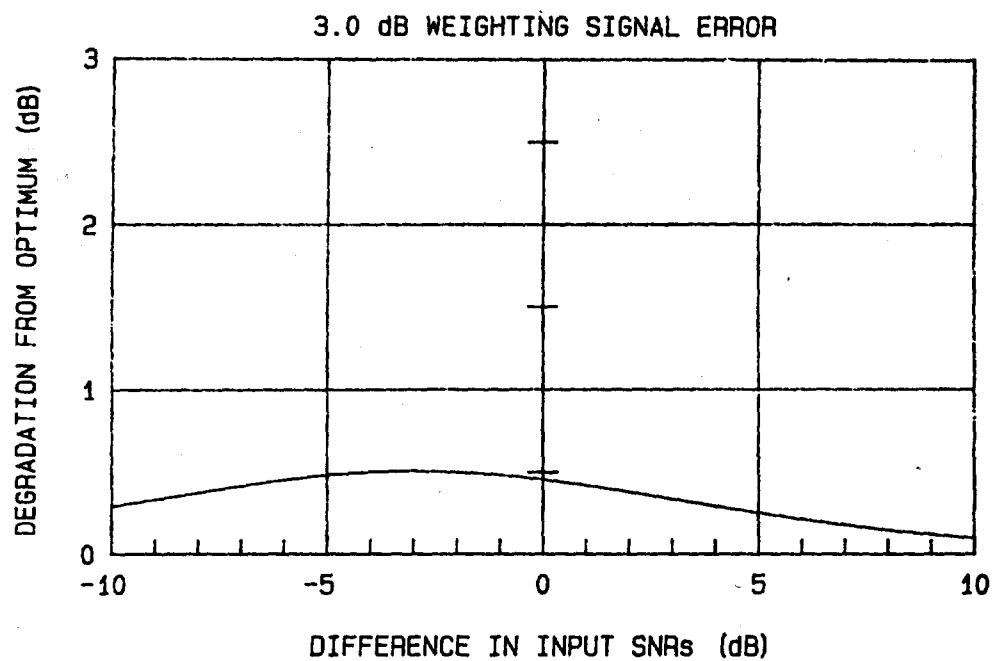


Figure 5.3-4. Combiner Degradation from Optimum with 3 dB Weighting Error.

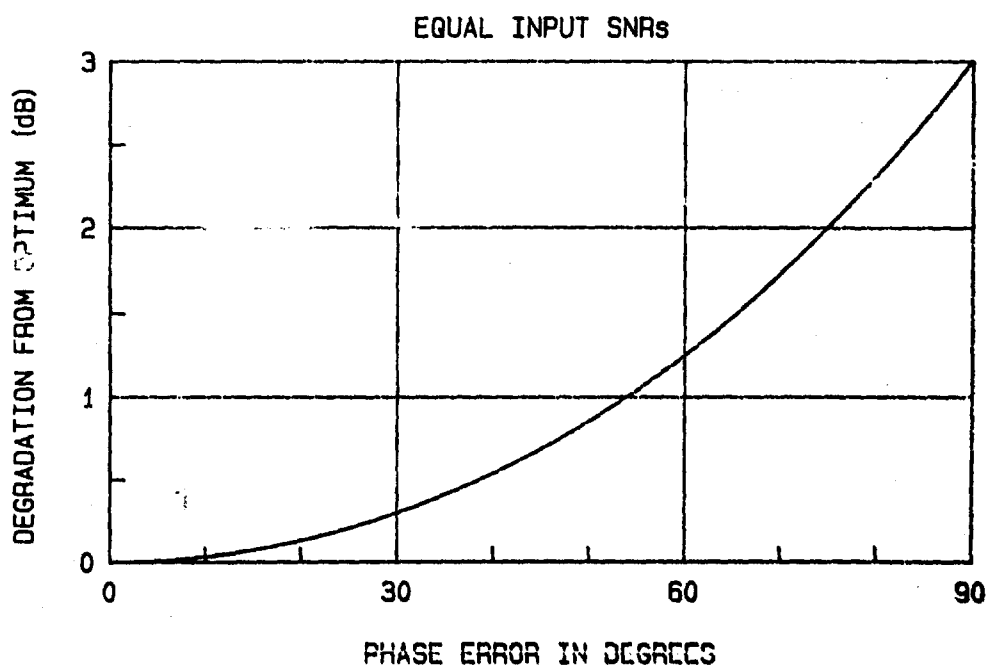


Figure 5.3-5. Combiner Degradation from Optimum Versus Phase Error.

Percent coverage refers to the percentage of the sphere around the antenna where a certain gain is equaled or exceeded. The data in table 5.3-1 shows that 50% of the time the combined output would be at least 3 dB better than a given channel. The data also shows that 1% of the time the improvement will be at least 9 dB. In other words, 99% of the time the improvement will be less than 9 dB. Another way of stating this is that if we want good data 99% of the time the use of optimal ratio predetection combining versus using only one polarization (not selecting the the best), can increase the link margin by 9 dB. Table 5.3-1 only includes effects due to transmitting antenna pattern polarization. The effects of multipath, ducting, flame attenuation, etc. are not included in table 5.3-1.

#### 5.3.12 Diversity Combining of PCM/FM Signals

Predetection combining works well for PCM/FM signals as long as the combiner phase-lock loop (PLL) can properly align the IF signals. The major sources of PLL problems are:

1. Telemetry receivers in AFC mode with independent local oscillator
2. The frequency difference between the IF signals may be too large for the phase-lock loop to attain lock.

Therefore, AFC should not be used with predetection combining and the receivers should be operated from a common local oscillator if possible.

Postdetection combining does not work as well as predetection combining for PCM/FM. The basic problem is that most of the bit errors in a near optimum PCM/FM system are caused by "pop" noise. An unfiltered pop has an area equal to one cycle. The area of an unfiltered PCM bit with peak deviation equal to 0.35 times the bit rate is 0.35 cycle. Therefore, the sum of two unfiltered bits is less than the amplitude of an unfiltered noise pop. The BER at the postdetection combined output is approximately equal to the BER of the best input channel. Therefore, its performance is like that of a selector rather than an optimal ratio combiner.

#### 5.3.13 Diversity Combining of PCM/PM Signals

Both predetection and postdetection combining work well for PCM/PM with carrier tracking demodulators as long as the demodulator is locked to the carrier. Predetection combining also works well for carrier reconstruction demodulators (Costas loop, squaring loop, etc) as long as the demodulator is locked to the input signal. Postdetection combining can not be used with carrier reconstruction demodulators unless an automatic polarity alignment circuit is added to the combiner to correct for the polarity uncertainty at the demodulator output. Without this circuit, the combiner could add two signals with opposite polarity and produce only noise at the output.

## 5.4 MAGNETIC TAPE RECORDERS/REPRODUCERS

### 5.4.1 Introduction

The purpose of this section is to discuss the important functions of the recorder/reproducer system in storing telemetry data for non-real time data processing operations. The characteristics of magnetic recording systems are discussed in references 12 through 19. The requirement to store telemetry data occurs frequently because: data rates may be too high to be processed in real time, data is recorded at a remote receiving site and relayed to a central processing site, detailed post-flight analysis is required for certain portions of mission data, there are shortages of data processing equipment and/or technical personnel, and there is a requirement to provide data for archival storage. The performance functions to be discussed include: amplitude and phase response, noise power spectral density, intermodulation distortion, signal-to-noise ratio (SNR), harmonic distortion, cross-talk, and the effects caused by tape speed variations. Consideration is also given to FM, direct, predetection and post-detection recording techniques, and the accepted head and tape handling practices. It is assumed during these discussions that all standard conditions, test methods, and measurement procedures of the IRIG documents 106-xx and 118-xx are adhered to in the selection of the recorder/reproducer system and in its alignment.

<sup>12</sup>Secretariat, Range Commanders Council. Telemetry Standards. White Sands Missile Range, NM, RCC, May 1986. (IRIG Standard 106-86).

<sup>13</sup>Jorgensen, F. The Complete Handbook of Magnetic Recording. TAB Books, Blue Ridge Summit, PA, 1980.

<sup>14</sup>Camras, M. Magnetic Tape Recording. Van Nostrand, New York, 1985.

<sup>15</sup>White, R. Introduction to Magnetic Recording. IEEE Press, New York, 1984

<sup>16</sup>Daniel, E. D. and C. D. Mee, Eds. Magnetic Recording-vol. I: Technology. McGraw-Hill, New York, 1986.

<sup>17</sup>Mee, C. D. and E. D. Daniel, Eds. Magnetic Recording-vol. II: Applications. McGraw-Hill, New York, 1987.

<sup>18</sup>Mallinson, J. C. Foundations of Magnetic Recording. Academic Press, Orlando, FL, 1987.

<sup>19</sup>Proceedings of the IEEE, November 1986.

A recapitulation of terms and parameters from the IRIG Telemetry Standards is given to alert operator awareness to the necessary considerations which must be made when using a recorder/reproducer system in the telemetry link.

1. Recorder/reproducer systems are classified by bandwidth. Intermediate bandwidth systems provide a maximum frequency response of 600 kHz at a tape speed of 60 IPS, wideband systems provide a maximum frequency response of 4.0 MHz at a tape speed of 240 IPS, and double density systems provide a maximum frequency response of 4.0 MHz at a tape speed of 120 IPS.

2. Recording methods are classified by the method which is used to put the information signal onto the magnetic tape. Direct recording is accomplished by adding a high frequency bias signal to the information signal at the record head before storage on the magnetic tape. FM recording is accomplished by applying an information signal to a subcarrier oscillator whose modulated output is applied to the record head. When using this method of recording, the high frequency bias signal may or may not be injected to the record head.

3. Record/reproduce signal levels and input/output impedances are important requirements to maintaining expected system performance. IRIG 106-86 states the recorder input and output impedances for all three classes of systems shall be 75 ohms nominal at all frequencies in the passband. However, some installations have a preference for 50 ohm outputs. In any event, it is highly advisable to pay attention to these impedances, especially when using long coaxial cables carrying high frequency signals.

4. Predetection recording (Pre-D) is the process of recording telemetry data signals prior to detection. In general, the practice involves heterodyning the output of the final IF in the receiver/combiner to a carrier frequency which falls within the passband of the recorder/reproducer system. The standard predetection carrier center frequencies vary from 112.5 to 2400 kHz. The heterodyned center frequency containing the data multiplex may then be "direct" recorded on the recorder/reproducer system. The purpose of recording the transmitted telemetry data multiplex in this manner is that it allows the opportunity to select optimum characteristics for the type of detector, signal conditioners, and other data processing equipments to provide the highest quality data in non-real time operations.

5. Post-detection (Post-D) recording is the process of recording received telemetry data signals after "detection" in the receiver system. It involves the recording of the raw telemetry signal before or after signal conditioning, including bit synchronization, and recording is done in the FM or direct record modes of operation; thus eliminating the need for heterodyning as in the Pre-D recording process. FM recording is used when a DC or very low frequency needs to be recorded and reproduced accurately. Post-detection direct recording is used with signals which do not have important information at frequencies below the reproduce system low frequency cutoff.

#### 5.4.2 Head Segment Gap Azimuth

This is defined in IRIG 106 (Telemetry Standards) as the angle formed in the plane of the tape between a line perpendicular to the head reference plane and a line parallel to the trailing edge of the record head segment gap or parallel to the center line of the reproduce head segment gap. The azimuth should always be peaked on the prime data track that you are playing back. All tracks are supposed to be within 2 dB of each other but they may not be! The problem that misadjusted azimuth creates is shown in figure 5.4-1. The reproduce gap segment was modelled as four separate segments (slanted line crossing the four signals). The output signal is the sum of the signals in each segment. As the frequency increases the phase differences along the gap increase. This causes the output signal to decrease in amplitude. The azimuth loss can be calculated using:

$$\text{azimuth loss} = 20 \log ((\sin x)/x)$$

where:

$$\begin{aligned} x &= (\pi w \tan \alpha) / \lambda \quad (\text{radians}) \\ w &= \text{width of recorded track} \\ \alpha &= \text{angle of misalignment} \\ \lambda &= \text{wavelength of recorded signal.} \end{aligned}$$

If we assume that the track width is 50 mils, the angle of misalignment is 1 minute of arc, and the wavelength is 60 microinches we get an azimuth loss of 0.85 dB. If we increase the angle of misalignment to 2 minutes of arc we get a loss of 3.6 dB. If we now decrease the wavelength to 30 microinches (double density recording) we get an azimuth loss of 29.3 dB. We can decrease this loss to 3.6 dB by decreasing the track width to 25 mils. The azimuth loss is a function of the product of the track width in inches and the azimuth error in radians divided by the wavelength in inches. When this term is approximately equal to 1.39 the azimuth loss is 3 dB. When this term is approximately 0.82 the azimuth loss is 1 dB. The azimuth loss for a 50 mil track width with 2 and 4 minutes of azimuth error is plotted in figure 5.4-2 as a function of frequency.

Azimuth alignment between reproduce head and the signal recorded on tape is extremely important in achieving full system response and in establishing cross play capability between different systems. Optimum frequency response and system to system compatibility can only be achieved when these alignments are maintained in accordance with the IRIG Telemetry Standards and monitored diligently. Misalignment of azimuth can significantly degrade system frequency response and subsequently data quality. A common practice is to align the reproduce head azimuth to produce the highest amplitude, of an upper bandedge signal, at the reproducer output. Some recorder/reproducer systems also have azimuth adjustable record heads; great caution must be exercised when adjusting the azimuth of the record heads so as not to destroy the alignment compatibility between different recorder/reproducer systems.

The correct azimuth alignment of the record head is a very important requirement to achieving system to system compatibility. Many recorder/reproducer manufacturers provide precision fixed mounting plates for the record heads; they do not include an adjustment for azimuth alignment by station operators. However, some systems do have external azimuth alignment adjustments accessible to station operators. Great caution must be exercised with those systems having external record head azimuth adjustments or system to system compatibility can and will be degraded or destroyed completely. The procedure to follow for correctly adjusting the azimuth alignment



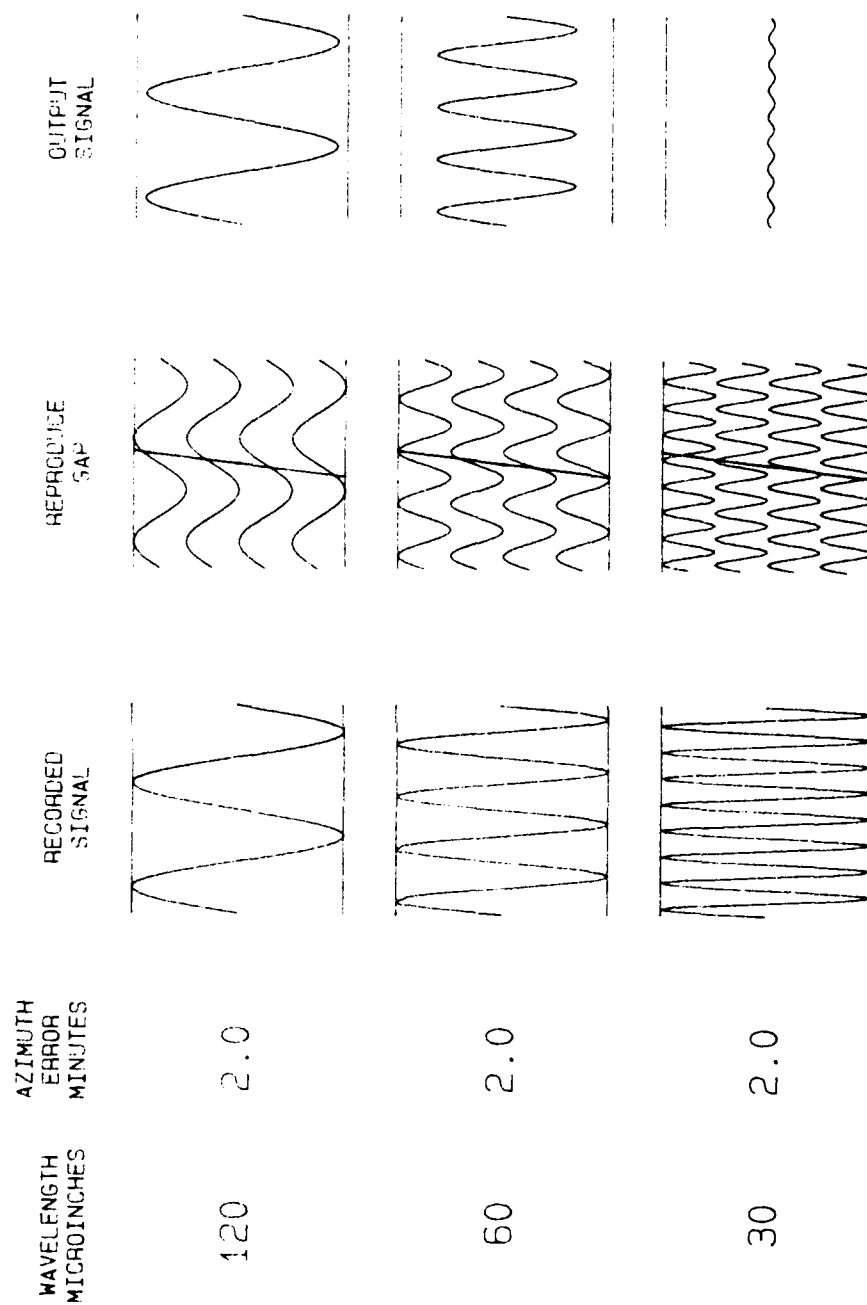


Figure 5.4-1. Azimuth Error Illustration.

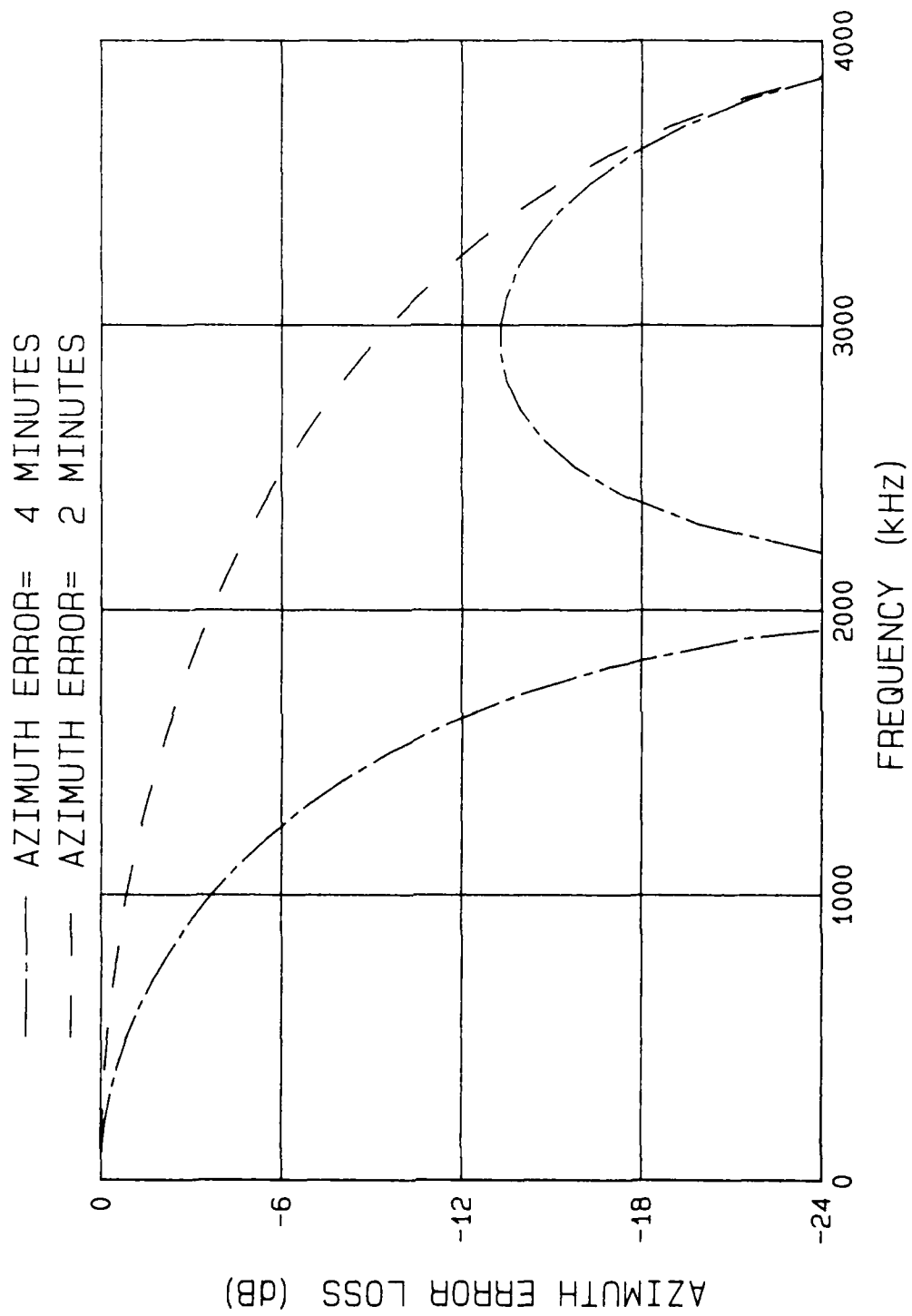


Figure 5.4-2. Azimuth Error Loss Versus Frequency (120 ips).

in systems with adjustable record head involves the use of a "standard" pre-recorded magnetic tape which contains record head azimuth adjustment signal information. The procedure, therefore, references all record head azimuth alignments to a standard recorder/reproducer system. The pre-recorded tape is reproduced on the system in question, the reproduce head azimuth is adjusted to produce the desired output from the pre-recorded tape. After having carefully adjusted the reproduce head azimuth, an upper-bandedge (UBE) signal is recorded and reproduced in real-time. The record head is then adjusted in real-time to produce the peak output amplitude of the upper-bandedge signal at the reproducer system output. It is highly advisable, due to the importance of this adjustment, to input a swept frequency signal to the system, record and reproduce it in real-time, and observe the output of the reproducer system for the desired continuous sweep frequency signal. Nodes of reduced amplitude in the reproduced sweep signal indicate that the azimuth adjustment has been done incorrectly and therefore, the procedure should be repeated. The correct record head azimuth adjustment is an assurance that system to system compatibility will not be degraded due to misalignment of this parameter.

#### 5.4.3 Spacing Loss

Spacing loss is caused by the effective spacing between the magnetic head and the magnetic particles in the tape. The formula for spacing (aka separation) loss was developed by Wallace<sup>20</sup> in 1951:

$$\text{spacing loss} = e^{-2\pi d/\lambda}$$

$$\text{spacing loss (dB)} = 20 \log_{10} e^{-2\pi d/\lambda}$$

$$\text{spacing loss (dB)} = 54.6 d/\lambda \text{ dB}$$

where:

$d$  = effective spacing between reproduce head and magnetic medium

$\lambda$  = recorded wavelength.

If we record a 1 MHz sine wave at a tape speed of 60 inches per second and the effective head-to-tape separation is 18 microinches we get a spacing loss of:

$$54.6 (18 \times 10^{-6} / 60 \times 10^{-6}) = 16.4 \text{ dB.}$$

Therefore, the spacing loss significantly lowers the slot SNR at short wavelengths. The effective spacing is a function of the physical spacing, tape roughness, and record and reproduce head gap lengths. Debris on the tape can decrease short wavelength signals to obscurity!

<sup>20</sup>Wallace, R. L. "The Reproduction of Magnetically Recorded Signals". *Bell System Technical Journal*, October 1951.

#### 5.4.4 Reproduce Gap Loss

The reproduce gap loss is caused by the finite length of the reproduce gap. This is illustrated in figure 5.4-3. The output signal is the average of the signals within the gap. When the recorded wave length is equal to the effective gap length, the average flux across the gap is zero, and therefore the induced voltage is zero. The formula for reproduce gap loss is:

$$\text{gap loss} = (\sin x)/x$$

or

$$\text{gap loss (dB)} = 20 \log ((\sin x)/x)$$

where:

$$x = \pi \ell / \lambda$$

$\lambda$  is the recorded wavelength

$\ell$  is the effective reproduce gap length.

The reproduce gap loss as a function of frequency is plotted in figure 5.4-4 for reproduce gap lengths of 12 and 28 microinches. The loss due to a 28 microinch reproduce gap length at a wavelength of 60 microinches is 3.4 dB. The loss at a wavelength of 120 microinches is 0.8 dB.

#### 5.4.5 Bias Recording

The purpose of recording with a bias signal is to overcome the inherent non-linearity of the record and reproduce processes (see figure 5.4-5). The input is along the  $B_r$  axis and the output is along the H axis in figure 5.4-5. If we record a small signal (solid line), the output amplitude is small. If we record with a large signal (dashed line), the distortion is severe. We can overcome some of these problems by using DC-bias as shown in figure 5.4-6. However, the SNR is still poor and the heads tend to become magnetized. Wideband instrumentation recorders typically sum an ac-bias signal with the signal to be recorded. The frequency of this bias signal should be at least 3.5 times the highest frequency signal to be recorded. The effect of the ac-bias signal is to increase the SNR and reduce the distortion. This is illustrated in figure 5.4-7. The normal bias current setting is 2 dB overbias (upper bandedge signal output amplitude reduced by 2 dB from maximum). The effects of under- and over-bias are illustrated in figure 5.4-8. If linearity is not important the SNR may be improved by the use of saturation recording instead of AC-bias recording.

#### 5.4.6 Equalization

The purpose of equalization is to correct for the amplitude and phase transfer functions of the record and reproduce processes. A separate equalizer is used for each playback speed. The amplitude equalizer must boost the low and high frequency components. A sample signal response curve at the input to the equalizer is shown in figure 5.4-9. The output of the equalizer is shown in figure 5.4-10. The equalizer has made the frequency response nearly constant from near DC to almost 800 kHz.

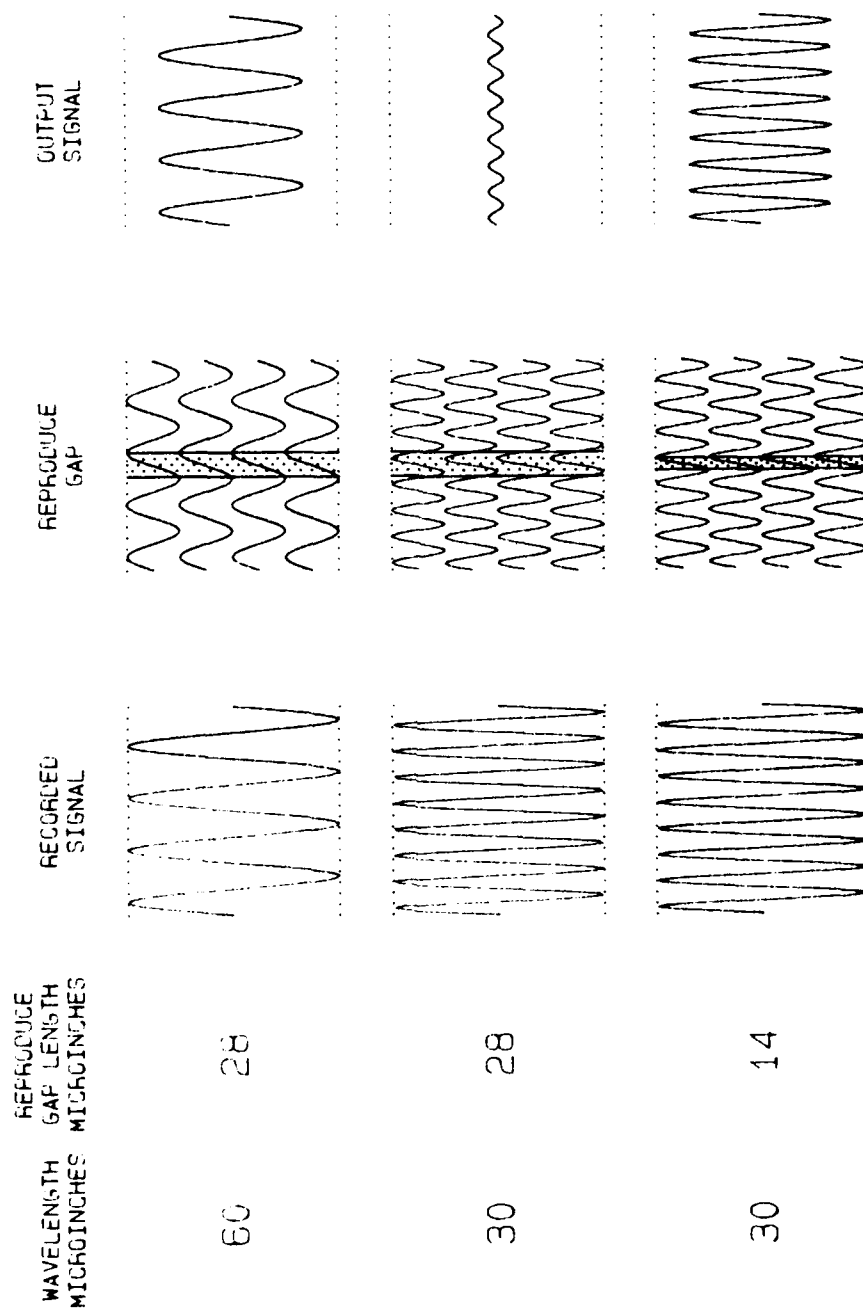


Figure 5.4-3. Reproduce Gap Loss Illustration.

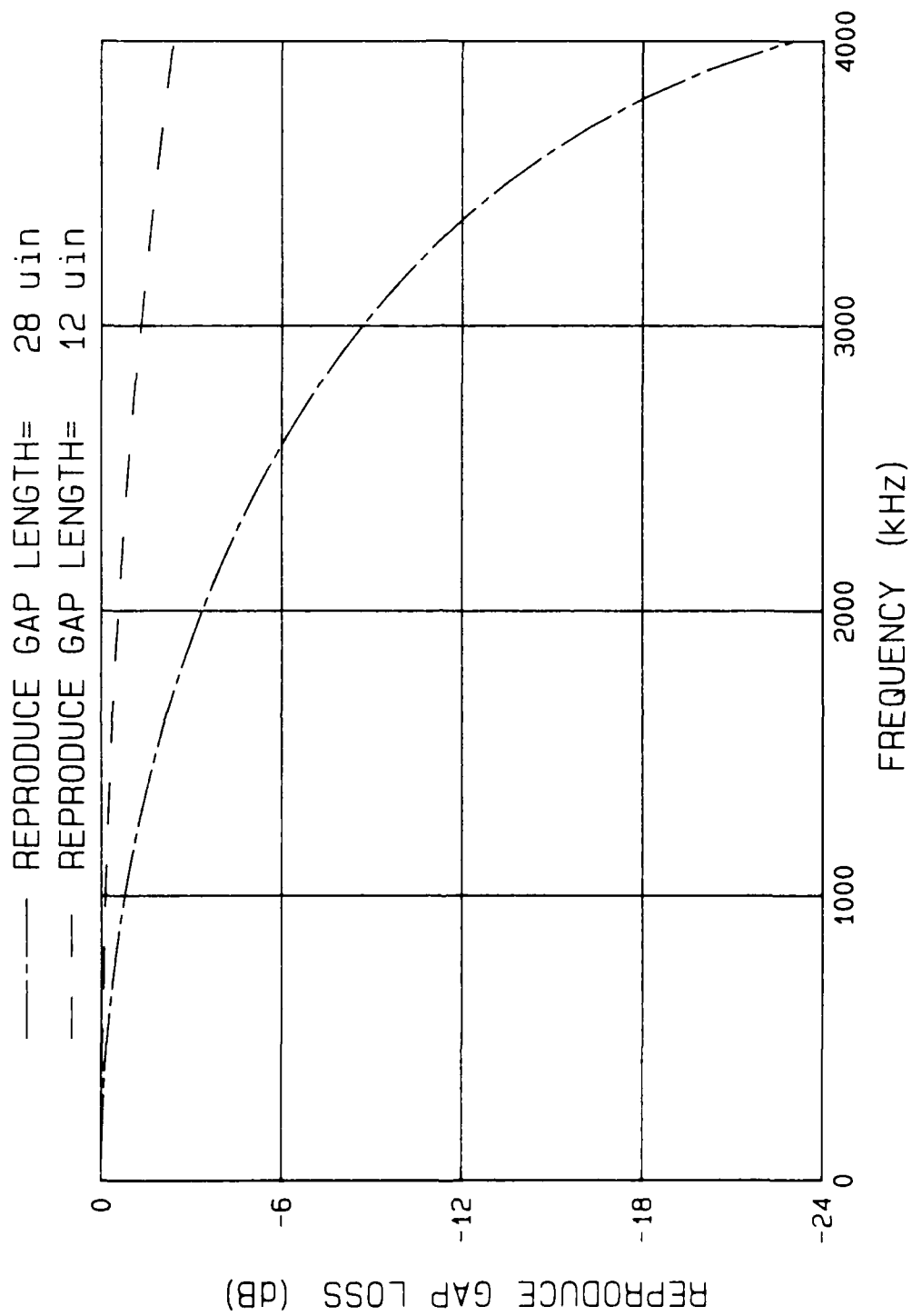


Figure 5.4-4. Reproduce Gap Loss Versus Frequency.

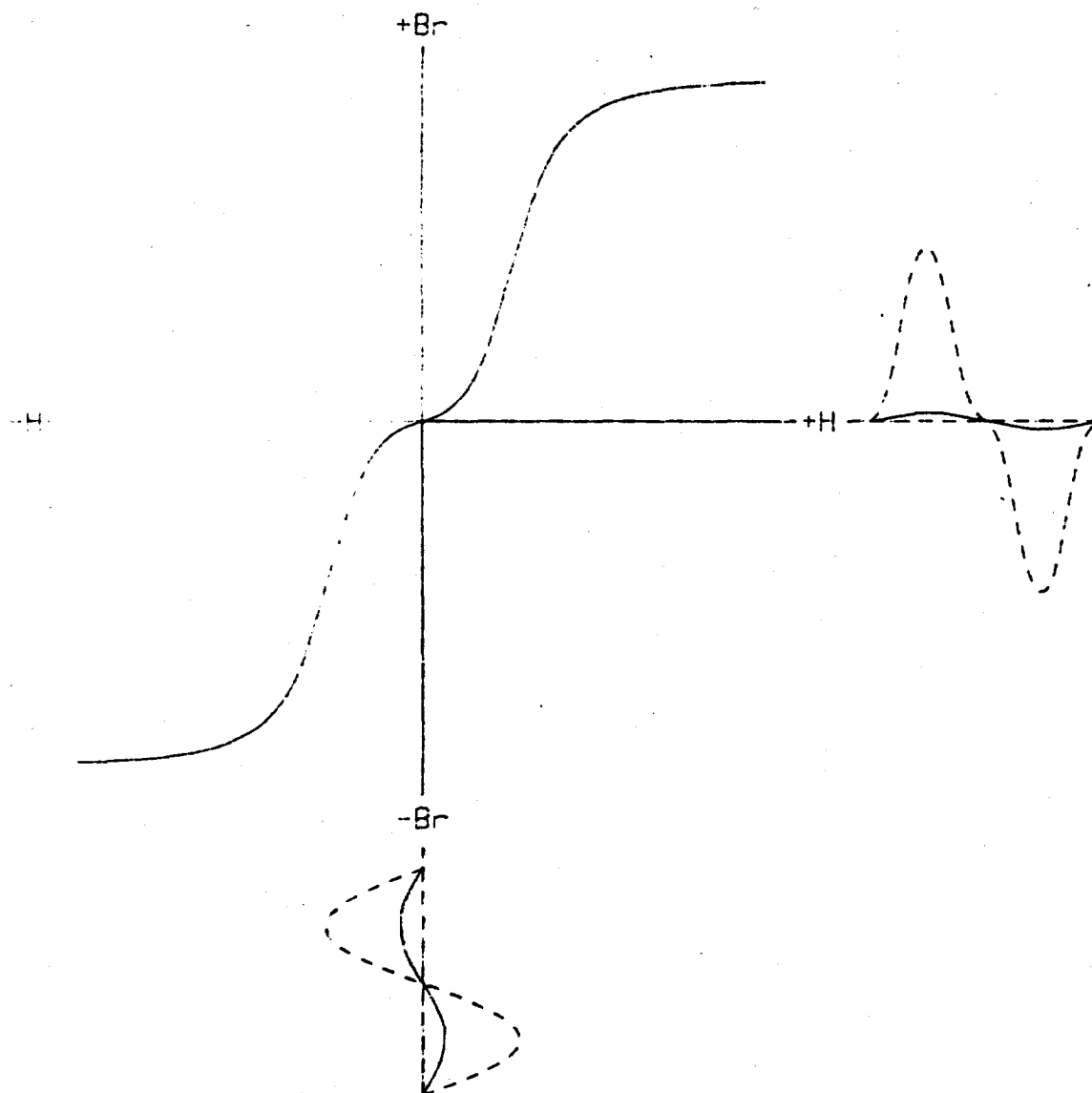


Figure 5.4-5. Recording Without Bias.

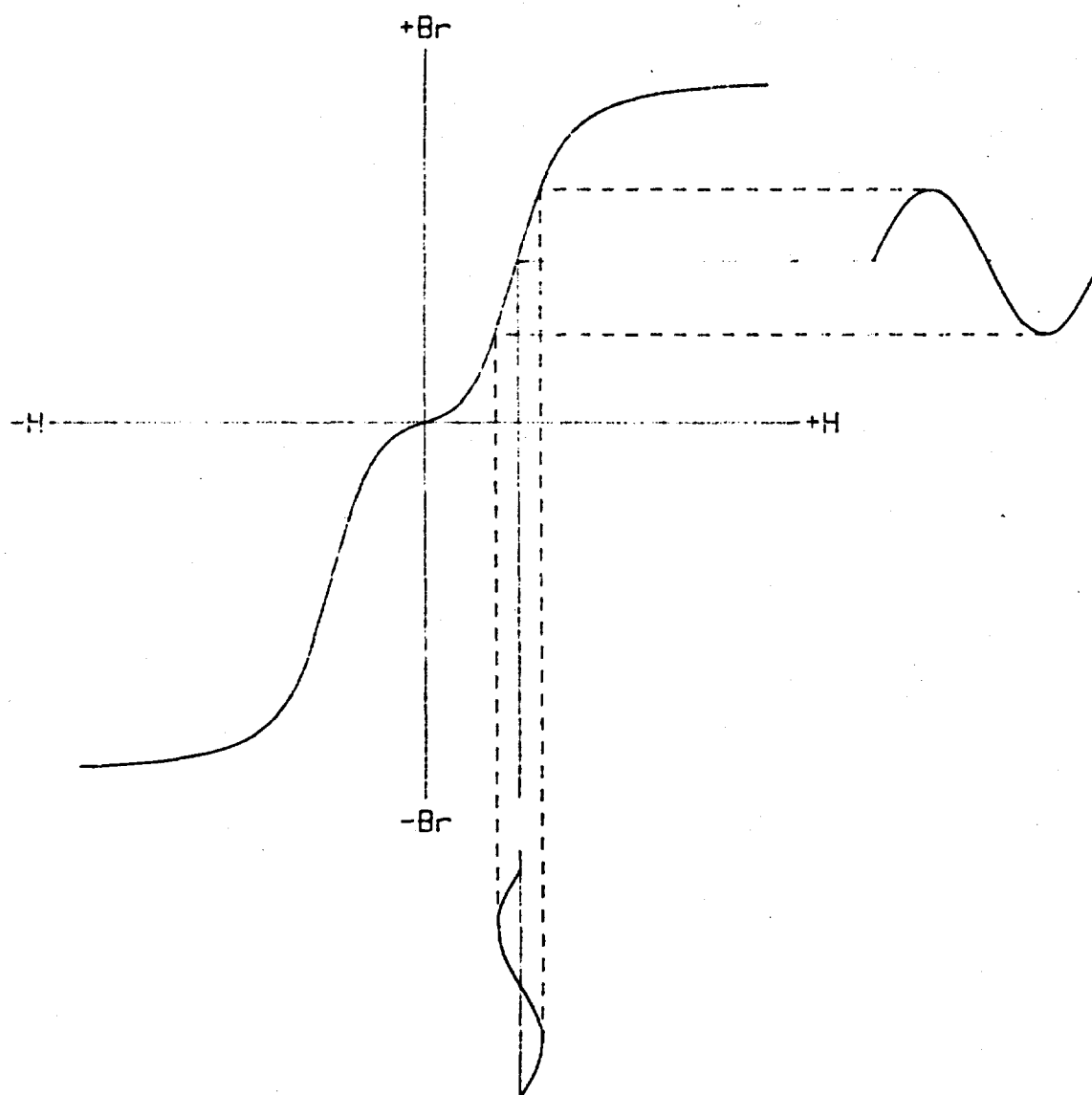


Figure 5.4-6. Recording With DC-Bias.



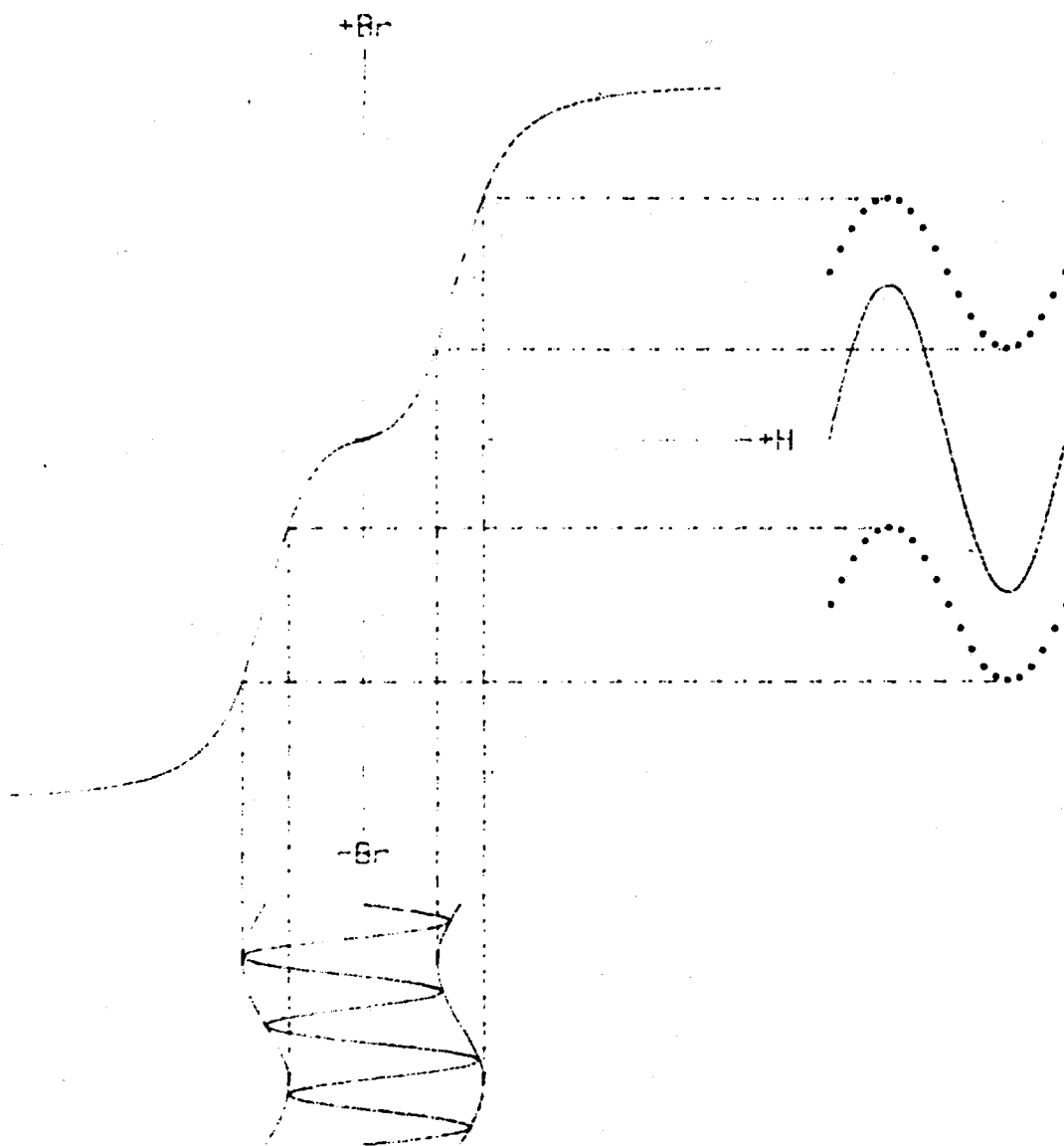


Figure 5.4-7. Recording With AC-Bias.

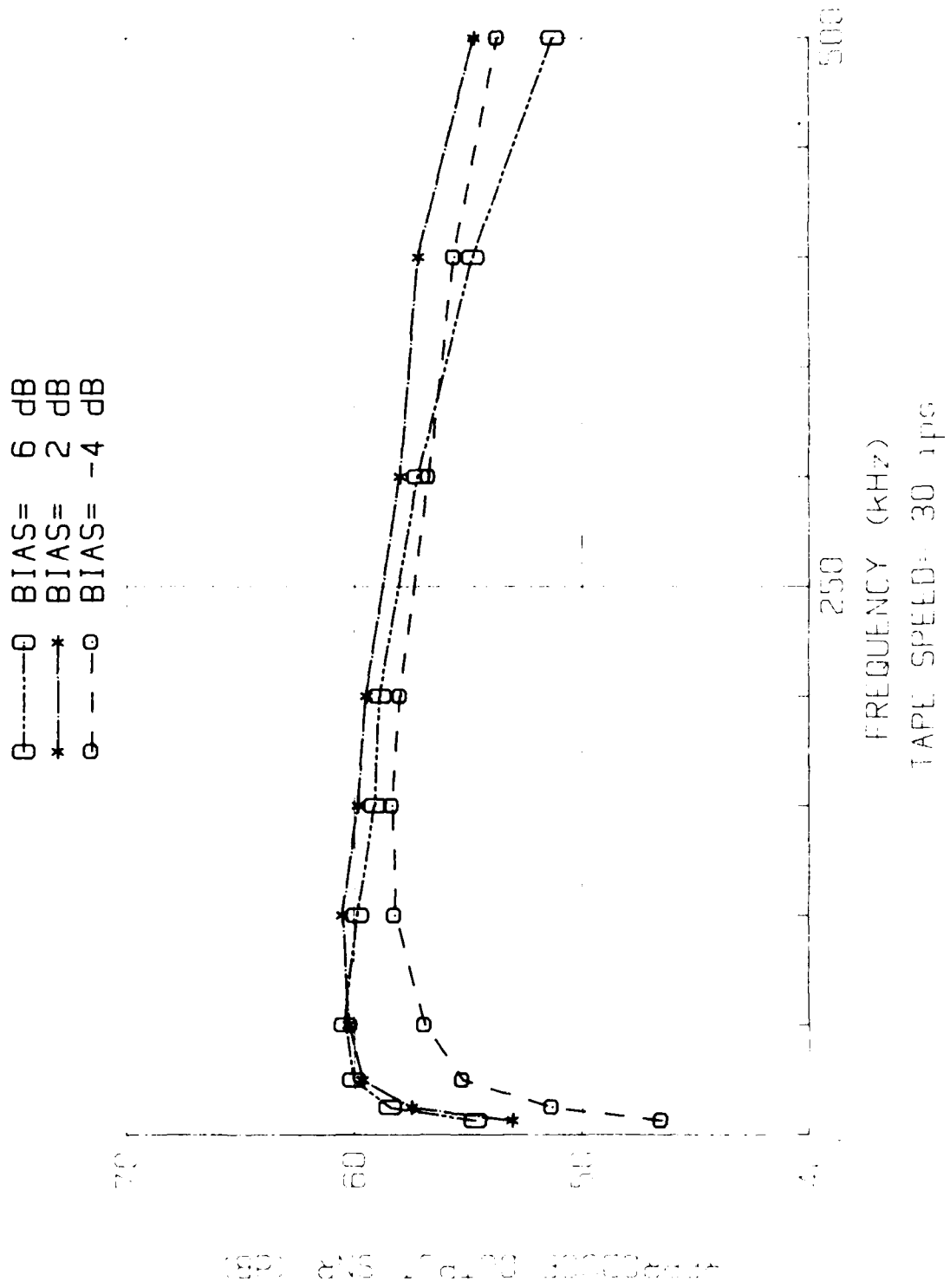


Figure 5.4-8. Effects of Over- and Under-Bias Recording (Input Level Constant).

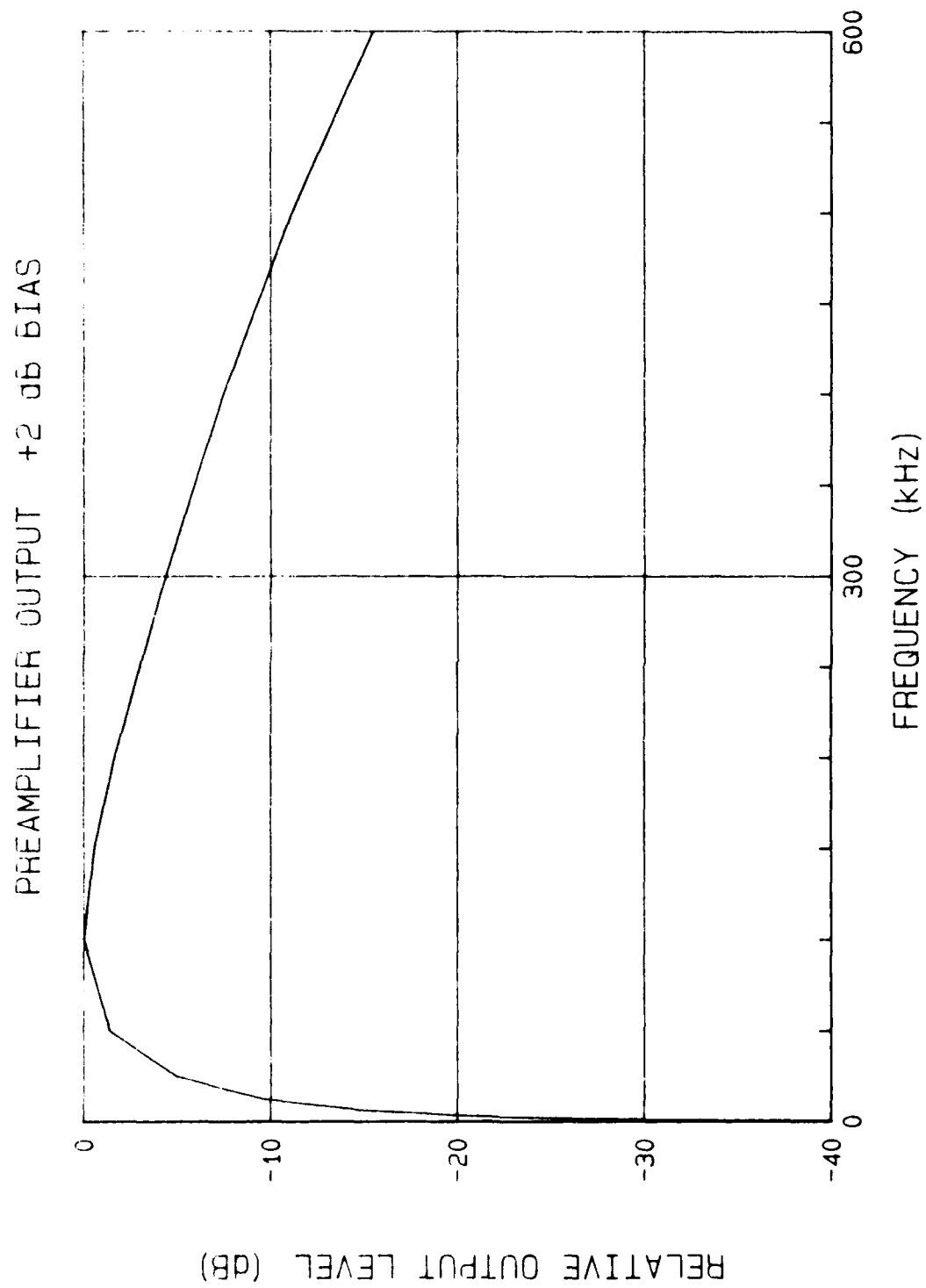


FIGURE 5.4-9. EQUALIZER INPUT AT 30 IPS.

EQUALIZER OUTPUT +2 dB BIAS

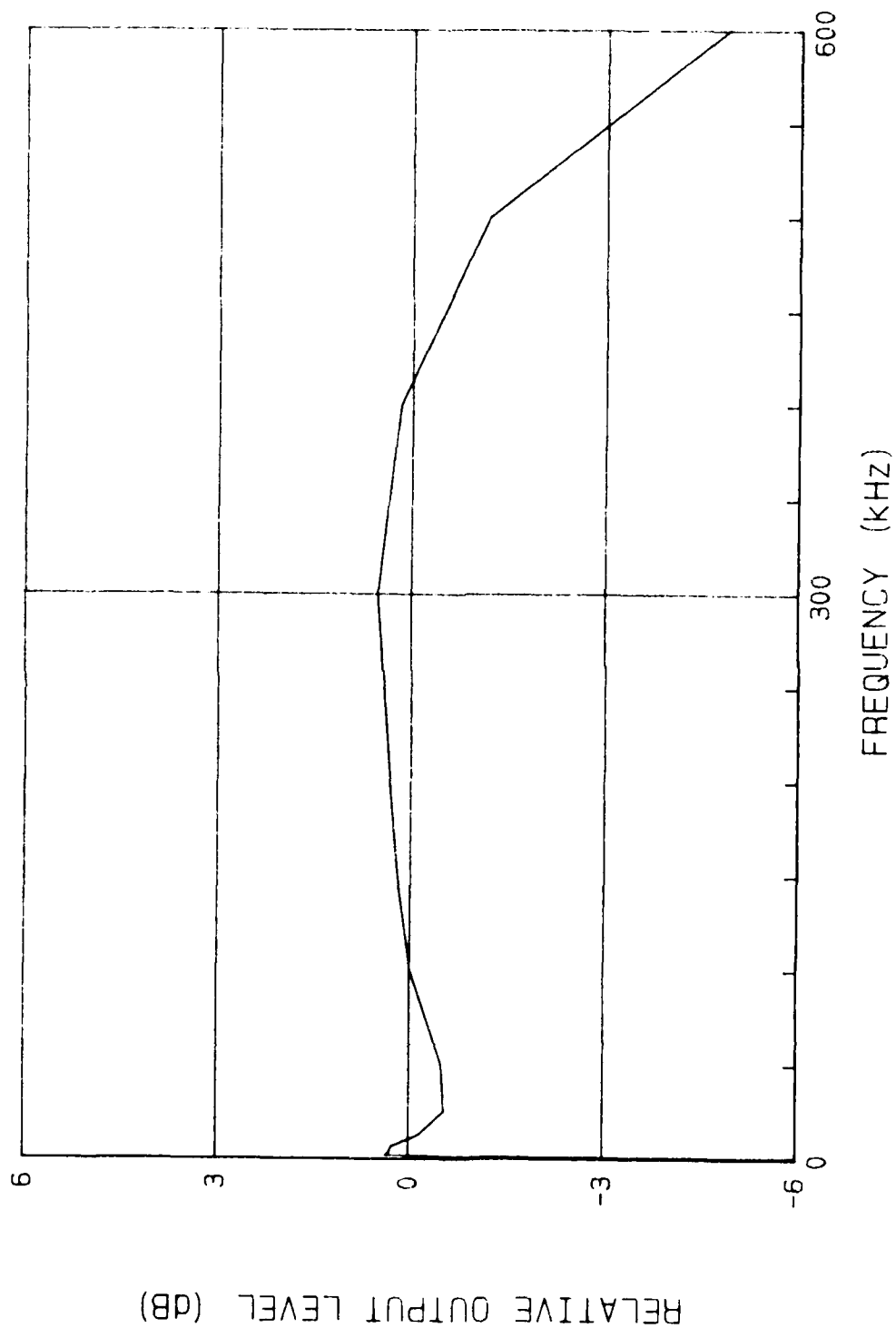


FIGURE 5.4-10. REPRODUCER OUTPUT AT 30 IPS.

#### 5.4.7 Reproducer Output SNR

The wideband SNR (dB) (direct recording) at the output of a properly aligned record/reproduce system varies from the low-twenties to the mid-thirties at tape speeds above 15 ips. The SNR (dB) in a 3 kHz bandwidth with a wideband direct system at a tape speed of 120 ips and a frequency of 400 kHz can exceed 70 dB in a well aligned system. The SNR is lower at other frequencies. These SNRs are more than adequate for most telemetry applications. The SNR is degraded by tape copying (dubbing). Tape dropouts can also degrade the SNR for short time intervals. The biggest sources of SNR problems seem to be: improper record level, improper bias level, undetected equipment problems, material build-up on the heads, and improper azimuth alignment.

#### 5.4.8 Predetection Recording

As discussed earlier, there are several methods for recording telemetry signals. These methods are illustrated in figure 5.4-11. This subsection will only discuss predetection recording. Typical performance data will be presented both with a tape recorder/reproducer and with the recorder bypassed and with demodulation at the tape carrier frequency and after upconversion to a higher frequency (typically 10 or 20 MHz). The data in this subsection are for PCM signals. Predetection recording is also frequently used for PAM signals.

Figure 5.4-12 shows that the BER performance of 300 kb/s NRZ-L PCM/FM is the same with either a 450-kHz or a 900-kHz predetection carrier frequency. The BER performance of the predetection signals with 500 kHz receiver and playback IF bandwidths was approximately 1 dB better than the BER performance of direct receiver video with a 500-kHz IF bandwidth. The reason for this is that putting two 500-kHz bandwidth filters in series results in a filter with a bandwidth of approximately 400 kHz. This increases the actual IF SNR by 1 dB and therefore improves the BER by approximately 1 dB. An entry of 0 in the legend for the figures in this subsection means that part of the test setup was not used for this data; e.g., no recorder was used for the data in figure 5.4-12. The data presented in figure 5.4-13 show the effects of receiver IF bandwidth and tape recording on BER performance. The degradation due to widening the receiver IF bandwidth at a  $10^{-4}$  BER was approximately 1.1 and 2.3 dB for the 2.4- and 4.0-MHz bandwidths, respectively. The recorder/reproducer caused a degradation of no more than 0.3 dB. Figure 5.4-14 shows the effect of varying the receiver IF bandwidth at a bit rate of 900 kb/s and a predetection frequency of 900 kHz. The BERs with the 1000- and 1500-kHz bandwidths were very similar, while the 2400-kHz bandwidth caused approximately 0.5 dB of degradation and the 4000-kHz bandwidth caused approximately 1.8 dB of degradation at a BER of  $10^{-4}$ . The degradation with the 4000-kHz IF bandwidth is mostly caused by noise folding back across zero hertz and increasing the noise power in the playback demodulator's passband. This is illustrated in figure 5.4-15. The higher amplitude trace in each group is the noise with a 3000-kHz IF bandwidth and the lower amplitude trace is the noise with a 1500-kHz IF bandwidth. The noise power is the same with both filters for frequencies between 9.6 and 10.4 MHz and 900 and 1300 kHz. However, the 3000-kHz IF bandwidth causes the noise power between 500 kHz and 800 kHz to increase by 1 to 2 dB. The predetection downconverter also does some low pass filtering. The unmodulated carrier level was 0 dBc for these plots. Figure 5.4-16 shows that using a 900-kHz predetection carrier with 900 kb/s NRZ-L PCM/FM data causes a data degradation of approximately 0.2 dB at a  $10^{-4}$  BER when compared to the BER performance using a 1.8-MHz predetection carrier frequency.

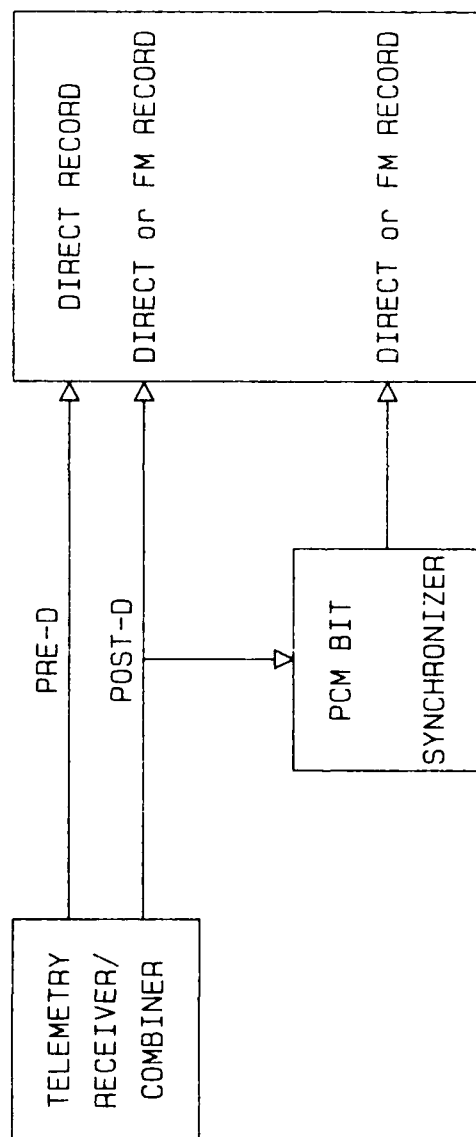


Figure 5.4-11. Methods for Recording Telemetry Signals.

MOD TYPE	BIT RATE kb/s	IFBW kHz	PRK kHz	PRED kHz	VID kHz	PEAK DEV	RCD IPS
x NRZ-L PCM/FM	300	1000	0	0	250	107	0
+ NRZ-L PCM/FM	300	500	0	0	250	107	0
o NRZ-L PCM/FM	300	500	500	900	250	107	0
* NRZ-L PCM/FM	300	500	500	450	250	107	0

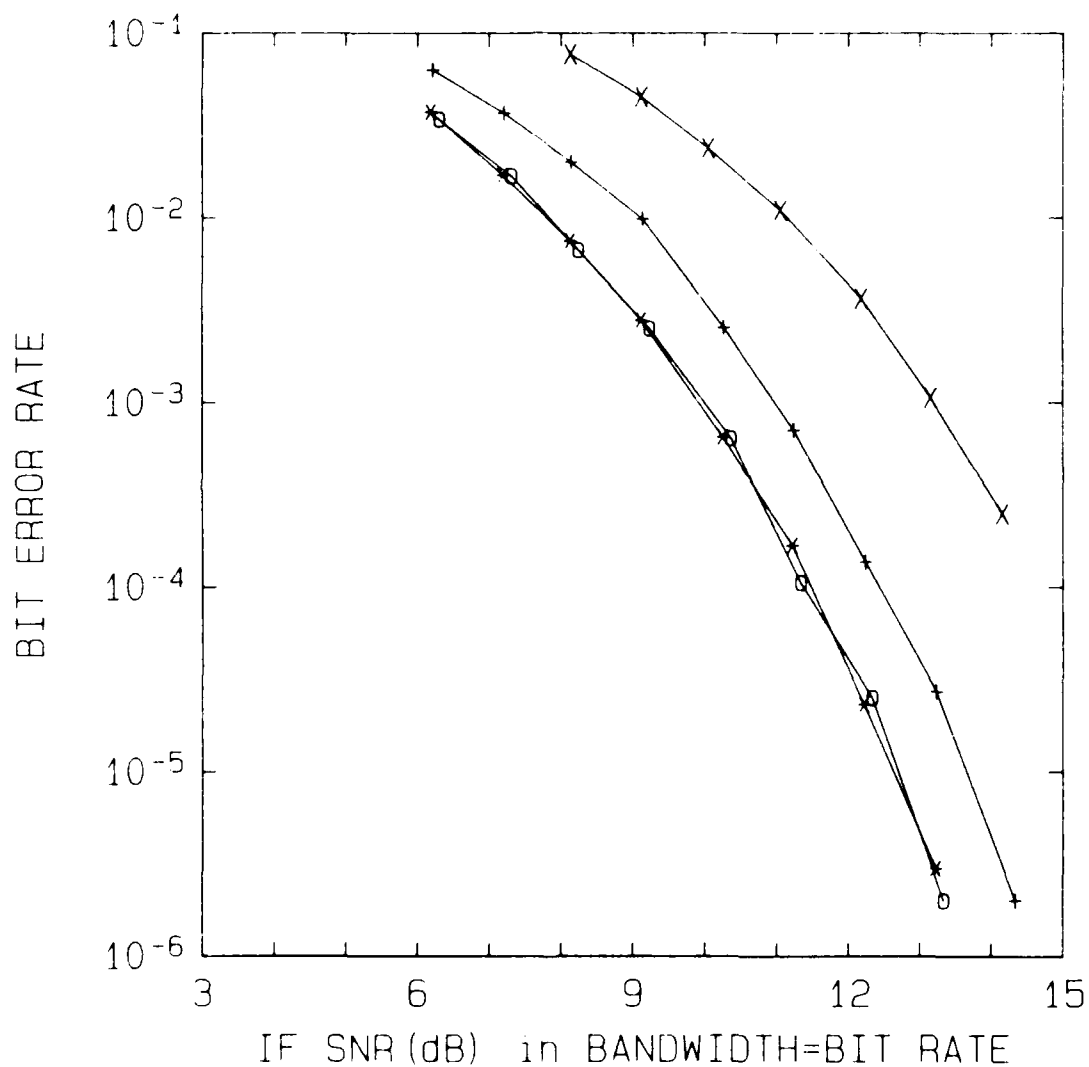


Figure 5.4-12. BER with 300 kb/s and 450 and 900 kHz PRE-D.

MOD TYPE	BIT RATE kb/s	IFBW kHz	PBW kHz	FREQ kHz	VIL kHz	PTAB dB	R/D Hz
X NRZ-L PCM/FM	600	4000	1000	900	500	214	120
O NRZ-L PCM/FM	600	4000	1000	900	500	214	0
+ NRZ-L PCM/FM	600	2400	1000	900	500	214	120
o NRZ-L PCM/FM	600	2400	1000	900	500	214	0
* NRZ-L PCM/FM	600	1000	1000	900	500	214	0

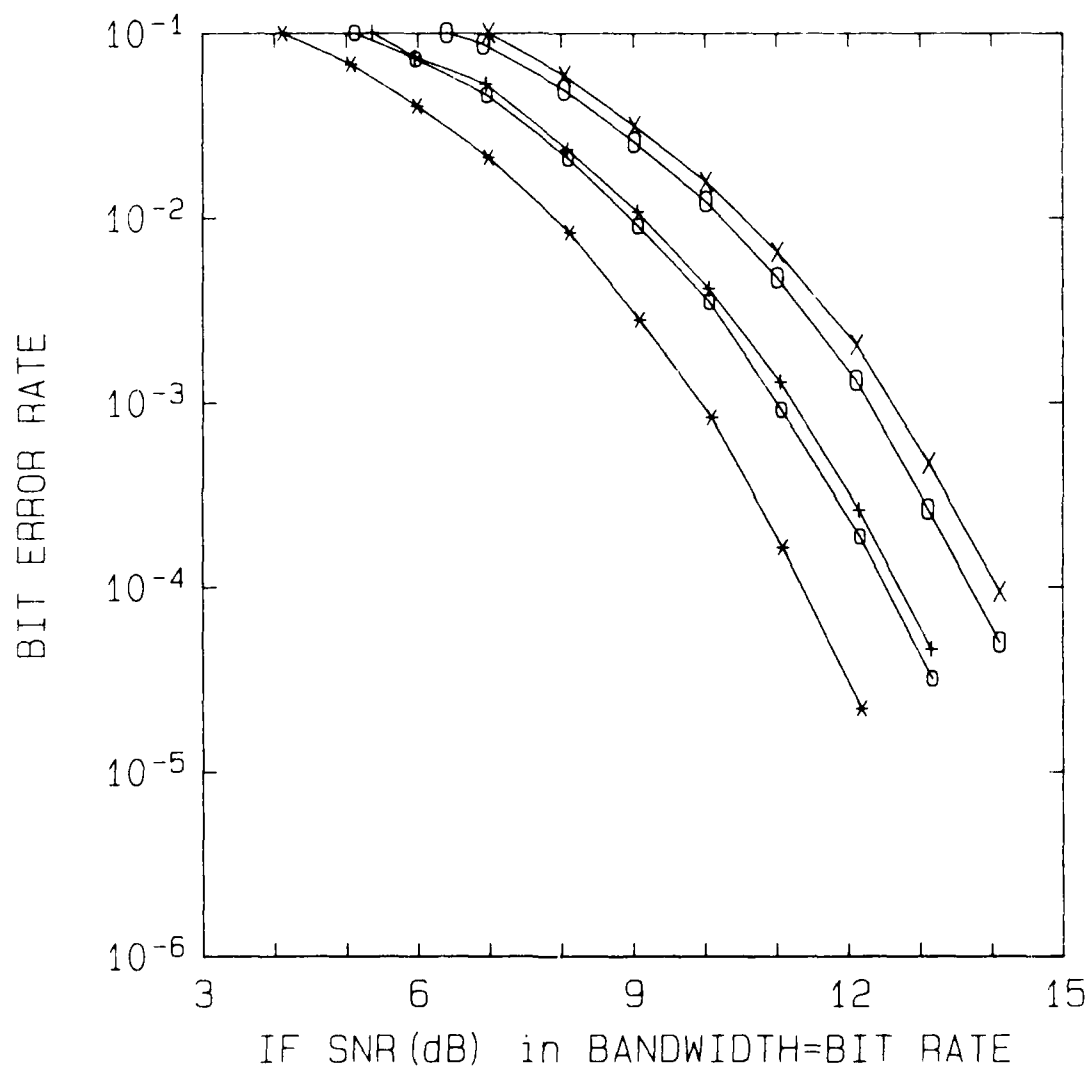


Figure 5.4-13. BER with and without Recording.



MOD	BIT RATE	IFBW	PBK	PRED	VID	PEAK	RCD
TYPE	kb/s	KHz	KHz	KHz	KHz	DEV	IPS

0	NRZ-L	PCM/FM	900	4000	1000	900	1000	321	0
+	NRZ-L	PCM/FM	900	2400	1000	900	1000	321	0
o	NRZ-L	PCM/FM	900	1500	1000	900	1000	321	0
*	NRZ-L	PCM/FM	900	1000	1000	900	1000	321	0

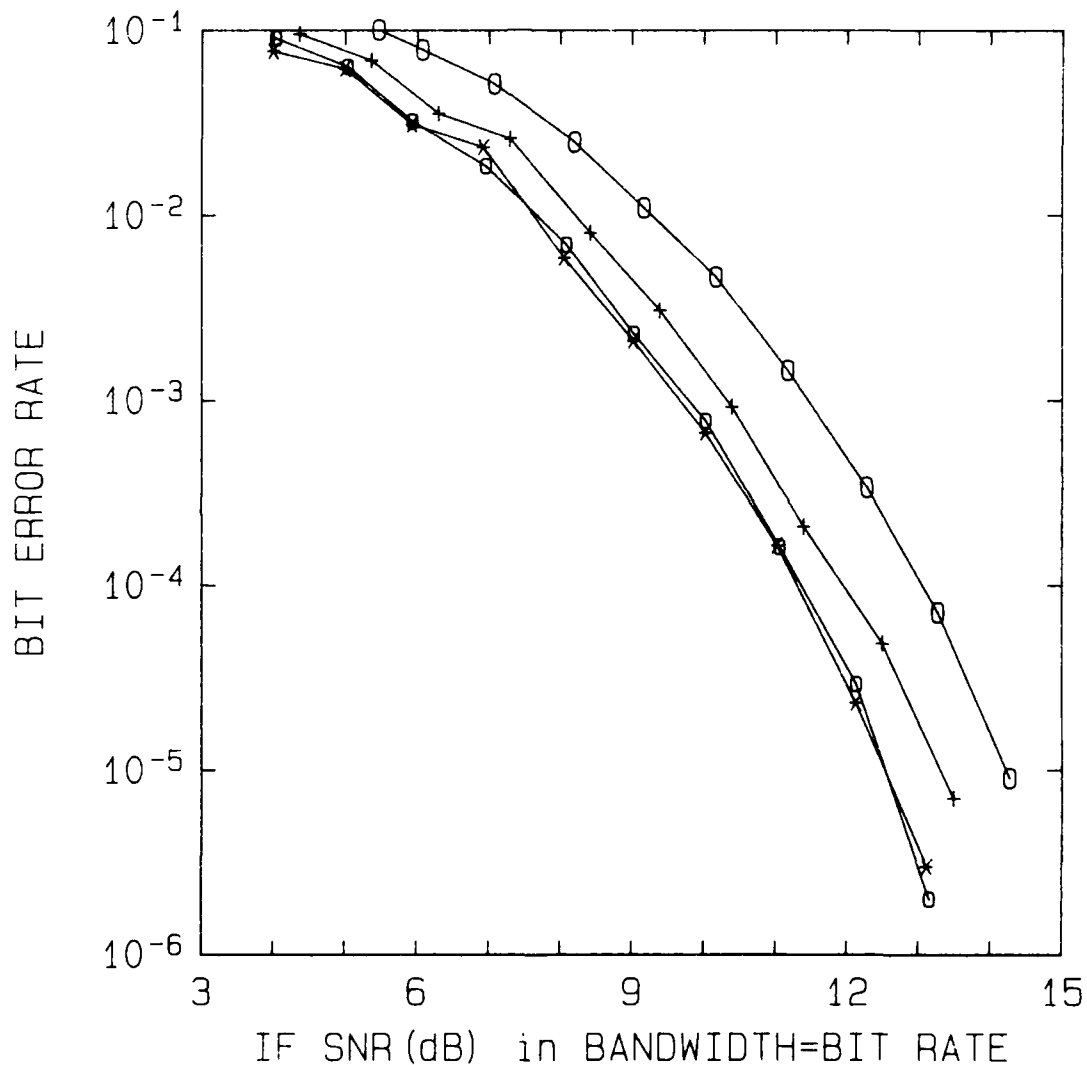


Figure 5.4-14. BER for 900 kb/s and 900 kHz PRE-D.

MOD	BIT RATE	IFBW	PBK	PRED	VID	PEAK	RCD
TYPE	kb/s	kHz	kHz	kHz	kHz	DEV	IPS
X NRZ-L PCM/FM	600	4000	1000	900	500	214	120
O NRZ-L PCM/FM	600	4000	1000	900	500	214	0
+ NRZ-L PCM/FM	600	2400	1000	900	500	214	120
o NRZ-L PCM/FM	600	2400	1000	900	500	214	0
* NRZ-L PCM/FM	600	1000	1000	900	500	214	0

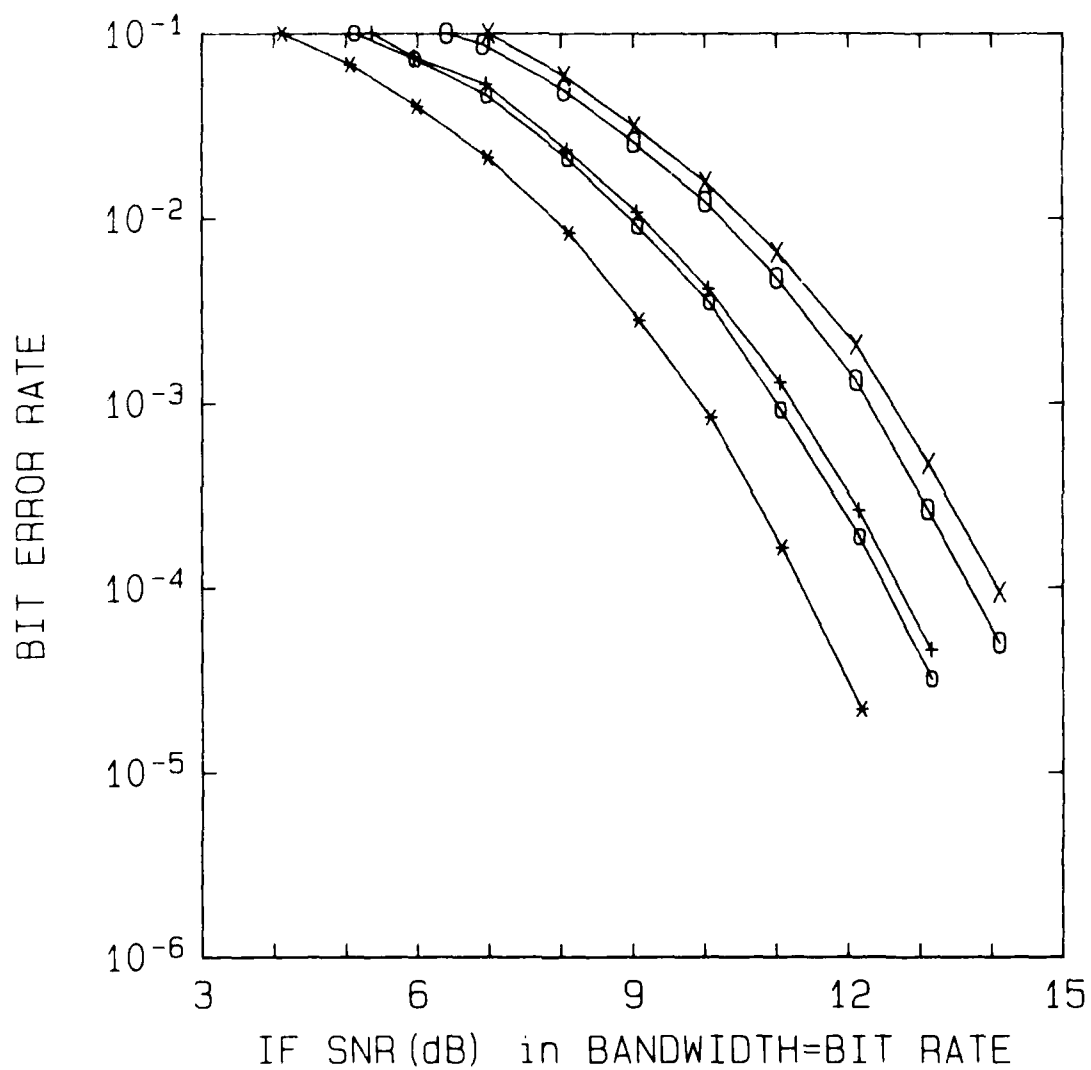


Figure 5.4-13. BER with and without Recording.

This slight degradation may well be preferable to doubling the tape speed so that the 1.8-MHz predetection carrier could be used.

The data in figure 5.4-17 show that upconversion and demodulation perform approximately 1.6 dB better than demodulation at the tape carrier frequency when the NRZ PCM/FM bit rate is equal to the predetection carrier frequency. Most of the degradation is due to excessive bandpass filtering in the tape carrier discriminator. The bandwidth is only 720 kHz ( $900 \pm 40\%$ ) which degrades the BER by more than 1 dB.

The data in figure 5.4-18 show that a 1200-kHz predetection carrier performs 2 to 3 dB better than a 900-kHz carrier for 1200 kb/s NRZ-M PCM/PM ( $90^\circ$ ). Figure 5.4-19 presents data for biphas-level PCM/PM ( $75^\circ$ ) for demodulation at 900 kHz and at 10 MHz (PRED = 0). Demodulation at 900 kHz degrades the 300-kb/s performance by 0.3 dB and the 600-kb/s performance by 1 dB at a  $10^{-4}$  BER. The difference in BER performance at a  $10^{-4}$  BER between 300 kb/s and 450 kb/s is approximately 0.5 dB, while the difference between 300 kb/s and 600 kb/s is approximately 1.8 dB. This suggests that the highest recommended biphas bit rate should be one-half of the predetection frequency.

#### 5.4.9 Serial High Density Digital Recording (HDDR)

Serial HDDR is a method of recording digital data on a magnetic tape where the digital data is applied to one track of the recording system as a bi-level signal<sup>21,22</sup>. Reference 22 also includes discussions of parallel HDDR and error correction codes for magnetic recording. The codes recommended for serial HDDR recording of telemetry data are biphas-level and randomized NRZ-L (RNRZ-L). The maximum recommended bit packing densities for reliable data interchange are 0.9 bits/Hz for biphas-level and 1.5 bits/Hz for RNRZ-L.

The properties of the biphas-level and RNRZ-L codes relevant to serial HDDR and the methods for generating and decoding RNRZ-L are described below. Recording with bias is required for interchange applications because reproduce amplifier phase and amplitude equalization adjustments for tapes recorded without bias usually differ from those required for tapes recorded with bias.

The biphas-level and RNRZ-L codes were selected for this standard because the "level" versions are easier to generate and are usually available as outputs from bit synchronizers. "Mark" and "Space" codes also have about twice as many errors as the level codes for the same SNR. If polarity insensitivity is a major consideration, agreement between interchange parties should be obtained before these codes are used.

<sup>21</sup>Law, E. L. Serial High Density Digital Recording Using a Wideband Analog IRIG Recorder/Reproducer. Pacific Missile Test Center, Point Mugu, CA, May 1981

<sup>22</sup>Kalil, F. and A. Buschman (Eds.) High-Density Digital Recording. NASA Reference Publication 1111, September 1985.

MOD	BIT RATE	IFBW	PBK	PRED	VID	PEAK	RCD
TYPE	kb/s	kHz	kHz	kHz	kHz	DEV	IPS
0 NRZ-L PCM/FM	900	2400	720	900	600	321	0
+ NRZ-L PCM/FM	900	2400	1000	900	1000	321	0
o NRZ-L PCM/FM	900	1500	720	900	600	321	0
* NRZ-L PCM/FM	900	1500	1000	900	1000	321	0

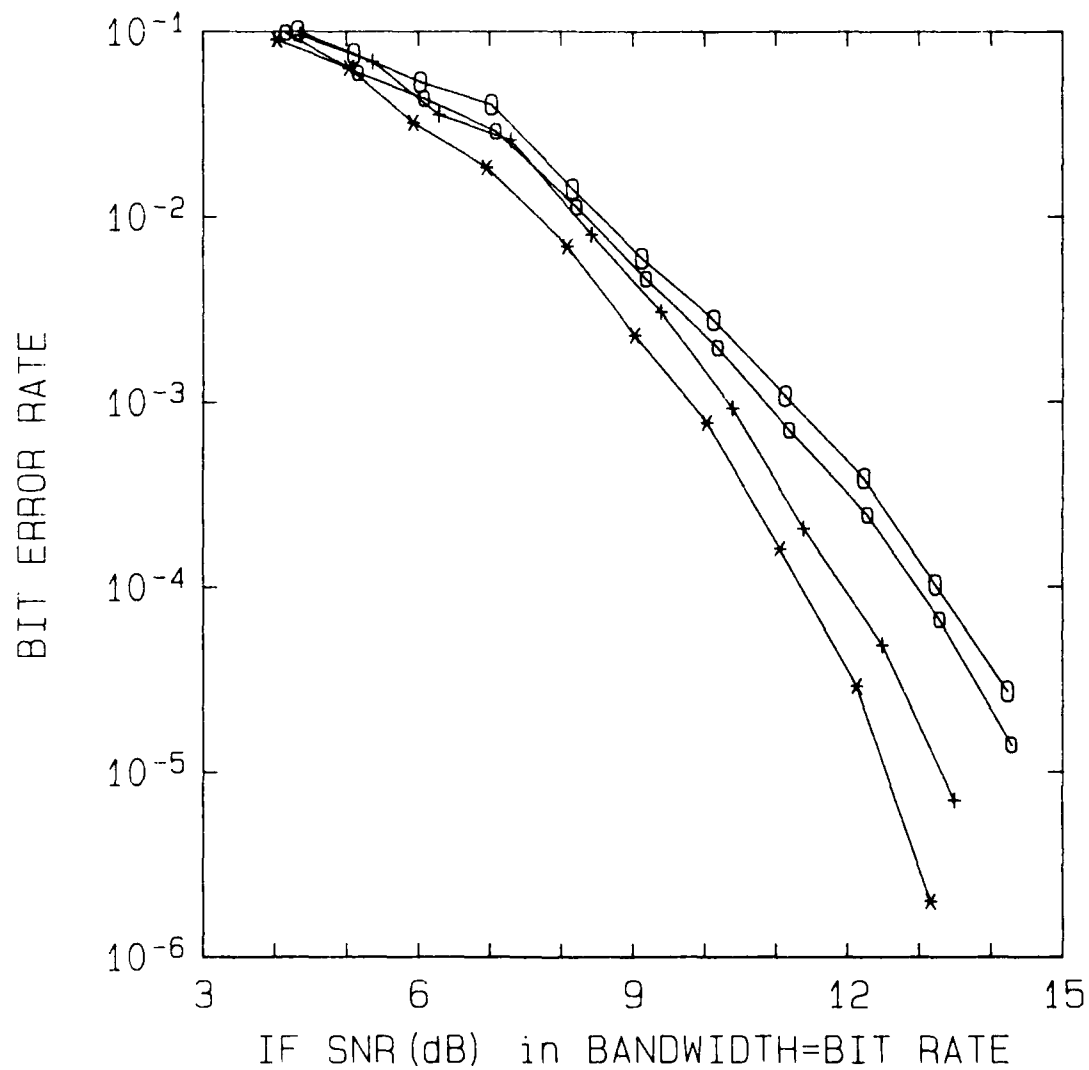


Figure 5.4-17. Upconversion versus Tape Carrier Demodulation.

MOD TYPE	BIT RATE kb/s	IFBW kHz	PBK kHz	PRED kHz	VID kHz	PEAK DEV	RCD IPS
0 NRZ-M PCM/PM	1200	1500	2400	900	1000	90	0
+ NRZ-M PCM/PM	1200	2400	1500	900	1000	90	0
o NRZ-M PCM/PM	1200	2400	2400	900	1000	90	0
* NRZ-M PCM/PM	1200	2400	2400	1200	1000	90	0

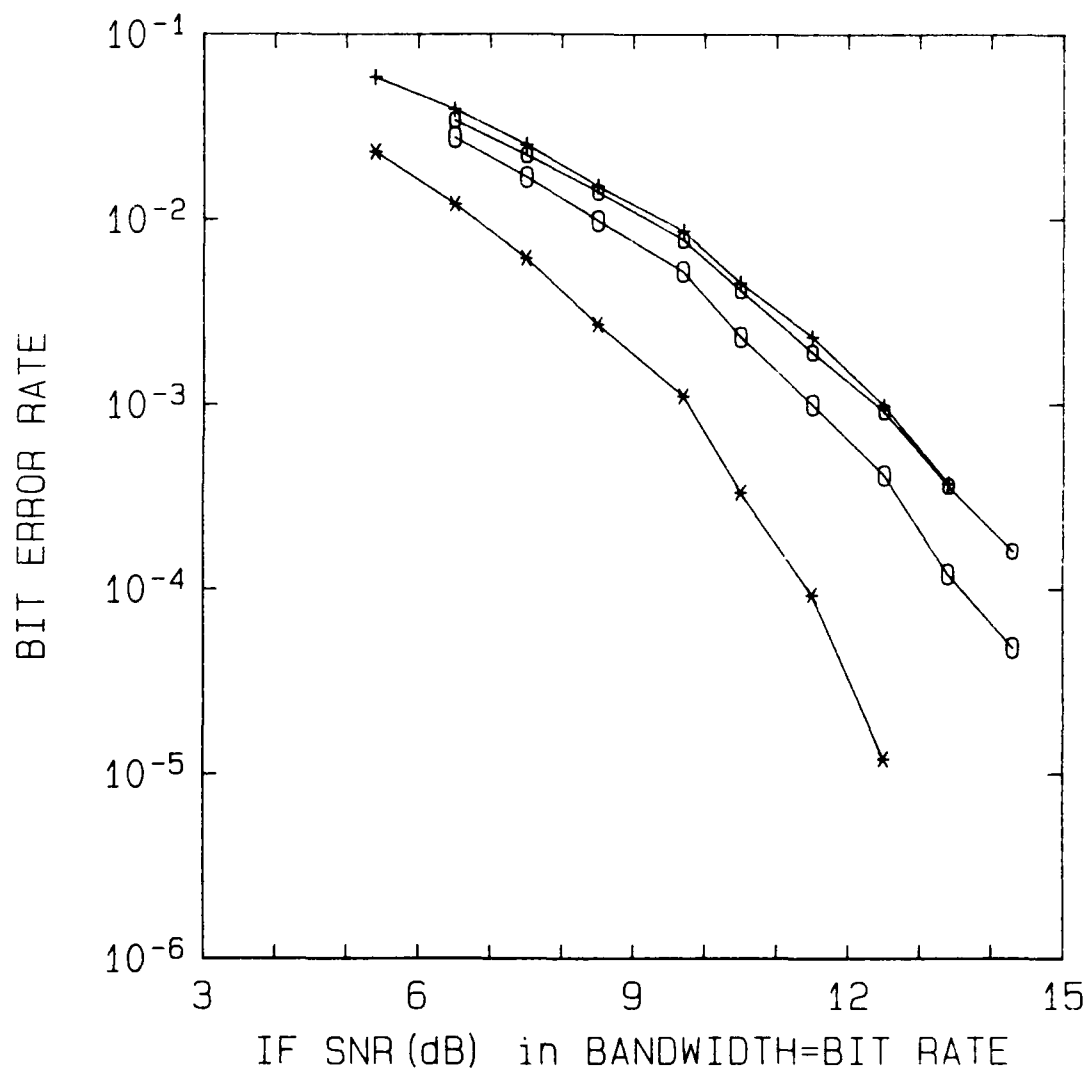


Figure 5.4-18. BER for 1200 kb/s PCM/PM with 900 and 1200 kHz PRE-D.

MOD	BIT RATE	IFBW	PBK	PRED	VID	PEAK	RCD
TYPE	kb/s	kHz	kHz	kHz	kHz	DEV	IPS
X BIO-L PCM/PM	600	1500	2000	0	2000	75	0
O BIO-L PCM/PM	600	1500	2000	900	2000	75	0
+ BIO-L PCM/PM	450	1500	2000	900	2000	75	0
o BIO-L PCM/PM	300	1500	2000	900	2000	75	0
* BIO-L PCM/PM	300	1500	2000	0	2000	75	0

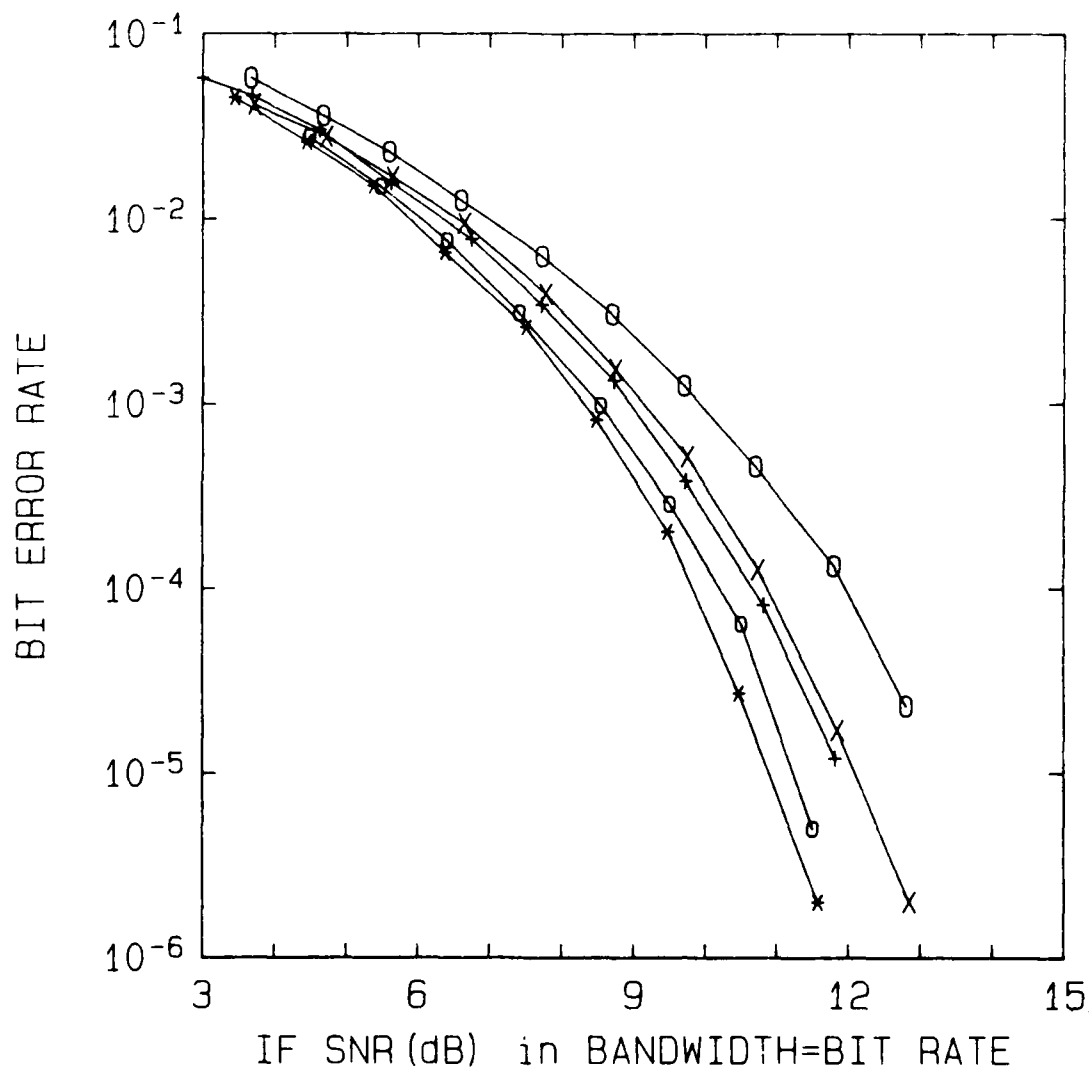


Figure 5.4-19. BER for 300, 450, and 600 kb/s Biphase PCM/PM.

Some characteristics of the biphas-level code favorable to serial HDDR are:

1. Only a small proportion of the total signal energy occurs near DC.
2. The maximum time between transitions is 1 bit period.
3. The symbols for a "one" and a "zero" are antipodal; that is, the symbols are exact opposites of each other. Therefore, the bit error probability versus SNR performance is optimum.
4. Biphas-level can be decoded using existing bit synchronizers.
5. Biphas-level is less sensitive to misadjustments of bias and reproducer equalizers than most other codes.
6. Biphas-level performs well at low tape speeds and low bit rates.

The most unfavorable characteristic of the biphas-level code is that it requires approximately twice the bandwidth of NRZ. Therefore, the maximum bit packing density that can be recorded on magnetic tape is relatively low.

Characteristics of the RNRZ-L code which favor its use for serial HDDR include:

1. RNRZ-L requires approximately one-half the bandwidth of biphas-level.
2. The symbols for a "one" and a "zero" are antipodal; therefore, the bit error probability versus SNR performance is optimum.
3. The RNRZ-L decoder is self-synchronizing.
4. The RNRZ-L data can be bit synchronized and signal conditioned using existing bit synchronizers with the input code selector set to NRZ-L.
5. The RNRZ-L code is easily generated and decoded.
6. The RNRZ-L data can be easily decoded in the reverse mode of tape playback.
7. The RNRZ-L data are bit detected and decoded using a clock at the bit rate. Therefore, the phase margin is much larger than that of codes that require a clock at twice the bit rate for bit detection.
8. The RNRZ-L code does not require overhead bits.

Unfavorable characteristics of the RNRZ-L code for serial HDDR include:

1. Long runs of bits without a transition are possible although the probability of occurrence is low, and the maximum run length can be limited by providing transitions in each data word.
2. Each isolated bit error that occurs after the data has been randomized causes 3 bit errors in the derandomized output data.

3. The decoder requires 15 consecutive error-free bits to establish and re-establish error-free operation.
4. The RNRZ-L bit stream can have a large low frequency content. Therefore, reproducing data at tape speeds which produce PCM bit rates less than 200 kb/s is not recommended unless a bit synchronizer or playback amplifier with specially designed DC and low frequency restoration circuitry is available.

#### 5.4.10 Randomizer for RNRZ-L

The randomizer is implemented with a network of shift registers and modulo-2 adders (exclusive-OR gates). The RNRZ-L bit stream is generated by adding (modulo-2) the reconstructed NRZ-L PCM data to the modulo-2 sum of the outputs of the 14<sup>th</sup> and 15<sup>th</sup> stages of a shift register. The output RNRZ-L stream is also the input to the shift register (see figure 5.4-20).

The properties of an RNRZ-L bit stream are similar to the properties of a pseudo-random sequence. A 15-stage RNRZ-L encoder will generate a maximal length pseudo-random sequence of  $2^{15} - 1$  (32,767) bits if the input data consists only of "zeros" and there is at least a single "one" in the shift register. A maximal length pseudo-random sequence is also generated when the input data consists only of "ones" and the shift register contains at least a single "zero." However, if the shift register contains all "zeros" at the moment that the input bit stream is all "zeros", the RNRZ-L output bit stream will also be all "zeros." The converse is also true: when the shift register is filled with "ones" and the input bit stream is all "ones", the RNRZ-L output bit stream will contain only "ones". In these two cases, the content of the shift register does not change and the output data is not randomized. However, the randomizer is not permanently locked-up in this state because a change in the input data will again produce a randomized output. In general, if the input bit stream contains runs of X bits without a transition with a probability of occurrence of  $p(X)$ , the output will contain runs having a length of up to  $(X + 15)$  bits with a probability of  $(2^{-15} \times p(X))$  bits. Therefore, the output can contain long runs of bits without a transition, but the probability of occurrence is low.

The RNRZ-L bit stream is decoded (derandomized) by adding (modulo-2) the reconstructed RNRZ-L bit stream to the modulo-2 sum of the outputs of the 14<sup>th</sup> and 15<sup>th</sup> stages of the shift register. The reconstructed RNRZ-L bit stream is the input to the shift register (see figure 5.4-21). RNRZ-L data which is reproduced using the reverse playback mode of operation is decoded by adding (modulo-2) the reconstructed RNRZ-L bit stream to the modulo-2 sum of the outputs of the 1<sup>st</sup> and 15<sup>th</sup> stages of the shift register (see figure 5.4-21). The net effect is that the decoding shift register runs "backwards" with respect to the randomizing shift register.

Although the RNRZ-L decoder is self-synchronizing, 15 consecutive error-free bits must be loaded into the shift register before the output data will be valid. A bit slip will cause the decoder to lose synchronization, and 15 consecutive error-free data bits must again be loaded into the shift register before the output data is valid. The decoded output data, although correct, will contain the bit slip causing a shift in the data with respect to the frame synchronization pattern. Therefore, frame synchronization must be re-acquired before the output provides meaningful data.



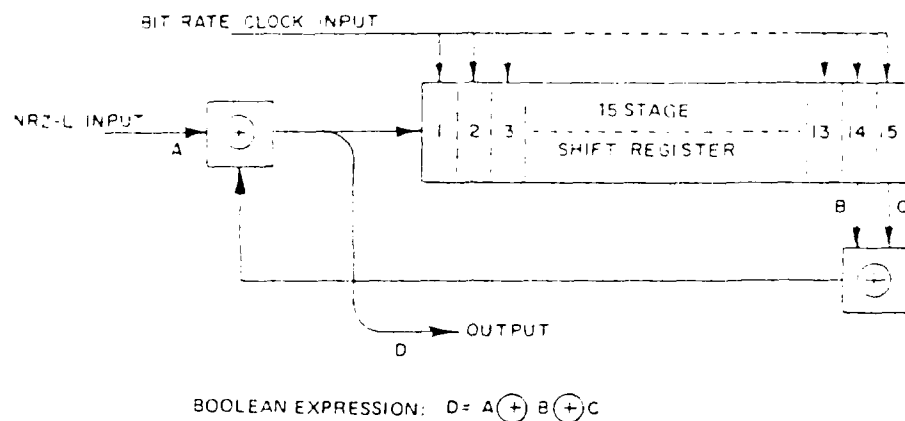
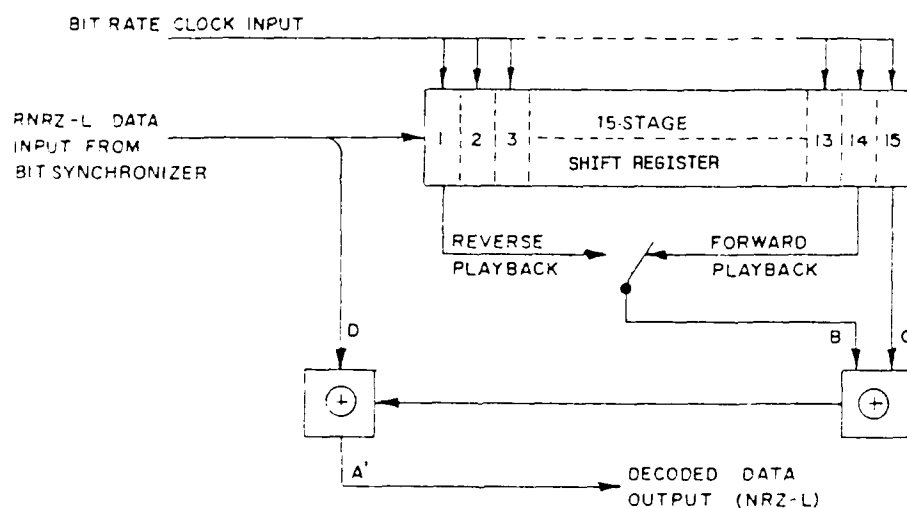


Figure 5.4-20. Randomizer.



BOOLEAN EXPRESSION:  
WITH INPUT DATA A INTO RANDOMIZER,  
ERROR-FREE NRZ-L DATA,  $D = A \oplus B \oplus C$

$$A' = D \oplus B \oplus C = A \oplus B \oplus C \oplus B \oplus C$$

$$= A \oplus B \oplus B \oplus C \oplus C \quad \text{BUT} \quad B \oplus B = 0$$

$$C \oplus C = 0$$

$$\text{THEREFORE: } A' = A \oplus 0 \oplus 0 = A$$

Figure 5.4-21. Denandomizer.

The RNRZ-L decoding system has an error multiplication factor of 3 for isolated bit errors (separated from adjacent bit errors by at least 15 bits). An isolated bit error introduced after randomization will produce 3 errors in the output data; the original bit in error, plus 2 additional errors 14 and 15 bits later. In addition, a burst of errors occurring after the data has been randomized will produce a burst of errors in the derandomized output. The number of errors in the output depends on the distribution of errors in the burst and can be greater than, equal to, or less than the number of errors in the input to the derandomizer. However, the derandomization process always increases the number of bits between the first and last error in the burst by 15. Errors introduced prior to randomization are not affected by either the randomizer or the derandomizer. The reverse decoder has the same bit error properties as the forward decoder.

Input data containing frequent long runs of bits without transitions creates potential DC and low frequency restoration problems in PCM bit synchronizers because of the low frequency cutoff of direct reproducer systems. The restoration problem can be minimized by reproducing the data at tape speeds which produce a bit rate for which the maximum time between transitions is less than 100 microseconds. Additional methods of minimizing these effects include selecting bit synchronizers which contain special DC and low frequency restoration circuitry or recording data using biphas-level code.

Alignment of the reproducer system is very important to reproducing high quality PCM data, that is, with the lowest possible bit error probability. A PCM signature using the standard 2047-bit pseudo-random pattern, recorded on the leader and/or the trailer of the tape, provides a good method for reproducer alignment. When a pseudo-random bit error detection system is not available or when a PCM signature signal is not recorded, the recommended procedure for reproducer alignment involves the use of the eye pattern technique. The eye pattern is the result of super positioning the "zeros" and "ones" in the PCM bit stream. The eye pattern is displayed on an oscilloscope by inserting the raw reproduced bit stream into the vertical input and the reconstructed bit-rate clock into the external synchronization input of the oscilloscope. The reproducer head azimuth, amplitude equalizers, and phase equalizers are then adjusted to produce the eye pattern with the maximum height and width opening.

## 5.5 DATA SYNCHRONIZERS AND DISCRIMINATORS

This section will briefly discuss PCM bit synchronizers, PCM decommutators, and FM discriminators.

PCM bit synchronizers are devices that reconstruct a binary data stream and a clock from a noisy analog signal. Most bit synchronizers allow the operator to select input code, input bit rate, loop bandwidth, bit detector type, and input impedance. The input code and bit rate should obviously be chosen to match the incoming data. The best choice for loop bandwidth depends on the application. A narrow bandwidth performs best when the SNR is low and when there are long periods with few or no transitions. A wide loop bandwidth performs best when the input data rate is unstable. The source of instability could be recorder/reproducer time base error or an unstable clock in the transmitting system. A good nominal choice is a loop bandwidth of approximately 0.3%. The problem with making the wrong choice is that additional bit slips can occur. Bit slips can create major problems in data quality. The best bit detector is usually the filter and sample (F/S) if the NRZ-L signal has been filtered significantly (effective cutoff of 0.7 times the bit rate or lower) and the integrate and dump (I/D) with less filtering. PCM frame synchronizers use the data and clock outputs of the PCM bit synchronizer. The frame synchronizer first "finds" the synchronization pattern. The location of any word can then be found by counting the clock. Frame synchronizers usually have three levels of synchronization status: search, verify or check, and lock. The number of errors allowed in the pattern and the number of correct or incorrect patterns is frequently a variable. Many synchronizers also allow the selection of a "window" in which to look for the best match to the synchronization pattern. These windows are typically  $\pm 1$  or  $\pm 2$  bits around the expected synchronization location. This allows for a clock slip of 1 and 2 bits respectively. Most decommutation and word selection systems hold the last "good" value when frame synchronization is lost. More data can be retrieved if errors are allowed in the pattern<sup>23</sup> and at least one bad pattern is allowed in lock mode. The data will also contain more noise because marginal data is more likely to be transferred to the output.

The probability of correctly detecting synchronization<sup>23</sup> with a BER of  $p$  (independent errors assumed), a pattern length of  $n$  bits, and allowing  $q$  errors is:

$$P_{\text{sync}} = \sum_{r=0}^q \frac{n!}{(n-r)! r!} p^r (1-p)^{n-r}$$

<sup>23</sup>Hill, E. R., "Techniques for Synchronizing Pulse-Code-Modulated Telemetry".  
Proceedings of the 1963 National Telemetry Conference, paper 3-3.

This is illustrated in figures 5.5-1 and 5.5-2 for synchronization pattern lengths of 16, 24, and 32 bits. The data in figure 5.5-1 shows that if we desire to have a probability of 0.9 of detecting a 24-bit frame synchronization pattern when the BER is 0.1, we need to allow 4 errors in the pattern. If the BER is reduced to 0.01 (see figure 5.5-2), we will have a probability of greater than 0.97 of detecting the pattern if we allow 1 error. This data is useful in determining the parameters for the search, verify, and lock phases.

The probability of randomly detecting false synchronization with random data, a pattern length of  $n$  bits, and allowing  $q$  errors is:

$$P_{\text{false sync}} = \frac{\sum_{r=0}^q \frac{n!}{(n-r)! r!}}{2^n}$$

Figure 5.5-3 presents data on the probability of false detection of the synchronization pattern for pattern lengths of 16, 24, and 32 bits. This data is useful for determining parameters in search mode. Assume we have a PCM minor frame which is 4000 bits long and we would like the probability of detecting a false synchronization pattern in one minor frame time to be less than 0.2. Therefore, the probability of false detection of the synchronization pattern in any location would have to be less than  $0.2/4000$  or 0.00005. The data in figure 5.5-3 shows that we could not allow any errors in search mode with a 16-bit pattern, we could allow 2 errors with a 24-bit pattern, and we could allow 4 errors with a 32-bit pattern. If the BER is 0.1, the probability of detecting the actual synchronization pattern with a 16-bit pattern and 0 errors allowed is only 0.19. Therefore, we are more likely to detect a false pattern than the correct pattern. The acquisition time will be long under these conditions. The probability of correctly detecting the 24-bit pattern while allowing 2 errors is 0.56, while the probability of correctly detecting the 32-bit pattern while allowing 4 errors is 0.79. This illustrates the advantages of long synchronization patterns when the data is noisy.

Some frame synchronizers also use an adaptive algorithm for frame synchronization. One adaptive technique is discussed in reference 24.

FM discriminators were discussed in section 3.7. A general comment is that fixed channel discriminators perform better than tunable discriminators because the filter characteristics are usually better with fixed discriminators.

<sup>24</sup>Cox, T. F. "Analysis of an Adaptive Sequential Probability Ratio Test Type of PCM Frame Synchronizer". *Proceedings of the International Telemetry Conference*, vol. XXII, 1986, pp 61-68.

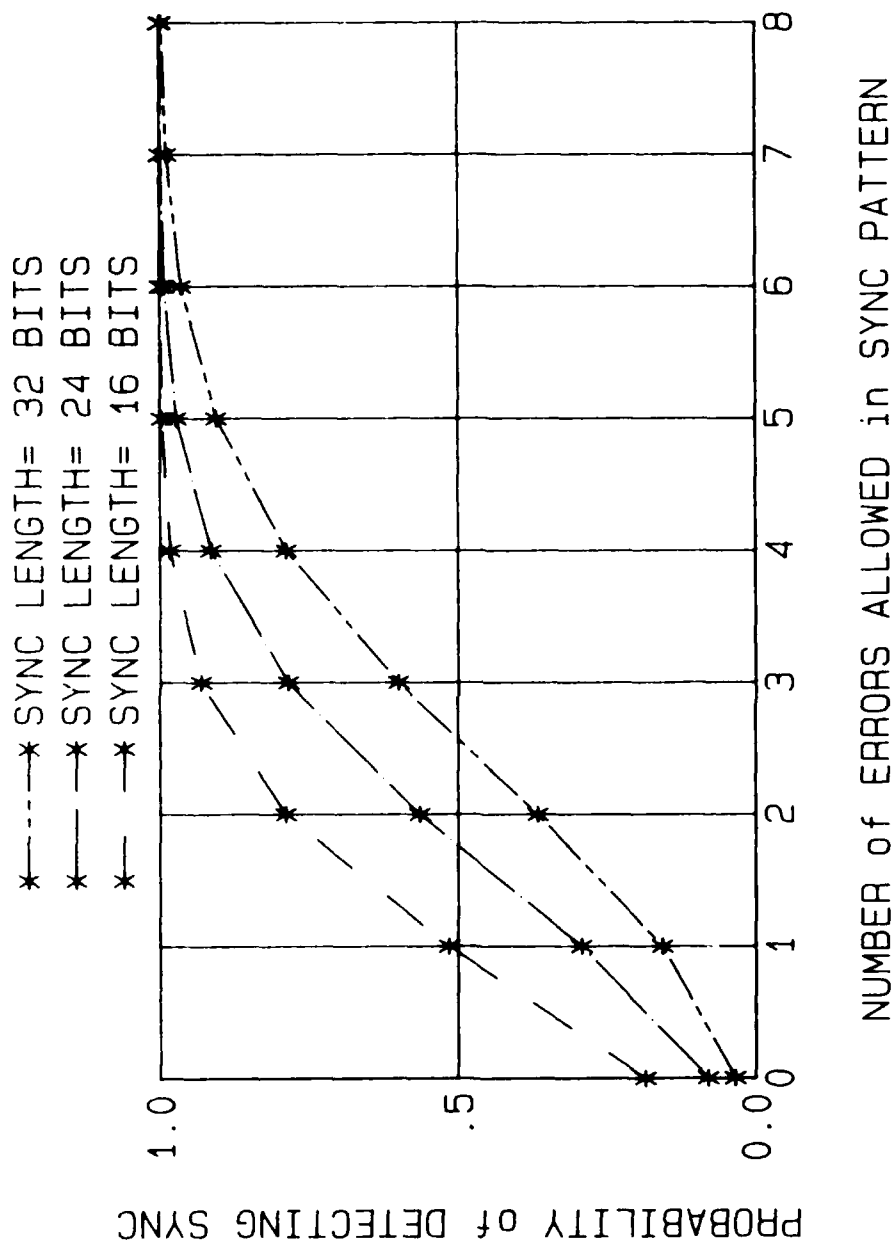


Figure 5.5-1. Probability of Detecting Sync Pattern with BER = 0.1.

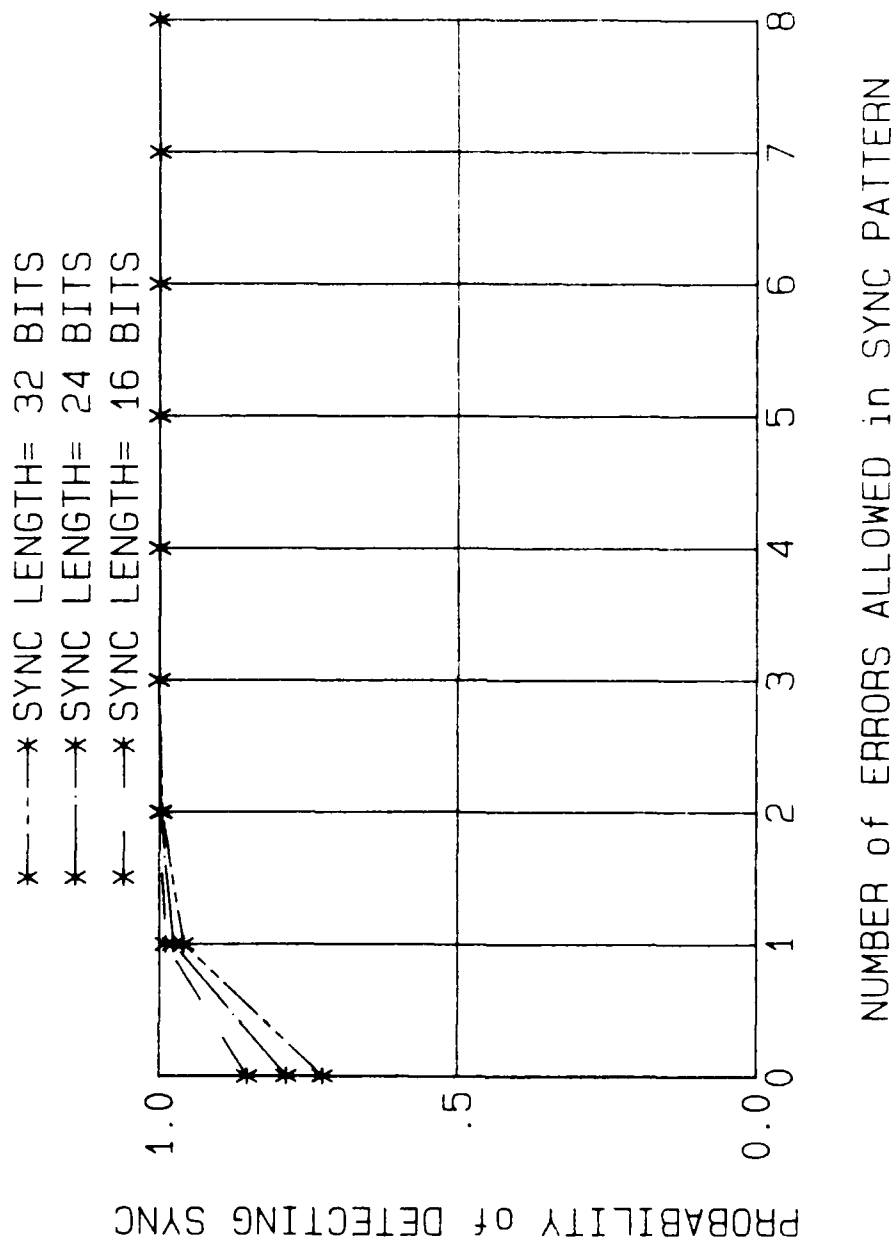


Figure 5.5-2. Probability of Detecting Sync Pattern with BER = 0.01.

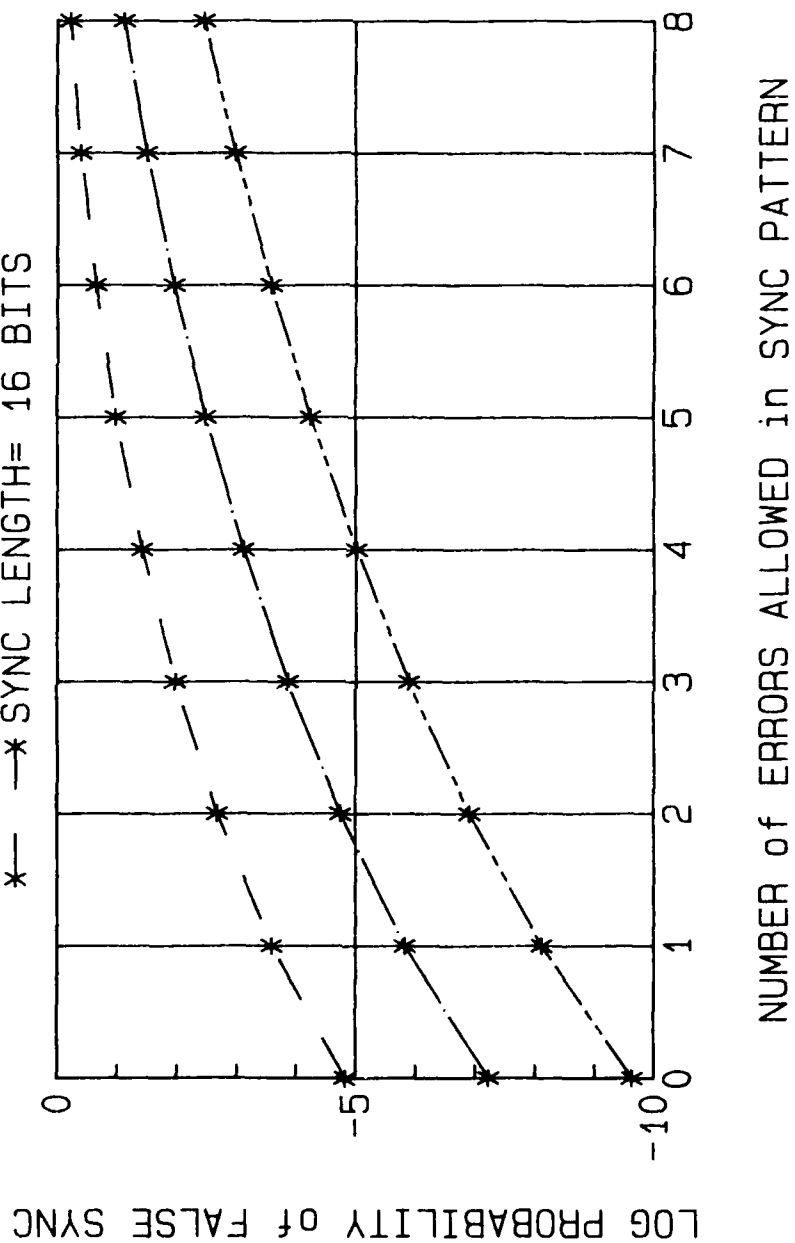


Figure 5.5-3. Probability of Detecting False Sync Pattern.

## 5.6 RECEIVING/RECORDING SYSTEM PARAMETER SELECTION GUIDELINES

### 5.6.1 Introduction

There are several important parameters to select in a telemetry ground station. These include:

1. Receiver IF bandwidth
2. Receiver oscillator type: XTAL, VFO, or AFC/APC
3. Receiver AGC time constant
4. Receiver video bandwidth and coupling (AC or DC)
5. PM or PSK demodulator loop bandwidth
6. Predetection or postdetection combining
7. Predetection carrier frequency
8. Predetection, postdetection direct, HDDR, or postdetection FM recording
9. Tape speed
10. Bit synchronizer loop bandwidth and bit detector type.

Many of these subjects are discussed in sections 3 and 5. Therefore, the discussions in this section will be brief.

### 5.6.2 Receiver IF Bandwidth

The best receiver IF bandwidth for an FM signal is the narrowest bandwidth that will pass the information without significant distortion. This is usually the narrowest IF bandwidth that is wider than two to three times the larger of maximum frequency of interest or peak deviation plus the frequency uncertainty in the system. The following IF bandwidths are listed in the Telemetry Standards (IRIG Standard 106-86): 100, 300, 500, and 750 kHz and 1.0, 1.5, 2.4, 3.3, 4.0, 6.0, 10.0 MHz. All of these bandwidths may not be available at a particular receiving facility. The best IF bandwidth for NRZ PCM/FM is 1 to 1.5 times the bit rate for peak deviations of 0.35 times the bit rate. If the bit rate is low, a larger deviation may be needed. If the peak deviation is 100 kHz and the bit rate is 10 kb/s, then a 300 kHz IF bandwidth would be a good choice. However, the system BER would normally be lower if a phase modulated system with 90 degree peak deviation were used in this case. The performance of various IF bandwidths with various modulation methods is discussed in more detail in section 3.

The best receiver IF bandwidth for a PM signal is the widest bandwidth that rejects all significant interfering signals. In practice, there is little to be gained by using an IF filter much wider than twice the premodulation bandwidth.

The IF filter should not be wider than twice the predetection carrier frequency. The problem with using wider filters is that the noise folds across zero frequency and back into the passband during the downconversion process.



### **5.6.3 Receiver Oscillator Type**

The XTAL mode is best for most applications. The VFO mode is useful if the receiver operator needs to fine tune the receiver during an operation. The AFC mode may be useful for tracking signals that have large carrier frequency variations. However, AFC systems usually perform poorly at low SNRs and may cause problems with predetection combiners. APC may be needed for proper operation of PM and PSK demodulators.

### **5.6.4 Receiver AGC Time Constant**

The best AGC time constant for data receivers is usually the fastest available time constant (frequently 0.1 ms). Tracking receivers may need longer time constants.

### **5.6.5 Receiver Video Bandwidth and Coupling**

The receiver video bandwidth must be wide enough to pass the maximum frequency of interest. DC coupling should be used if the transmitted signal has a significant DC component. DC is especially important for baseband PAM/FM.

### **5.6.7 PM and PSK Demodulator Loop Bandwidth**

The best loop bandwidth depends on the application. If rapid, spurious, phase variations are expected, due to unstable transmitter or flame attenuation, a wide loop bandwidth is needed to track the variations. A narrow loop bandwidth is best with a noisy signal and a stable transmitter.

### **5.6.8 Predetection or Postdetection Combining**

A predetection combiner will always perform as well as or better than a postdetection combiner if the predetection combiner can maintain proper phase alignment of the signals. AFC systems introduce excessive phase noise which tends to cause problems in the combiner phase-locked loop, therefore, AFC and predetection combining should not usually be used together. Postdetection combining does not work well with PCM/FM signals. Postdetection combining should not be used with PSK demodulator outputs unless a polarity alignment circuit is added to the combiner. Diversity combining is discussed in more detail in subsection 5.3.

### **5.6.9 Predetection Carrier Frequency**

The predetection carrier frequency should be at least twice the maximum information frequency of interest. This means that a 900 kHz predetection carrier should not be used with NRZ PCM bit rates higher than 900 kb/s or biphase PCM bit rates higher than 450 kb/s. The predetection carrier frequency should also be larger than one-half of the IF bandwidth.

#### **5.6.10 Recording Method**

Predetection recording is recommended whenever possible because the signal has been processed less than with other methods. However, predetection recording and FM recording are the least efficient methods in terms of data bandwidth per inch per second of tape speed. Serial HDDR has the most record margin for PCM signals. Biphasic (Manchester) signals are recommended for serial HDDR if the bit packing density is less than 15 kb/in for wideband systems or 30 kb/in for double density systems. Randomized NRZ-L is recommended for serial HDDR at packing densities up to 25 kb/in for wideband systems (50 kb/in for double density systems) as long as the reproduce bit rate is greater than 200 kb/s (400 kb/s for double density systems). Hybrid systems can be recorded directly on the baseband if low frequency response is not needed.

#### **5.6.11 Tape Speed**

The tape speed is determined by the maximum frequency to be recorded. Wideband systems have a bandwidth of 1 MHz at 60 ips while double density systems have a bandwidth of 1 MHz at 30 ips.

#### **5.6.12 Bit Synchronizer Loop Bandwidth and Bit Detector Type**

The best loop bandwidth depends on the application. Narrow bandwidths perform better in noisy environments if the bit rate is stable while wide bandwidths perform better with unstable bit rates. Recorder time base error and unstable transmitting system clock are two sources of bit rate instability. A loop bandwidth of 0.3% is a good choice for most applications. The best bit detector for a heavily filtered signal is the filter and sample (F/S) detector. The best bit detector for a relatively unfiltered data stream is usually an integrate and dump (I/D) detector.

## 5.7 DATA QUALITY MONITORING

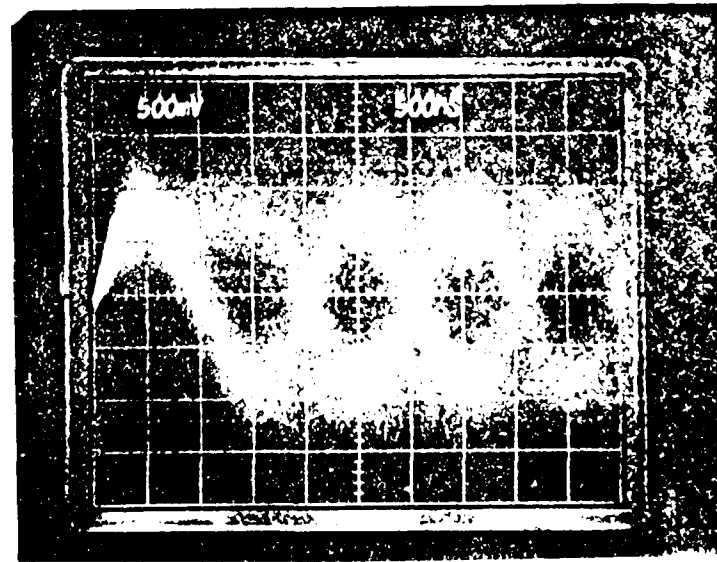
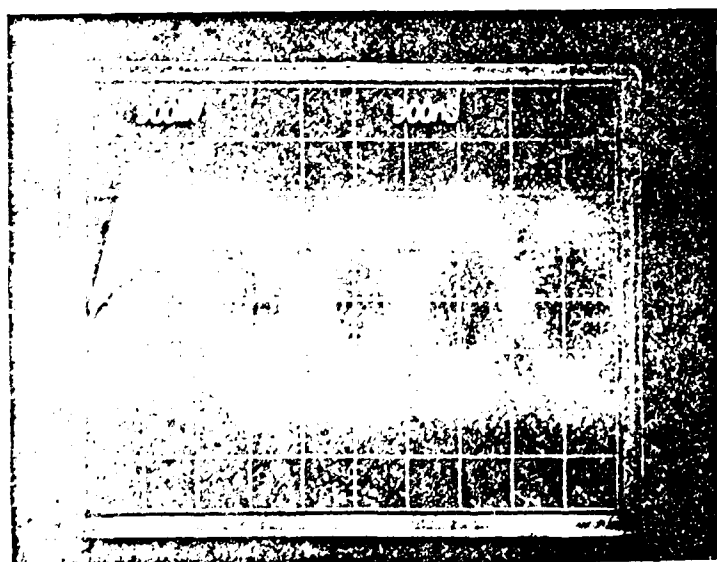
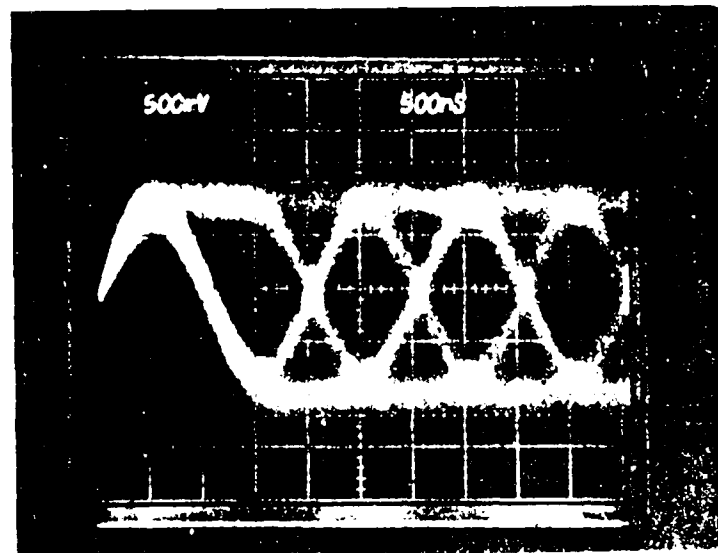
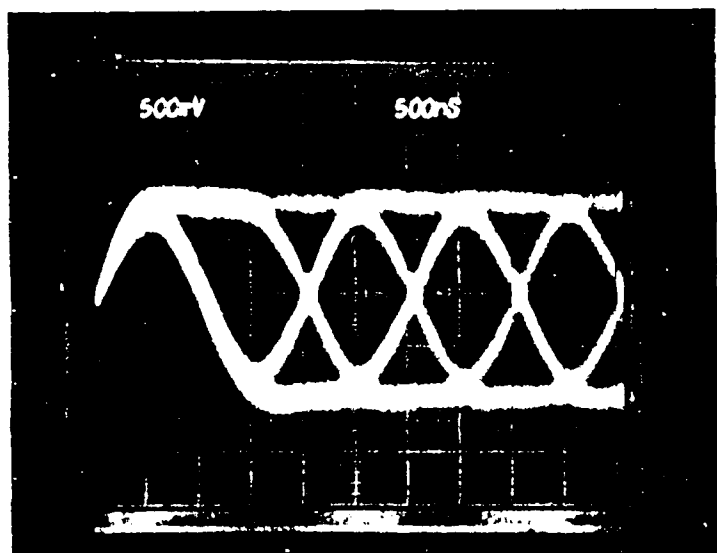
The data quality can be monitored at various points in the telemetry ground station. This subsection will discuss monitoring the data quality using calibrated AGCs, spectrum analyzer displays of predetection and postdetection signals, and oscilloscope displays of postdetection signals. Time division multiplex systems can also be monitored using the synchronization status of a decommutator. The data quality of individual demultiplexed signals can be monitored using strip chart recorders, etc.

The received data quality can be monitored by using a calibrated AGC voltage to estimate received SNR along with monitoring the predetection signal on a spectrum analyzer and the video output on an oscilloscope. The predetection and video outputs are monitored to look for improper tuning and filtering.

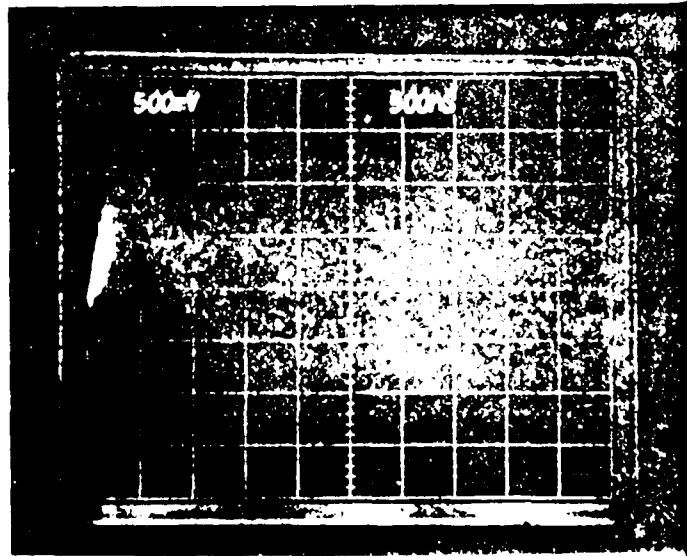
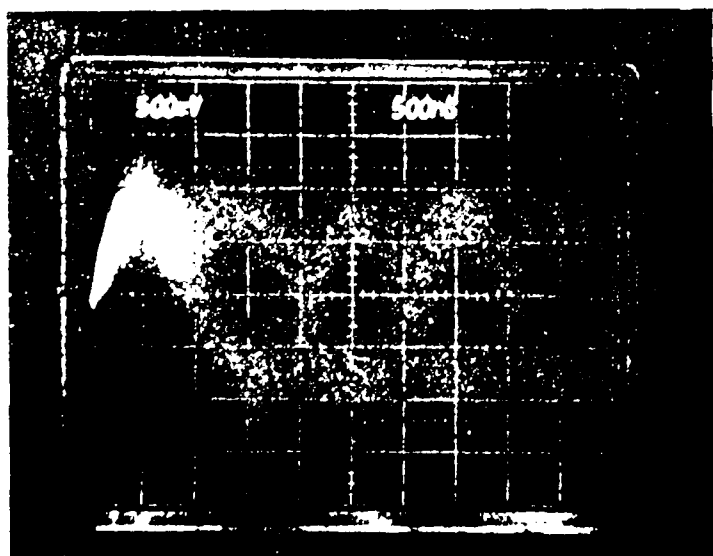
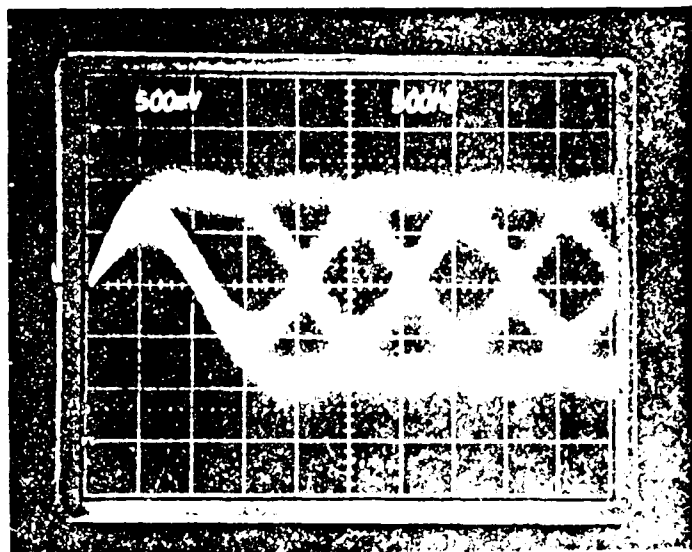
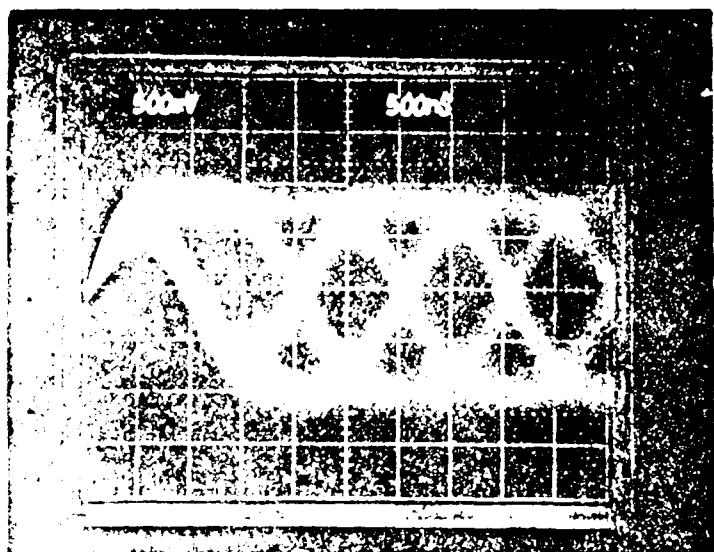
Typical oscilloscope eye patterns are shown in figures 5.7-1 and 5.7-2 for IF SNRs from 18 dB to 2 dB. These photos can be used to get a qualitative estimate of SNR and data quality for PCM signals. The BER was less than  $10^{-8}$  for the 14 and 18 dB IF SNRs. The BER was approximately  $10^{-4}$  at a 10 dB IF SNR,  $1.4 \times 10^{-2}$  at a 6 dB IF SNR, and  $1.2 \times 10^{-1}$  at a 2 dB IF SNR.

Figures 5.7-3 through 5.7-7 show typical IF spectra for randomized NRZ-L PCM/FM signals with an IF bandwidth of 1.5 times the bit rate and a peak deviation of 0.35 times the bit rate. These figures show that we can estimate the IF SNR by subtracting approximately 3 dB from the ratio of the signal in the center of the band to the noise at the spectral minimum. The spectral minimum in this case is at  $\pm 65\%$  of the bit rate from the receiver output center frequency. This estimate is quite accurate for IF SNRs less than 15 dB as long as the deviation is approximately 0.35 times the bit rate. The correction factor (3 dB in this case) is a function of the ratio of IF bandwidth to bit rate. This method does not work well for IF bandwidths approximately equal to the bit rate. The spectrum of the video signal can also be used to estimate SNR.

The tape recorder outputs should be monitored to verify that the tape recorder is working properly. The recorder output also includes the entire receive/record path and if the signal is good at the recorder output it must have been good at all points upstream in the signal path. Therefore, the recorder output is the best single point to monitor the data quality.



$\frac{1}{2} \times \frac{1}{2} = \frac{1}{4}$ 
 $\frac{1}{2} \times \frac{1}{4} = \frac{1}{8}$ 
 $\frac{1}{4} \times \frac{1}{4} = \frac{1}{16}$ 
 $\frac{1}{2} \times \frac{1}{16} = \frac{1}{32}$ 
 $\frac{1}{4} \times \frac{1}{16} = \frac{1}{64}$ 
 $\frac{1}{2} \times \frac{1}{64} = \frac{1}{128}$ 
 $\frac{1}{4} \times \frac{1}{64} = \frac{1}{256}$



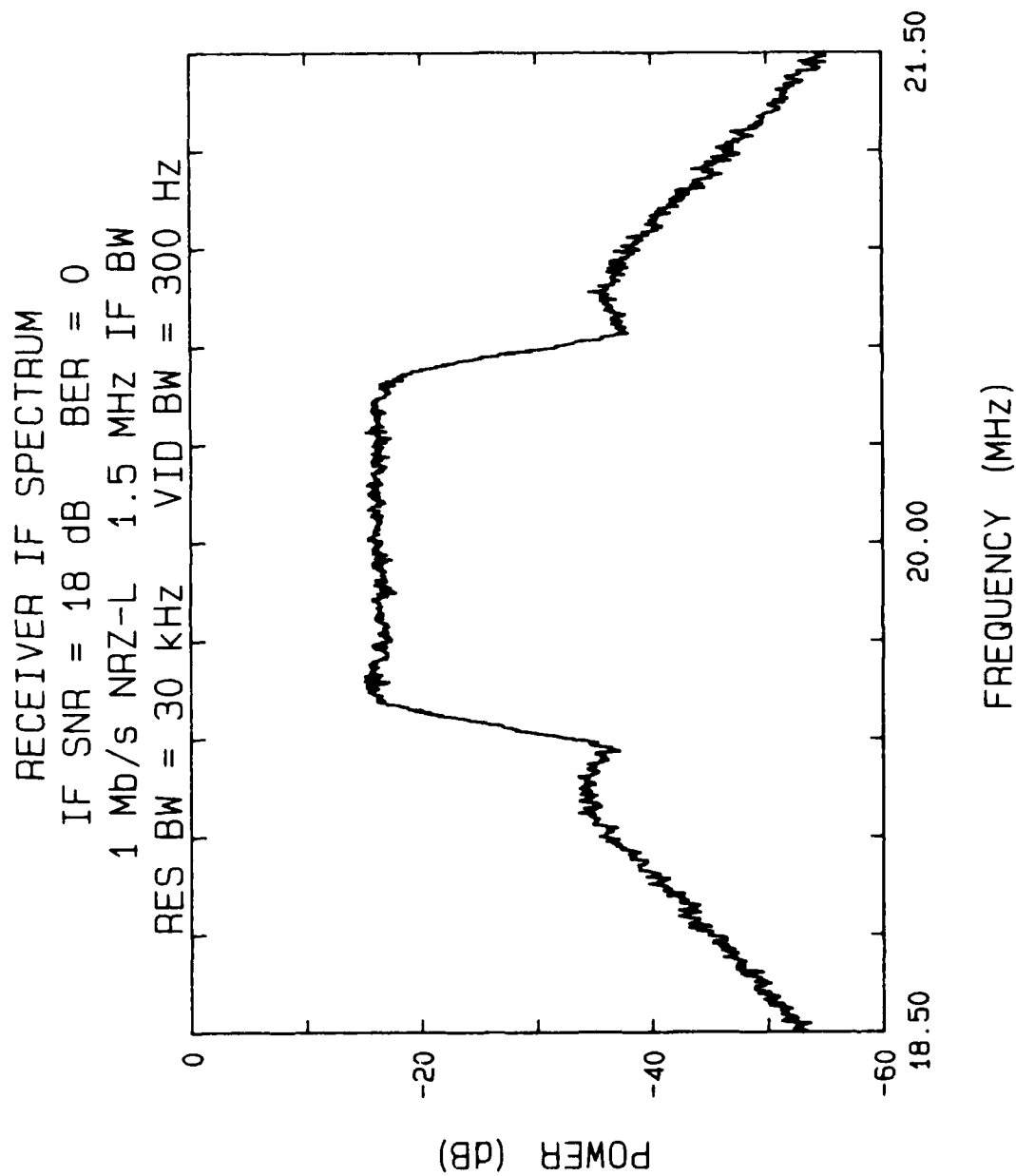


Figure 5.7-3. Receiver IF Spectrum at 18 dB IF SNR.

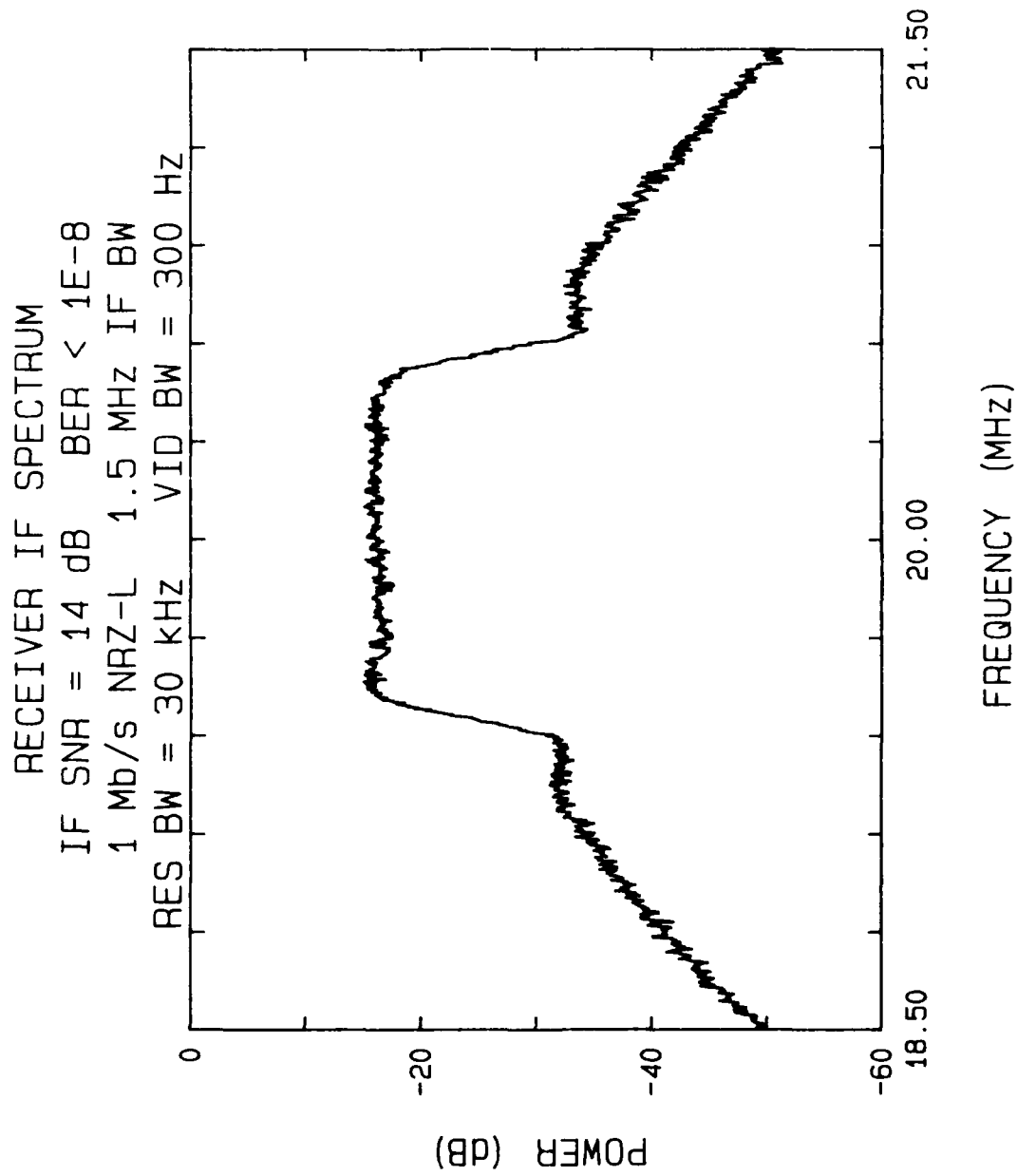


Figure 5.7-4. Receiver IF Spectrum at 14 dB IF SNR.

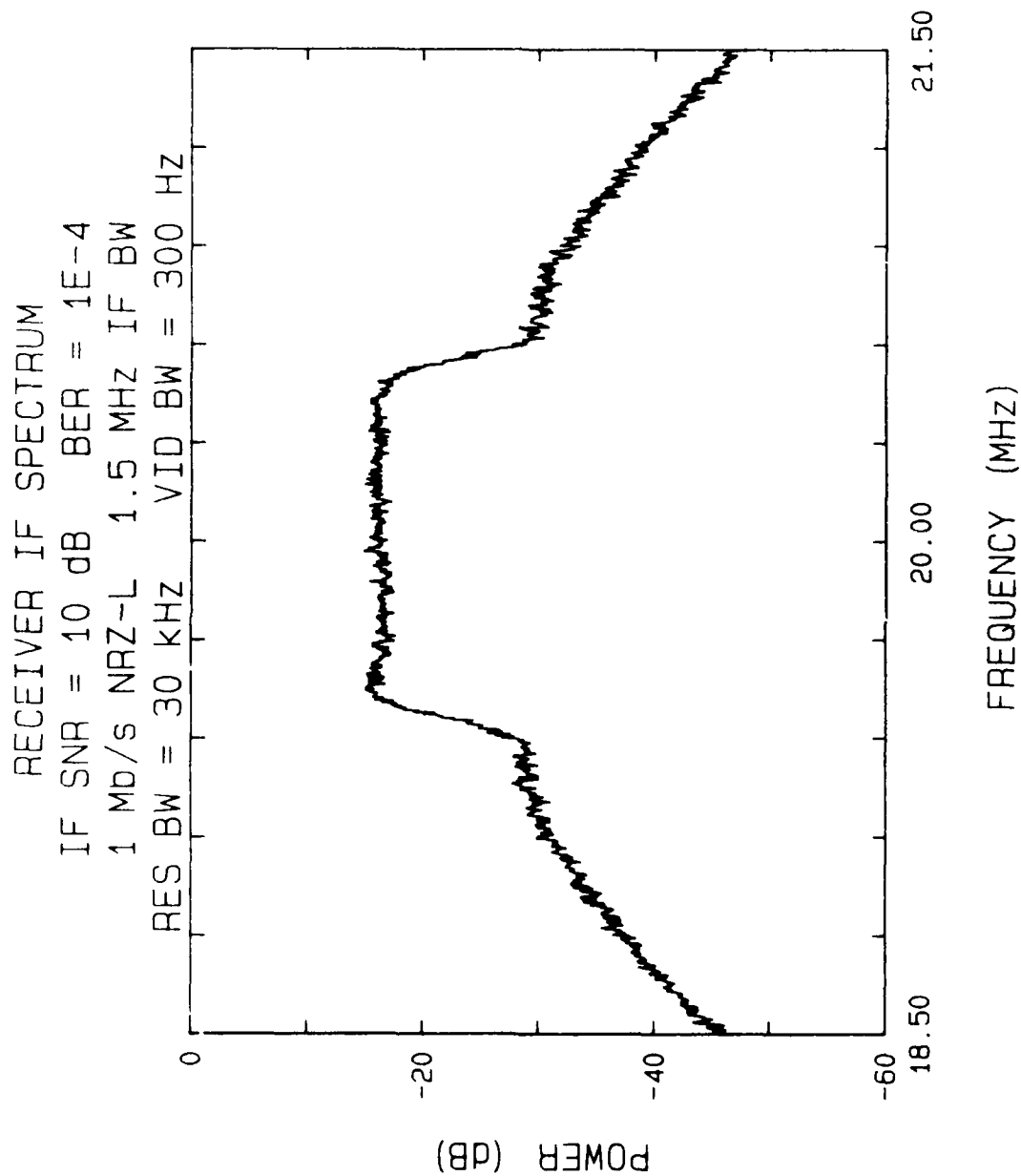


Figure 5.7-5. Receiver IF Spectrum at 10 dB IF SNR.



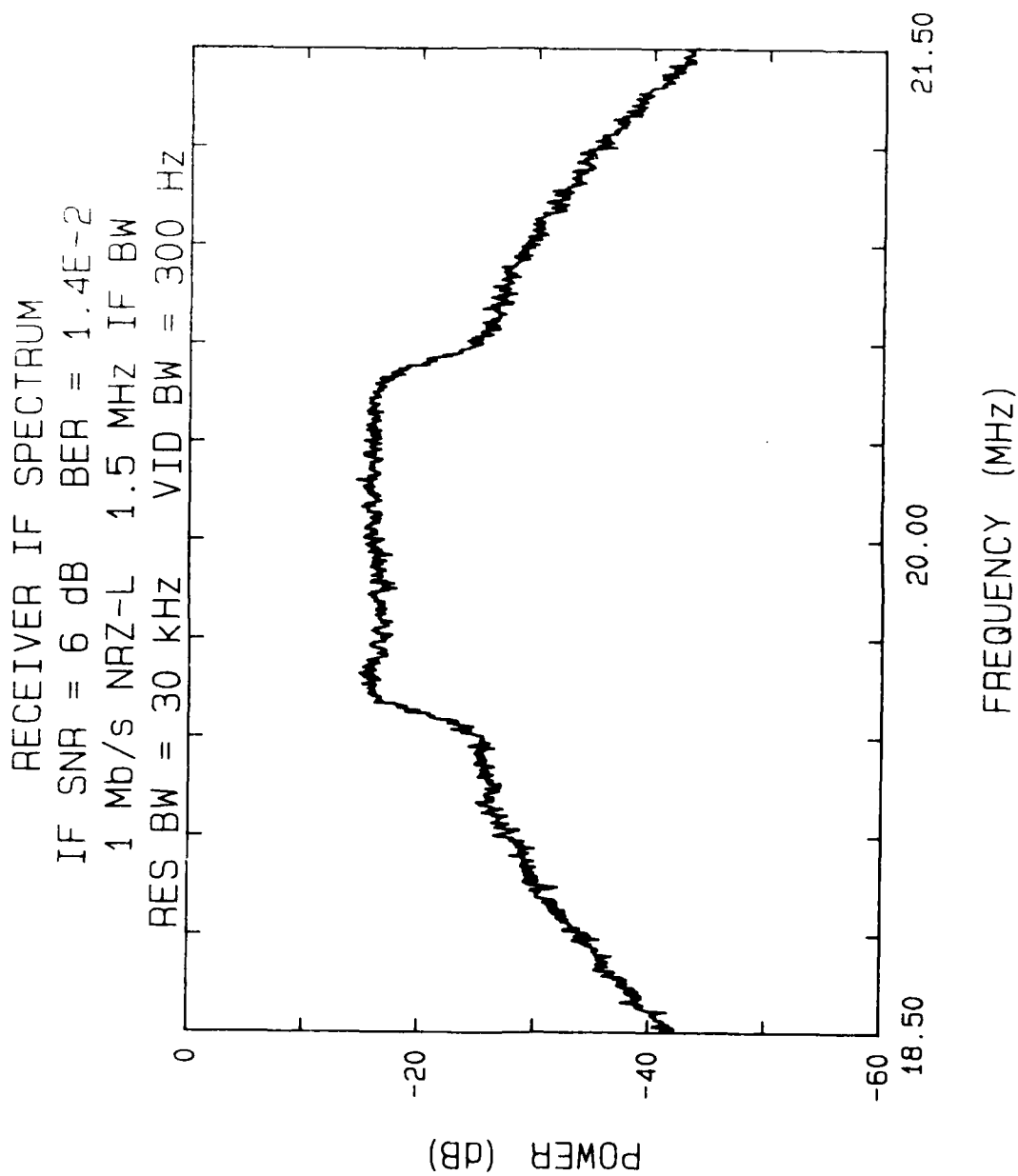


Figure 5.7-6. Receiver IF Spectrum at 6 dB IF SNR.

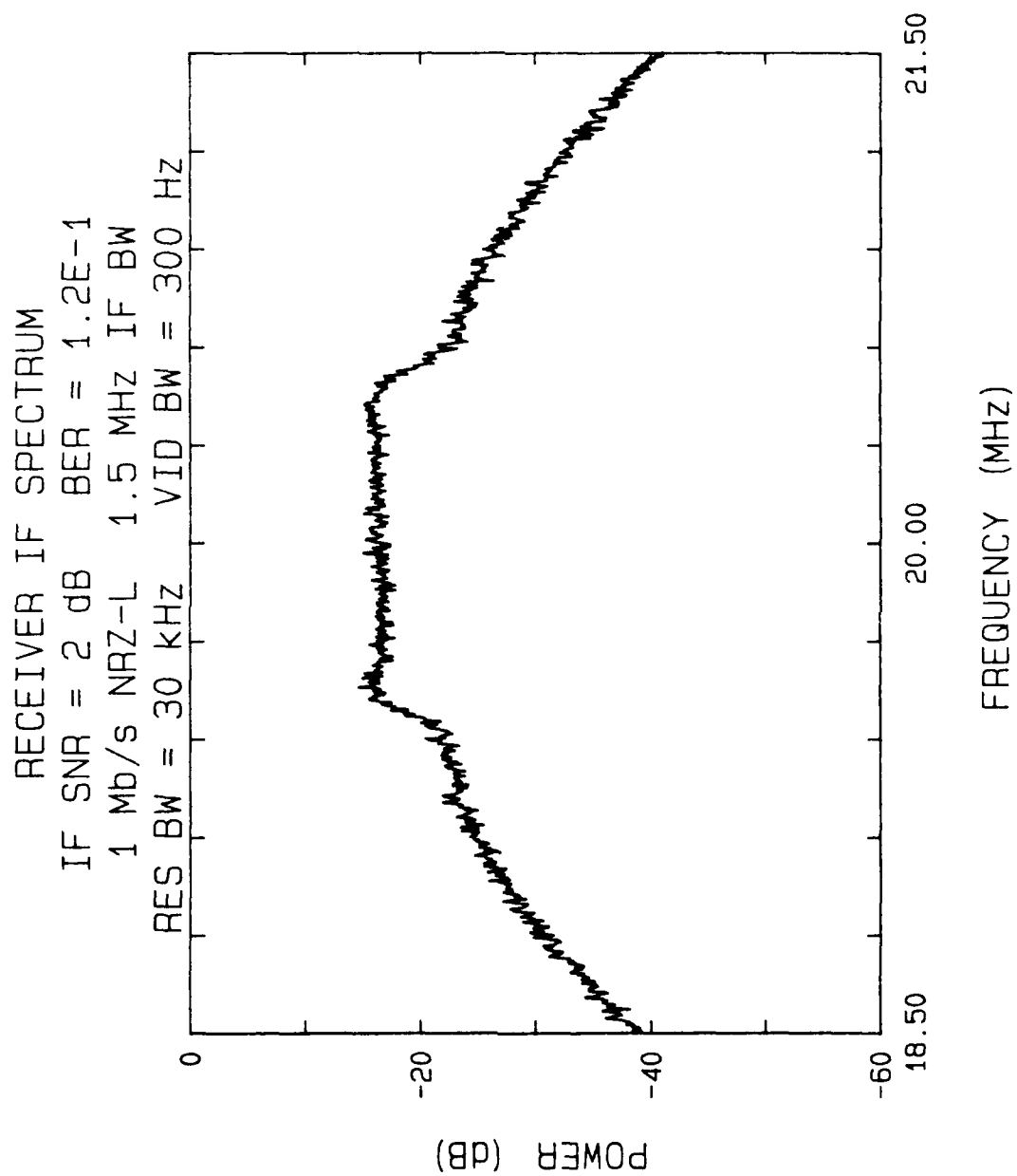


Figure 5.7-7. Receiver IF Spectrum at 2 dB IF SNR.

## 5.8 REFERENCES

Secretariat, Range Commanders Council. End-to-End Test Methods for Telemetry Systems. White Sands Missile Range, NM, RCC Document 118-79 Volume I.

Hedeman, W. R. "The Sun as a Calibration Source for L- and S-band Telemetry". in Proceedings of the International Telemetry Conference, Vol. IV, pp.330-342, 1977.

Guidice, D. A. and J. P. Castelli. "The Use of Extraterrestrial Radio Sources in the Measurement of Antenna Parameters", IEEE Transactions on Aerospace and Electronic Systems, Vol. AES-7 No. 2, March, 1971.

Secretariat, Range Commanders Council. Test Methods for Data Multiplex Equipment. White Sands Missile Range, NM, RCC Document 118-79 Volume-IV.

Johnson, R. C., and H. Jasik. Antenna Engineering Handbook, Second Edition, McGraw-Hill, New York, 1984.

Stutzman, W. L., and G. A. Thiele. Antenna Theory and Design, John Wiley, New York, 1981.

Pettai, R. Noise in Receiving Systems. Wiley, New York, 1984.

Gregg, W. D. Analog and Digital Communication. Wiley, New York, 1977.

Gagliardi, R. M. Introduction to Communications Engineering. Wiley, New York, 1978.

Hill, E.R. "AM/AGC weighted Pre-Detection Diversity Combining," in Proceedings of International Telemetry Conference, Vol. 13, pp 215-238, Oct. 1977.

Berns, K.L. "Benefits of Polarization Diversity Reception," in Proceedings of International Telemetry Conference, Vol. 20, pp 627-642, Oct. 1984.

Secretariat, Range Commanders Council. Telemetry Standards. White Sands Missile Range, NM, RCC, May 1986. (IRIG Standard 106-86).

Jorgensen, F. The Complete Handbook of Magnetic Recording. TAB Books, Blue Ridge Summit, PA, 1980.

Camras, M. Magnetic Tape Recording. Van Nostrand, New York, 1985.

White, R. Introduction to Magnetic Recording. IEEE Press, New York, 1984.

Daniel, E. D. and C. D. Mee, Eds. Magnetic Recording-vol. I: Technology. McGraw-Hill, New York, 1986.

Mee, C. D. and E. D. Daniel, Eds. Magnetic Recording-vol. II: Applications. McGraw-Hill, New York, 1987.

Mallinson, J. C. Foundations of Magnetic Recording. Academic Press, Orlando, FL, 1987.

Proceedings of the IEEE, November 1986. (Special Issue on Magnetic Recording).

Wallace, R. L. "The Reproduction of Magnetically Recorded Signals", Bell System Technical Journal, October 1951.

Law, E. L. Serial High Density Digital Recording Using a Wideband Analog IRIG Recorder/Reproducer. Pacific Missile Test Center, Point Mugu, CA, May 1981.

Kalil, F. and A. Buschman (Eds.) High-Density Digital Recording. NASA Reference Publication 1111, September 1985.

Hill, E. R., "Techniques for Synchronizing Pulse-Code-Modulated Telemetry". Proceedings of the 1963 National Telemetry Conference, paper 3-3.

Cox, T. F. "Analysis of an Adaptive Sequential Probability Ratio Test Type of PCM Frame Synchronizer". Proceedings of the International Telemetry Conference, vol. XXII, 1986, pp 61-68.

Gagliardi, R. M. Introduction to Communications Engineering. Wiley, New York, 1978.

Tjhung, T. T., and Wittke, P. H. "Carrier Transmission of Binary Data in a Restricted Band," in IEEE Transactions on Communications, Vol. COM-18, pp. 295-304, August 1970.

Cartier, D. E. "Limiter-Discriminator Detection Performance of Manchester and NRZ Coded FSK," in IEEE Transactions of Aerospace and Electronic Systems, Vol. AES-13, pp. 62-70, January 1977.

Korn, I. "Error Probability and Bandwidth of Digital Modulation," in IEEE Transactions on Communications, Vol. COM-28, pp. 287-290, February 1980.

Tan, C. H., T. T. Tjhung, and H. Singh. "Performance of Narrow-Band Manchester Coded FSK With Discriminator Detection," in IEEE Transactions on Communications, Vol. COM-31, pp. 659-667, May 1983.

Taub, H. and D. L. Schilling. Principles of Communication Systems, McGraw-Hill, New York, pp 162-179, 1971.

Gregg, W. D. Analog and Digital Communication, John Wiley and Sons, New York, pp 267-294, 1977.

Downing, J. J. Aerospace Telemetry, Volume I, (ed. by H. L. Stiltz), Prentice-Hall, Englewood Cliffs, NJ, pp 83-141, 1961.

Hochman, D. Handbook of Telemetry and Remote Control, (ed. by E. L. Gruenberg), McGraw-Hill, New York, pp 9-2 to 9-198, 1967.

Heberling, E. D. An Experimental Evaluation of the Characteristics of PAM-NRZ/FM Telemetry Systems, Naval Ordnance Laboratory Corona, Corona, California, September 1967. (NOLC Report 741).

Nichols, M. H. and L. L. Rauch. Radio Telemetry, J. Wiley, 1956.

Law, E. L., E. T. Kimball, and M. H. Nichols. "Relationship of Noise Power Ratio to FM/FM Data Quality", in Proceedings of the International Telemetry Conference, Vol. XII, pp 234-250, 1976.

Law, E. L., E. T. Kimball, and M. H. Nichols. Relationship of Noise Power Ratio to Subcarrier Discriminator Signal-to-Noise Ratio, Pacific Missile Test Center, Point Mugu, CA, Aug 1975. PMTC TP-75-21.

Sklar, B. "What the System Link Budget Tells the System Engineer or How I Learned to Count in Decibels", in Proceedings of the International Telemetry Conference, Vol. XV, pp 331-344, 1979.

Lantz, N. F., and M. H. Nichols. "Approximate Design Formulae and Procedures for Designing Hybrid Telemetry Systems Using an FM Carrier", in Proceedings of the International Telemetry Conference, Vol. XIII, pp 261-271, 1977.

Law, E. L. Pulse Code Modulation Telemetry, Properties of Various Binary Modulation Types. Pacific Missile Test Center, Point Mugu, CA, TP000025, June 1984.

## INDEX

- AGC, receiver, 5.3-2, 5.6-2
- Amplifier, low noise, 2.1-1, 5.2-1
- Antenna, receiving, 3.9-6, 5.1-1
  - transmitting, 3.9-5
- Attenuation
  - Atmospheric, 3.9-6
  - Flame, 3.9-6
  - Path, 3.9-5
- Azimuth, 5.4-3
- Bandwidth, occupied RF
  - NRZ PCM/FM, 3.1-21
  - Biphase PCM/FM, 3.2-5
  - NRZ PCM/PM, 3.3-12
  - Biphase PCM/PM, 3.4-10
  - NRZ PAM/FM, 3.6-20
  - FM/FM, 3.7-37
- Bias recording, 5.4-7
- Biphase PCM signals, 3.2-1, 3.4-1
- Bit error rate
  - NRZ PCM/FM, 3.1-1
  - Biphase PCM/FM, 3.2-1
  - NRZ PCM/PM, 3.3-1
  - Biphase PCM/PM, 3.4-1
  - PSK, 3.5-1
  - Link analysis, 3.9-8
  - Testing, 5.0-2
  - Estimating, 5.7-1
- Bit synchronizer
  - NRZ PCM/FM, 3.1-14
  - Biphase PCM, 3.2-5
  - NRZ PCM/PM, 3.3-12
  - Loop bandwidth, 5.6-3
- Constant bandwidth, 3.7-1, 3.7-23, 3.7-24
- Crossplay, 5.4-3
- Crosstalk, 3.7-22
- Data multiplexing, 3.0-1, 4.1-1
- Derandomizer, 5.4-28
- Deviation
  - Peak, 3.1-3, 3.2-1, 3.3-1, 3.4-3, 3.6-1, 3.7-19
  - Ratio, 3.7-1, 3.7-5
  - Residual, 3.1-3, 3.6-1
- Direct recording, 5.4-2
- Discriminator, FM 3.7-1 -24, 5.5-2
- Diversity combiner, 3.9-5, 5.3-5-9
- Diversity reception, 3.9-5
- Downconverter, 5.2-4
- Ducting, 3.9-6
- Equalization, 5.4-7
- Eye pattern, 3.4-15, 5.7-1-3
- Filter
  - Constant amplitude, 3.1-8, 3.3-12, 3.7-5
  - Constant delay, 3.1-8, 3.3-12, 3.7-5
- Flame attenuation, 3.9-6
- Flutter, 3.7-24
- FM/FM, 3.7-1-41
- Frequency division multiplex, 1.2-3, 3.0-1, 3.7-1
- Frequency modulation, 3.1-1, 3.3-1, 3.6-1, 3.7-1
- Gap, magnetic recording, 5.4-7
- Ground station, 5.0-1
- G/T, antenna, 5.0-1
- Head, magnetic recording, 5.4-3
- High density digital recording, 5.5-23-30
- Hybrid modulation, 5.8-1
- Incidental FM, 3.1-3, 3.6-1
- Interference, FM/FM, 3.7-22
- Magnetic tape recording, 5.4-1-30
- Modulation index, 3.7-32-37
- Multicoupler, 5.2-4
- Multipath, 3.9-6
- Noise
  - Figure, 5.2-1
  - Fluctuation, 3.1-4, 3.11-1-4
  - Pop, 3.1-4, 3.11-1-18
  - Temperature, 5.0-1, 5.2-1
- Noise power ratio, 3.7-42-50, 5.0-2
- Non-return-to-zero
  - PAM, 3.6-1-19
  - PCM, 3.1-1-30, 3.3-1-15
- Normal record level, 3.7-24, 5.4-7, 5.4-16
- Packing density, 5.4-23
- Polarization diversity, 3.9-5-7, 5.3-5-9
- Preemphasis, 3.7-24
- Premodulation filtering
  - NRZ PCM/FM, 3.1-8, 3.1-21
  - Biphase PCM/FM 3.2-5

- Premodulation filtering
  - NRZ PCM/PM, 3.3-7, 3.3-12
  - Biphase PCM/PM, 3.4-3, 3.4-10
  - PSK, 3.5-1
  - PAM, 3.6-4, 3.6-18-225
- Propagation loss, 3.9-5
- Proportional bandwidth, 3.7-1, 3.7-19-24
- Phase shift keying, 3.5-1
- Pulse amplitude modulation, 3.6-1-25
- Pulse code modulation
  - NRZ PCM/FM, 3.0-2, 3.1-1-30
  - Biphase PCM/FM, 3.0-3, 3.2-1-11
  - NRZ PCM/PM, 3.0-4, 3.3-1-15
  - Biphase PCM/PM, 3.0-5, 3.4-1-20
- Randomized NRZ, 5.4-23-30
- Receiver, telemetry, 5.3-1-5, 5.6-1
- Receiver IF filter selection, 5.3-2, 5.6-1
  - NRZ PCM/FM, 3.1-11
  - Biphase PCM/FM, 3.2-5
  - NRZ PCM/PM, 3.3-8
  - Biphase PCM/PM, 3.4-10
  - NRZ PAM/FM, 3.6-18
  - FM/FM, 3.7-22
- Receiver video filter selection, 5.3-2, 5.6-2
  - NRZ PCM/FM, 3.1-14
  - Biphase PCM/FM, 3.2-5
  - NRZ PCM/PM, 3.3-8
  - NRZ PAM/FM, 3.6-18
- Relay Systems, 3.10-1-5
- Serial high density digital recording, 5.4-23-28
- Signal conditioning, 1.2-3, 4.1-1
- Signal-to-noise ratio, 3.1-1, 3.6-4, 3.7-1, 3.9-8, 3.10-2-4, 5.4-16, 5.7-1
- SNR margin, 3.9-8
- Tape recording, 5.4-1-30
- Threshold, FM, 3.7-5
- Time division multiplex, 1.2-3, 3.0-1, 4.1-1
- Transducer, 1.2-1, 4.1-1